MODEL FOR PREDICTION OF HIGHWAY CONSTRUCTION PRODUCTION RATES

Ву

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A DISSERTATION PRESENTED TO THE GRADUATE SCHOOL
OF THE UNIVERSITY OF FLORIDA IN PARTIAL FULFILLMENT
OF THE REQUIREMENTS FOR THE DEGREE OF
DOCTOR OF PHILOSOPHY

UNIVERSITY OF FLORIDA

1989

ACKNOWLEDGEMENTS

I would like to express my gratitude to Professor Zohar Herbsman. His guidance and support have contributed a great deal to this research.

Additionally, have appreciated the suggestions and comments of Professor James Schaub, Professor Rodney Cox and Professor Fazil Najafi. Their participation has been very helpful.

Finally, I would like to thank Mr. David Enck, who provided a great deal of assistance with the statistical considerations.

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Abstract of Dissertation Presented to the Graduate School of the University of Florida in Partial Fulfillment of the Requirements for the Degree of Doctor of Philosophy

MODEL FOR PREDICTION OF HIGHWAY CONSTRUCTION PRODUCTION RATES

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August 1989

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Construction production rates are important in many construction management functions. Cost estimating, cost control, scheduling and resource allocation all rely upon production rate data. The prediction of future production rates is essential.

Construction production rates are extremely variable. Historically the prediction of production rates has been difficult and often inaccurate.

This dissertation presents the concept of a factorial model for explaining the variance associated with construction production rates. Production rates are affected by many influencing factors. Identification and quantification of the influencing factors allow a more complete understanding of the work process.

The considerations of factor identification and data collection systems are discussed. Model development and statistical procedures are presented. A comprehensive approach for developing a production rate prediction model is developed.

A demonstration prediction model is developed from a survey data base of production rate observations taken from 60 different highway construction projects in the state of Florida.

CHAPTER 1

INTRODUCTION AND PROBLEM STATEMENT

Importance of Production Rate Information

Production rates are perhaps the key data element in the construction industry management process. Almost all central management functions depend directly on production rate data. Cost estimating, cost control, scheduling and resource allocation are all based upon calculations which include production rate values. In fact, it is difficult to imagine a construction management function which is not influenced by production rates. Consequently, the effectiveness of the management process is largely dependent upon the quality of the production rate data available. In this instance, quality refers to the accuracy, relevance and timeliness of the production rate data. Figure 1 presents a schematic illustration of the relationship between production rates and the construction management process.

The construction manager relies heavily upon production rate information when performing the following three fundamental project management functions:

Estimating

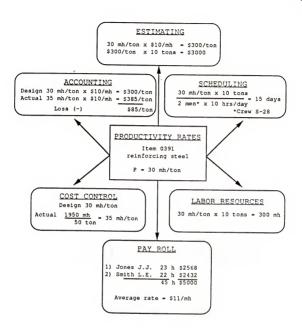


Figure 1. - Relationship Between Productivity Rates and Other Areas in the Construction Management Process, (Herbsman and Ellis 1989) Reprinted with permission of publisher

- 2. Planning and Scheduling
- Resource Allocation

Estimates of labor or equipment cost are based upon production rates. Given a certain level of resources, the manager must determine how quickly the work can be performed. Cost also is directly related to production rate. Consider the following example:

Cost Estimating:

Unit Cost = Cost/time x Production Rate
Unit Cost = \$60/hr. x .20 Tons/Hr. = \$120/Ton
Reinforcing

_

Crew S-28

 $\label{thm:continuous} \mbox{Variations in production rates significantly effect cost.}$

Production rates also determine the time required to perform individual activities. Consequently the schedule and plan for accomplishing the project are based upon production rates.

As an example, consider a calculation of the time required to install reinforcing steel.

Scheduling:

Activity Duration = $\frac{\text{Quantity of Work}}{\text{Production Rate}}$

Activity Duration = 200 Tons = 1000 Hrs. Reinforcing Steel .20 Tons/Hr Crew S-28

Activity times are a direct function of the production rate.

Construction resource management generally involves the allocation of resources to obtain certain time and cost objectives. We want to complete the construction project within a given amount of time and at minimum cost. Since production rates are used in both time and cost calculations, they are an integral part of construction resource management.

Need for Accurate Predictions of Production Rates

Construction is a rather unique production process. In traditional manufacturing cost estimating, planning and scheduling, and resource management are also important management concerns. The manufacturing process involves application of resources and materials to produce a large number of identical products. As the manufacturing process proceeds, production rate assumptions can be refined from actual experience.

Construction, however, is concerned with manufacturing a single one-time product. It is true that similar projects may be done in the future, but the basic circumstances are likely to be different. Variables such as site location, weather, subcontractors change from job to job. Consequently, the construction manager is challenged to estimate and schedule the construction project on the basis of predicted production rates.

Clearly the effectiveness of the construction management is directly dependent upon the quality of the

production rate data. Inaccurate production rate predictions can produce serious problems in the construction process. Pre-bid cost estimates and budgets are only as valid as the underlying production rate information. Coordination of construction activity must be based upon activity durations derived from production rates.

Production Rate Variability

In spite of the importance of accurate production rate information, construction production rates are extremely variable. Rates of production for identical activities vary considerably from project to project. A great deal a variation can even occur on the same project.

Table 1 presents a listing of production rate guidelines used by various state departments of transportation. The activity shown is the Installation of Plant Mix Asphalt Pavement. Installing asphalt pavement was chosen for this illustration because it is a well defined highway construction activity. The actual process is basically the same regardless of where it is performed.

It is interesting to note that even within a given state the predicted production rates are extremely variable. For example, New Jersey DOT uses a value of 50 to 1000 tons per day and Minnesota uses values of 1500 to 7400 tons per day. Even though these highway departments

Table 1. - DOT Production Rates for Asphaltic Pavement Installation

Source	Production Rate Guidelines (Tons/Day)
Arkansas	600
Louisiana	500 - 1000
Minnesota	1500 - 7400
New Jersey	50 - 1000
North Carolina	200 - 1500
North Dakota	600 - 2000
Oklahoma	250 - 1000
Wisconsin	500 - 1000
Wyoming	1500 - 2000
Colorado	500

Source: (Herbsman and Ellis 1988)

rely heavily on production rate predictions, they apparently have been unable to develop more exact estimates of productivity.

Research Objectives

Predicting construction production rates is often difficult. Unlike the controlled conditions found in industrial situations, the construction environment is temporary. Each project is likely to involve a unique combination of factors such as location, weather, site conditions, and other project parameters. All of these unique factors are potential modifiers of individual activity production rates. Acceptable accuracy in predicting production rates can only be achieved by taking into account all of the principal factors influencing the work activity.

The objective of this study was to develop a model building system for the prediction of highway construction production rates. To be valid, such a model must provide a mechanism for identifying influencing factors and quantifying their effect on the production rate.

It was apparent from the onset that each different construction activity might be subject to a unique set of influencing factors. Any model for predicting production rates would then have to be custom tailored to a specific activity. Therefore, research emphasis was directed towards developing a general modeling procedure rather

than a single specific model. This approach hopefully will permit a more general application of the research results.

The production rate modeling system should give consideration to several key subjects. The following are some of the areas which must be addressed:

- 1. Data Collection Techniques
- 2. Classification and Recording of Data
- 3. Data analysis and Management
- Identification and Measurement of Influencing Factors
- 5. Model Development
- 6. Model Validation

Considering the broad scope of the problem, the systems approach appears to be the correct choice. Each of these separate areas should be investigated and integrated into a complete system. The complete model building system would then be applicable to the task of predicting and analyzing production rate information in a wide range of construction situations.

Research Methodology

The basic theory which was to be explored in this study is that construction production rates can be predicted by a model which includes the principle factors.

In general, we are concerned with the following relationship:

$$P = f (F_1, F_2, ..., F_k)$$

Where P is the expected mean value of the production rate and $F_1,\ F_2,\ \cdots,\ F_k$ are the variables influencing production.

If the influencing factors can be identified and their relationship to the production rate determined, then the production rate can be predicted. Additionally, the accuracy of the prediction can be estimated using inferential statistical methods.

In order to accomplish the research objective, the investigation was organized into four phases as follows: Phase I literature survey

Initial research concentrated on acquiring a library of information developed by previous researchers and scholars. The objective was to develop a more comprehensive understanding of the problem and to begin the study with all available information. The literature survey focused on three primary areas:

- 1. Analysis of the Highway Construction Process
- 2. Construction Productivity Measurement Studies
- Statistical Analysis and Modelling Techniques.

Phase II analysis of the highway construction process

It was evident from the onset that any attempt at model building should be based upon a through understanding of the underlying process being considered. Therefore, it was essential that the model building begin with a detailed analysis of the process being considered.

Analysis of the highway construction process was focussed on developing information about several specific subjects. These areas of interest are as follows:

- 1. Basic Activities Involved in the Work Process
- 2. Types of Projects Performed
- 3. Factors Which May Influence Production
- How Highway Construction Compares to Other
 Types of Construction

Phase II statistical analysis and model development

Based upon information gained from the first two phases, statistical analysis procedures and modelling techniques were examined. A comparison of different procedures was made in order to determine the one best suited for analyzing and predicting construction productivity. A preliminary model was developed for predicting the construction production rate. Attention was given to both theoretical development and to use of advanced computational computer software such as SAS.

Phase IV model demonstration

The final research phase involved testing the statistical procedures and model with real production data. The object was to perform trials of the modelling system on a variety of highway construction situations. The experimental research data were obtained from highway construction projects throughout Florida. A total of 60 projects was sampled, which resulted in 645 production rate observations.

Testing of the model resulted in further refinement and recommendations for future research. A flow chart of the research procedure is presented as Figure 2.

State of the Art--Factorial Model Theory

The factorial model for productivity has been applied quite extensively in industrial management. Currie presented a comprehensive treatment of the subject within an industrial context (Currie 1963). Only recently, however, has the theory been applied to the construction industry.

Initial research on production rate factors in construction has been generally limited to investigating only a single factor. Weather appears to be the most popular subject. The weather effects on construction productivity have also been studied (Clapp 1966) and (Grim 1974). A study released by the National Electrical Contractor Association (NECA) in 1974 has become the industry reference for predicting the effects of temperature on construction labor productivity (National Electrical Contractors Association 1974).

However, investigations by Horner and Whitehead sought to identify all factors which had a significant effect on construction labor productivity (Horner and Whitehead 1984). The most recent and comprehensive treatment of the subject to date appears to be by Thomas (1988).

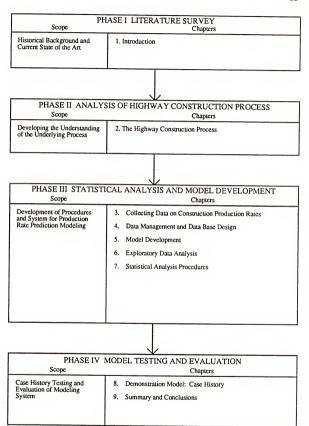


Figure 2. - Flow Chart of the Research Procedure

Thomas addresses the concept of using a factorial model to describe production rates. The research, however, was limited to dealing with the affects of weather on building construction activities. The data used consisted of production measurements obtained on three building construction projects in central Pennsylvania. All three projects were multi-story, steel frame, masonry exterior structures. A total of 78 observations of production were obtained from the three projects.

Each day the amount of production achieved was recorded as well as the temperature and relative humidity at 1:00 p.m. The production rates were reported as performance ratios, which were defined as:

Performance Ratio (PR) = <u>Actual Productivity</u> Expected Productivity

Clearly the object of the research was to establish the relationship between weather (temperature and humidity) and production rate. According to Thomas, multiple regression analysis of the data revealed the following equation:

$$PR^1 = 9.448 + 0.0518/T - 2.819 Int + 3.89 x 10^{-37} e^{H}$$

where

PR1 is the predicted daily performance ratio T is the air temperature at 1:00 pm in degrees F H is the relative humidity at 1:00 pm as a \$

This relationship is said to have resulted in a R^2 value of 0.649 and an F statistic of 17.7. The relatively high F statistic indicates that there is a statistically significant relationship between the model and the dependent variable. However, the R^2 value indicates that only about 65% of the variability was accounted for with the equation.

Thomas clearly demonstrates the validity of the factorial model concept but also indicates the need for additional research in several key areas. Obviously factors other than weather exist and should be included in the model. How do we identify and measure the effect of these factors? Which statistical analysis and linear modelling techniques are best suited for construction productivity. Thomas confirmed the need for additional research (Thomas 1987). In his paper he states,

Analysis techniques range simple to complex. A great deal of development work needs to be done in this area as well, but good quality data are need first. A comprehensive study of the literature verifies that essentially no progress has been made in any of these fundamental areas. (page 624)

Summarv

Production rates are an essential information element in the construction management process. In construction, many management decisions are based upon production rate predictions. Being able to accurately predict production rates improves management efficiency.

This research study deals with the development of a factorial modelling system for improving the accuracy of production rate predictions. Data collection, statistical analysis and model building techniques are reviewed. A preliminary model was developed and tested with extensive observational data obtained from recent construction projects.

CHAPTER 2

THE HIGHWAY CONSTRUCTION PROCESS

Introduction

Any attempt at modeling should be based upon a thorough understanding of the underlying process. One of the most common statistical traps is the confusion of correlation with causation. Preference must be given to a model which actually describes the process being considered. Therefore, it is essential that model building begin with a detailed analysis of the process being considered.

In the case of highway construction, several fundamental understandings must be developed. The basic work activity components of the construction process must be identified and described. Additionally, the relationship between activities must be defined. Finally, we need to generate a list of potential factors which will influence activity production rates.

In general, we are interested also in the similarities and dissimilarities between highway construction and the building construction process. This

knowledge will facilitate the adaptation of the modelling system to other construction categories.

The Highway Construction Work Process

The highway construction process proceeds in a linear fashion over the length of the roadway with one operation following another. The whole process consists of a relatively limited number of activities.

An interesting comparison can be made between the highway construction process and that of a manufacturing assembly line. In the manufacturing industry the product is moved from one fixed work station to another along an assembly line where the same activities are repeated over and over again at each station. The highway construction process is similar with the exception that the highway is a fixed assembly line. Therefore, the work stations (machines) must travel along the stationary assembly line.

In simple terms the highway construction process is composed of four basic operations. Figure 3 present a schematic illustration of the basic highway construction process. Table 2 provides a listing of basic highway construction work activities.

Survey. The first step is the establishment of the alignment and elevation grade of the new roadway. This is accomplished using engineering surveying procedures to transfer the design data from the engineering drawings to the existing terrain. The survey proceeds from control

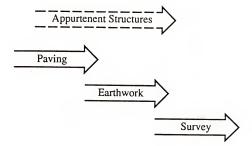


Figure 3. - Illustration of the Highway Construction Process

Table 2. - Listing of Basic Highway Construction Work Activities

Activity	Unit of Measure	
Clearing and Grubbing	Acres	
Excavation	Cubic Yards	
Stabilizing	Square Yards	
Base Construction	Square Yards	
Surface Treatment	Cubic Yards	
Concrete Pavement	Cubic Yards	
Milling	Square Yards	
Plant Mix Asphalt	Tons	
Storm Sewers	Lineal Foot	
Gurband Gutters	Lineal Foot	
Sidewalk	Square Yards	
Sod	Square Yards	
Guardrails	Lineal Foot	

reference points and results in a series of grade states. It is these layout states which serve as position controls for the construction process.

Earthwork. The heart of highway construction is the earthwork activity. This consist of reworking the existing terrain to conform to the alignment and grade required for the new road. Excess earth material is excavated and then transported along the roadway to an area requiring fill or for waste at preselected locations.

Excavation, hauling and dumping is typically accomplished with large earth moving equipment.

Excavation is frequently performed by an excavating-hauling unit called a scraper. The scraper consist of a tractor which pulls a load carrying called a bowl. The bottom of the bowl contains a blade which shaves off the existing earth. As the unit moves forward, the earth is forced up into the bowl. The operator riding in the tractor attempts to maintain a constant loading speed by varying the depth of cut. The bowl and the blade are raised and lowered to change the depth of cut. When full the scraper hauls material to the fill area where the earth is dumped out the back of the bowl.

Installation of earth fill consists of spreading the material by a dozer tractor or motor grader and stabilizing the material by compaction. As the cut or the fill approaches the required elevation, a work process called grading begins.

Grading is the process of bringing the earth road bed to the design finish elevation. Grading requires a skilled motor grader operator who must control the grader blade in order to achieve the required surface elevation within a strict tolerance. The grader operator works to grade stakes or "bluetops" which are placed in the roadway with the top of the stake set at the desired finish grade elevation of earth.

Paving operations. The pavement surface of the roadway is composed of either portland cement concrete or asphaltic concrete. Both materials are usually plant mixed and transported to the point of application. The actual installation process of both materials is similar. Both asphaltic pavement and concrete pavement are spread over the road surface by a paving machine. These paving machines receive the plant mix material from the transport unit and spread the material over the roadway as the machine travel along. With both the asphalt and the concrete pavers the operator must be skillful in maintaining the correct pavement thickness and smoothness.

Appurtenant structures. In addition to the roadway construction, highway projects commonly include the construction of appurtenant structures such as bridges, culverts, barricades and drainage systems. The construction of these appurtenant structures in generally undertaken as a distinct work process which must tie in to the work schedule established for the roadway work. Many

of the structures more closely resemble the work process used in building construction than that of highway construction.

Factors Effecting the Work Process

Classification of Factors

The number of different factors which may effect construction production rates is very large. This is a result of the dynamic nature of the construction process. Generally each product (or project) is unique and is produced in a different location. The set of potential influencing factors may be different for each project considered. Therefore, developing a basis for analysis can be difficult.

Consequently, a system for classifying factors is needed. The following system (Herbsman and Ellis 1989) provides a mechanism for rationally organizing influencing factors. Factors which may effect production rates are designated as Construction Production Influence Factors (CPIFs). For classification purposes, the CPIF's can be separated into three distinct groupings as follows:

- 1. Project Factors
- 2. Site Factors
- 3. Organization Factors

Project factors are influencing factors which are directly related to the particular product which is to be constructed. This would include project parameters such

as the type of construction, size of the project, specifications, and construction details. These projects factors would be valid for a specific project regardless of the choice of site or construction organization.

Site factors are derived from physical conditions of the site at which the project will be built. Site factors might include items such as the geographic location, type of earth, weather, local traffic conditions and adjacent land use. These site factors are unique for a specific site and are valid for any project which might be considered at that site.

Organizational factors are the influencing factors resulting from the organizations involved in the construction process. This includes all relevant parties such as the owner, construction manager, inspecting authority and builder. Significant organizational factors might include the level of skill of the workmen, supervisory skill, degree of inspection, safety and managerial expertise. These are factors which primarily are related only to the people side of the process.

It is important to note that each of the three different classes of influencing factors is not necessarily independent of the other two. This means that the effect on production of one class of influencing factors may depend upon the existence of other influencing factors of another class. For example, the effect on activity production rate resulting from any of the site

factors may be directly related to the type of project to be constructed.

The statistical importance of this interaction between factors will be discussed further in Chapter 7 which covers statistical analysis procedures.

The classification of factors assists in the identification of CPIFs and in the management of CPIF data. An exact determination of classification is not absolutely necessary. For instance, certain factors relating to project site layout might originate from the physical limitations of the specific site, or from the builders plan for site layout, or might be dictated by the particular project.

Figure 4 presents a schematic diagram showing a CPIF classification system.

Relating CPIFs to Work Activities

Matching potential CPIFs to specific work activities is an essential prerequisite to predicting activity production rates. Identifying potential influencing factors requires a careful and objective analysis of the particular work activity being considered. The most desirable approach involves input from those persons directly involved in the work process. The project superintendent, crew foreman and machine operator should all contribute to the development of the list of potential influencing factors. A systematic approach will produce the best results.

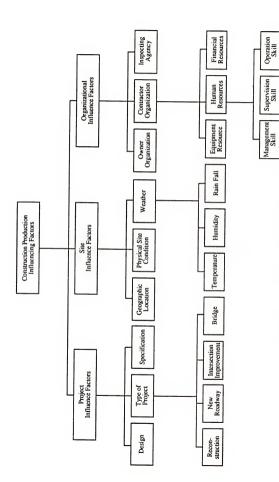


Figure 4. - Schematic Diagram of a CPIF Classification System

The most effective method appears to be for the researcher to interview the participants using a checklist. The checklist provides a standard format for soliciting input. Figure 5 presents an example of a CPIF checklist. After obtaining input from the work participant, the researcher then develops a preliminary list of influencing factors. This list of factors will be used in designing the production rate data collection procedure and in model formulation.

Comparison of Highway Construction with Building Construction

It should be noted that the highway construction process differs considerably from that of traditional building construction. Highway projects generally involve only a relatively small number of basic work activities. Each of these activities is changed very little from project to project.

Building construction on the other hand, generally involves a much larger number of distinct work activities. The scope of construction specialties required for a typical building project today far exceeds that of a road project. Except in certain cases where the same structure is being repeated each building construction project requires a customized approach to its basic work activities.

Highway construction is also more of a linear process. Highway construction proceeds along the roadway

Constr	ruction Production Rate Influen	icing Factor
	CHECK LIST	
Activity No.:		Date:
Activity:		
Project	Site Factors	Organization Factors
Project Type	Location	Inspection
Specifications	Layout	Supervision
Materials	Adjacent Area	Operator Skill
Size	Weather Weather	Equipment
		<u> </u>

Figure 5. - Example of CPIF Checklist

from beginning to end. In certain cases, vertical building construction might be considered a linear progression, but for the most part building construction is a complex sequence of interdependent activities.

The concept of influencing factors applies equally to both building construction and highway construction.

However, the complexity of the building construction process makes the production rate modelling system more complex. The simplicity and standardization of the highway construction process facilitate development of the production rate modelling system.

These characteristics of highway construction (limited number of uniform activities) facilities the study of factors effecting production rates. Uniformity in the work activity is essential in acquiring an adequate research data base for analysis. If the work activity remains unchanged from project to project, correlation of the production rate observation is possible.

Summarv

Highway construction process involves four fundamental operations:

- Surveying
- Earthwork
- Paving
- Constructing Appurtenant Structures

The process consist of a relatively small number of basic work activities which are repeated in a linear fashion.

Understanding this process is an important part of the model building procedure.

A variety of factors may effect the highway construction work activities. These Construction Production Influencing Factors (CPIFs) can be classified into three main groups.

- 1. Project Factors
- 2. Site Factors
- 3. Organizational Factors

Classification assists in identification and in data management.

Identification of potential CPIFs involves input from the participants in the work process. Final verification of the significance of potential CPIFs is based upon statistical analysis of the production rate observation data.

CHAPTER 3

COLLECTING DATA ON CONSTRUCTION PRODUCTION RATES

Introduction

Production rate measurement and recording is an essential prerequisite to the development of a prediction model. Accurate and timely data are required. The structure of the model and its predictions of future production rates are based upon historical production rate data. The validity of the model and the accuracy of predictions are directly dependent upon the quality of the input data. Incomplete and erroneous data will produce unsatisfactory results. Therefore, careful consideration must be given to the many issues associated with the collection of production rate data.

Certainly there are several fundamental issues which must be decided. How are the production rates to be measured? Which activities should be observed? What form of sampling program should be used? Each of these issues will be addressed in this chapter with respect to the development of the production rate prediction model.

General Requirements for the Measuring System Criteria

The following criteria are suggested for a meaningful measurement system (Bain 1982):

- Validity
- 2. Completeness
- 3. Comparability
- 4. Inclusiveness
- 5. Timeliness
- Cost-effectiveness

These criteria were derived in an industrial context but they apply equally well to construction. They provide useful guidelines for evaluating and selecting production rate measuring procedures.

 $\underline{\text{Validity}}$. Validity measures of production rates indicate actual changes in the ability production rate. The choice of units of measure may result in validity problems.

For example, consider the measurement of the production rate for the installation of concrete pavement as shown in Table 3. If production is measured in units of square yards, data indicating differences in production rates may be misleading. Pavement with significant differences in thickness would have been grouped together. The unit of measure (square yards) is not a good choice for concrete pavement. A unit which more accurately represents the work effort would be volume or cubic yards.

Table 3. - Comparison of Production Rate Units of Measure

Project	Average Production SY	Rate per Day
A	2790	620
В	3870	430
С	3420	570

Completeness. Meaningful measures of production rates must take into account all significant factors which effect the work activity. Comparing asphalt pavement production rates for a project located in an urban, highly congested area with that of a project located in a rural area is meaningful only if the environmental factors are identified. The measurement and reporting process must also include the influence factors associated with the work produced.

The identification and qualification of CPIFs provides a basis for comparison of activity production rates.

Comparability. Much of the value obtained from production rate measurement results from comparison. We would like to compare current production rates with past values. We might want to compare production rates achieved on one type of project with the rates on another type of project. Also, after having made a particular management decision, we would like to compare the new production rates with the previous rates.

Standardization of the data collection techniques is mandatory, if valid comparisons are to be made. Thomas also expressed this opinion (Thomas 1987):

Standardized data collection is needed to ensure consistency. Ways of combining data from different projects need to be found because reliable analyses cannot be done using 30-60 data points, as may be the case if data from only one project were used.

Each organization must develop a standard procedure for production rate data collection. The method of collection, measurement and recording must be uniform. ONly then can valid comparisons be made over the entire data base.

Comparability of the data is enhanced by the inclusion of factorial data in the production rate collection system.

Consider production rate data for the work activity of general excavation. Production rate observations obtained from two projects with differing working conditions can be compared only if information concerning the appropriate CPIF's is also known.

For example, Table 4 presents production rate observation data for general excavation. The mean production rate for Project A is 1167 cy/day. The mean for Project B is 780 cy/day. It is not possible to make an informed managerial interpretation without the factorial data. In this case, given the relevant CPIF data, we would suspect that the difference in the means values is the result of the three days of rain which occurred on Project B.

<u>Inclusiveness</u>. The production rate modeling system should include work activities which contribute significant information used by management in obtaining organizational goals. Most likely the cost of data collection and analysis will preclude including all

Table 4. - Example of Production Rate Data Comparability

	F5 Crew Total Quantity (Range)	S-28 4											
Influence Factors	F3 Project Type	NC	NC	NO	NC	Ç.							
Inf	Rain	NO	NO	ON	ON	ON	ON	YES	YES	YES	ON	NO	
	F1 Material Type	SC	00										
Excavation	Production Rate cy/day	1120	1240	1090	1150	1120	1280	520	410	380	950	1240	1185
	Project	A	A	A	A	A	A	ш	В	ф	т	Ą	A
	Obs. No.	н	2	3	4	r,	9	7	8	6	10	11	12

activities. Therefore, a decision must be made as to which activities to include. Selection criteria should be developed for prioritizing work activities.

Assigning a rank in accordance with the activities importance to the organization appears to be a logical first step in the selection process. The number of activities to be measured would ultimately be based upon budgetary considerations.

Timeliness. Timeliness is an essential criteria for all managerial information. The production rate measuring system should provide information which is as current as practical. Timely measures of organizational performance are essential for improving productivity. Post completion evaluations may be useful for planning future projects but they are of no value for the project just completed.

This means that for most construction applications the timing of the data collection-analysis-reporting cycle should be a matter of days not weeks. The normal monthly accounting period is probably too long a turn around time. Mangers who have the primary responsibility for project planning and scheduling will require at least weekly production rate updates. Managers in a more passive role such as owner's representatives, may be satisfied with monthly updates.

<u>Cost-Effectiveness</u>. Collecting data on production rates should be based upon overall cost-effectiveness just as with any other management information system. The

degree of detail and the number of activities to be included in the system must be decided by each organization. Each participant in the construction process will have different requirements for production rate information. Therefore, the production rate modeling system is expected to be adjusted by each user to the organizational needs.

Measuring and Reporting Completed Work

General Considerations

The method of measurement and the reporting documentation are most effective when matched to the project and organizational situation. A number of possible measuring techniques exist. Each has advantages and disadvantages. The following three different methods are available for measuring completed work (Thomas and Kramer 1988):

- 1. Units Completed
- Percent Completed
- 3. Level of Effort

Each of these methods will be discussed in the following sections.

United Completed

Actually counting or measuring the quantity of work accomplished is the most direct method of measurement. Physically measuring or counting the completed work can be the simplest approach.

For the most part, highway construction work activities are compatible with this form of measurement. We can determine by direct measurement or count how much of each work activity has been accomplished. For example, the number of cubic yards of pavement installed can be determined from actual measurement. The number of drainage inlets installed can be actually counted.

Measuring the units completed provides an accurate, simple method of measurement. However, there are a few disadvantages. First, actually measuring work quantities on the project site can be time consuming and costly. Secondly, for certain items physical measurement may not be readily obtainable. Some of the appurtenant work on highway projects more closely resembles building construction. Work activities are likely to be partially completed.

For example, consider a concrete bridge deck. A significant amount of preparatory work must be accomplished prior to the final placement of concrete. If we count only completed work units, the work effort involved in forming and reinforcing will not be considered until the deck is complete.

The units completed method may not be appropriate for activities which involve several subtasks.

Percent Complete

The percent complete method consist of a subjective opinion. Usually the job superintendent and the owner's representative agree on how much of the particular activity has been accomplished.

This method is useful with some activities which may be difficult to measure. However, the accuracy of the technique is obviously dependent upon the judgement of the measurer.

Level of Effort

One way to make the percent complete method more objective, is too divide the work activity into its subtasks. Each subtask is then pre-assigned a portion of the overall work effort. This weighing of the subtask is sometimes called a rule of credit. For example, the concrete bridge deck previously mentioned might be subdivided into the following levels of effort.

Work activity: concrete bridge deck

Subtask	Rules of Credit
Formwork	0.50
Reinforcement	0.15
Concrete Placement	0.25
Form Removal	0.10

In this case, as each subtask is completed its portion of the overall activity may be counted. The advantage of the level of effort procedure is that it provides greater accuracy and objectivity in the measurement of work activities which are difficult to measure (Thomas and Kramer 1988).

Choosing the Appropriate Method

Each of the measurement options have advantages and disadvantages. Selection should be made with consideration for the characteristics of the particular activity. However, it is essential that the measuring procedure reflect what has actually occurred at the project site. Table 5. presents a summary of the measurement methods with advantages and disadvantages.

Reporting the Data

Daily Reports

Reporting production rate data on a daily basis is an option available to the contractor. The daily submission of time reports and equipment usage reports is routine. The reporting of completed work quantities could be conveniently combined with the organization's standard daily reporting documentation.

The advantage of daily reporting is the level of detail provided and the timeliness of the information.

The disadvantage is that measuring and reporting requires supervisory time and performing this function daily may be too costly to justify.

Table 5. - Methods of Quantity Measurement

Method	Criteria	Advantages	Disadvantages
Units Completed	Well-defined scope	Most detailed and accurate Cost of data collection	Cost of data collection
	Output determined quickly by counting or elementary math	Does not rely on subjective opinions or evaluations	
	Relatively few subtasks	Claimed output can be	
	Short duration for completing each unit of output	readily verified	
	Single craft or trade		
Percent Complete	Relatively minor tasks where reasonably accurate estimates can be made	Simple Inexpensive Quick	Can be very inaccurate and misleading
Level of Effort	Activities involving overlapping subtasks	Greater detail and objectivity than simply esti-	More involved than simply
	Subtasks must be measurable or their status easily defined	mating how much work was done and less expensive than counting or measuring the units completed	estimating the percent complete
	Best suited where there is a large number of similar commodity items, and the work will be ongoing for an extended pariod of time		

Source: (Thomas and Kramer; 1988)

Monthly Reporting

Another option is to report production rate information as a part of the normal payment estimate process. Highway construction projects are typically bid and paid on the basis of unit prices. Calculation of the monthly payment estimate involves a determination of the quantities of work accomplished. If the time spent working on the work activities can be verified also, the production rate information should be available from the data worked up for payment estimates.

The use of a CPM type project schedule with the updating of actual start and finish dates also would provide a means of reporting time spent. Some consideration must, however, be given to insuring compatibility between the activities selected for production rate modeling and those activities making up the payment and scheduling systems.

Figure 6 presents an example of a monthly payment estimate/production rate report.

The advantage of monthly reporting is that it is less costly. However, information is less timely.

		Pay Esti	mate/Product	ion Rate Report		
•	desurface I-75 10005-IA-002			eriod Ending: 30		
Activity No.	Activity Description	Unit	Total Quantity	Completed This Period	Days Worked	Comments
2105	Milling	SY	320000	27150	18	
2211	Asphalt Pavement	Tons	75000	5600	8	3 Days Rain

		_				
2504	Guardrail	LF	6000	2100	12	

Figure 6. - Example Monthly Pay Estimate/Production Rate Report

Sampling Considerations

Activity Selection

Measuring and analyzing production rates for all activities will probably be too costly for most organizations. Therefore, a selection criteria should be developed for choosing those activities which are to be measured. The selection criteria should be based upon the objectives and goals of the organization.

Establishing a priority ranking for each activity can be done based upon the following criteria:

- 1. Amount of Work
- 2. Critical Path

The amount of work refers to the proportion of work performed by the organization which is represented by the activity. For example, asphalt pavement may represent 10.2% of the organization's total annual volume. Storm drainage may represent only 1.2% of the total effort. Each activity is graded based upon historical records.

The second criteria pertains to the activity's occurrence on project critical paths. Some activities may represent only a small percentage of the total work effort but still be significant because of their impact on project scheduling. Therefore, these critical scheduling activities may also be important candidates for production rate modeling.

Each activity can be assigned a priority ranking derived from a priority weighing system. The equation for calculation the ranking can be expressed as

where

A = activity ranking

Ww = weight assigned to work percentage

P = activity's percentage of the total work

Wc = weight assigned to critical path

N = frequency of occurrence on critical path

Activities are submitted to the production rate modeling system on the basis of their ranking or A value. The total number of activities to be handled by the system is determined by management generally on the basis of cost.

Randomization

In an ideal situation we would like to collect all production rate data for any activity of interest. Having a complete historical data base provides the strongest possible input for the prediction model.

Economics, however, may preclude the collection of all production rate data. In this case, we can make predictions concerning future production rates by using a sample of the total work.

Suppose that the production rate modeling system is being developed by a state highway department. During any

given year hundreds of projects are performed throughout the state. It is not possible to make observations on all projects. Therefore, only a small number of projects will be observed. The selection of projects should be made randomly.

That is, each project should have an equal chance of being selected. If we do not insure randomization, we can not insure the validity of our inferences about the data analysis.

Selecting a project because it is of particular interest may serve management's immediate needs, but will also introduce challenges to the sampling system's validity. If conclusions are to be made concerning the entire population of projects from a sample of projects, then the sample must be randomly selected.

The assumption of randomization is a fundamental prerequisite to the statistical analysis and regression procedures used in the evaluation of the production rate data. Analysis procedures will be discussed further in Chapter 7.

Sample Size

How many sample observations should be made? This very practical question must be confronted by each user of the prediction model. Making observations and analyzing the data cost money. In general we would like to work

with the smallest sample size which will still produce acceptable prediction model results.

Logically, we might expect that larger samples would more closely match the overall population. Further, we might suppose that our <u>prediction</u> ability to predict the populations statistical parameters from a sample would depend also upon the variability of the values.

It turns out that the number of sample observations required is determined by two factors: variability of the population values, and the desired prediction accuracy. The sample size required may be estimated by the following equation (Scheaffer 1986, 237):

$$n = \begin{bmatrix} \frac{Z}{\alpha/2} & \sigma \\ \frac{---}{\beta} \end{bmatrix}$$

where

n = number of sample observations required
z = a standardize normally distributed
 variable which is a function of

variable which is a function of probability. (values of z are commonly given in statistical tables for normal probability distributions.)

 α = rejection region chosen for the z value

 σ = variance

 β = desired prediction confidence interval

For example, suppose we are interested in predicting the daily production rate for the highway construction activity, Asphalt Pavement Installation. We would like our prediction to be within 100 tons/day of the actual value. Furthermore, we do not want to encounter an

actual value which is outside of our 100 ton/day confidence interval more than 10 percent of the time. From past historical data or perhaps we have done some preliminary test, we estimate the variance to be 22500 tons 2 /day 2 .

Therefore, the values for the sample size equation are

z.05 = 1.645

 $\sigma = 150 \text{ tons/day}$

 $\beta = 100 \text{ tons/day}$

It follows that

$$n = \left[\frac{1.645 * 150}{100}\right]^2 = 24.35$$

In this example, 25 observations must be obtained to obtain the desired results.

It is important to note that the preceding estimate of sample size is based upon the assumption that the production rate values are normally distributed about the mean. However, with construction production rates we have reason to believe that the frequency distribution of the values is not normally distributed. In fact, the frequency distributions of production rate observations appear to be skewed to the right of the mean.

Therefore, our estimate is not as precise as it would be if the assumption of normality was valid. The issue of normality will be discussed further in Chapter 7.

Summary

The systems used for collection of production rate information are important to the success of the production rate prediction model. Observations of actual production rates and corresponding factorial measurements are the input data used by the model to generate production rate predictions. The accuracy of the model's predictions and its cost effectiveness depend directly upon the data collection system.

In general, the production rate measurement system should conform to the following criteria:

- 1. Validity
- 2. Completeness
- 3. Comparability
- 4. Inclusiveness
- 4. Timeliness
- Timeliness
- 6. Cost Effectiveness

The method selected for measuring the production rate should be selected after considering these criteria.

Three measuring techniques which are appropriate for production rates are:

- 1. Units Complete
- 2. Percent Complete
- 3. Level of Effort

The number of observations which should be obtained is a function of the desired prediction accuracy, data

variability and the number of factors considered.

Selection of which activities to include in the model can be made on the basis of relative significance to organizational objectives.

Data management and storage considerations will be reviewed in the next chapter.

CHAPTER 4

DATA MANAGEMENT AND DATA BASE DESIGN

Introduction

Data management and storage are important considerations for the construction production rate model. The production rate model will deal with substantial amounts of data. The efficiency and utility of the model will largely depend upon the design of the data management and storage systems.

This chapter will cover data management concepts as they apply to production rate data. The structure of the data base will be discussed. Also, the concept of integrating the production rate model within the organization's management information system will be presented.

Data Base Structure

A data base is simply the logical arrangement of information. Usually, the following conventions are used in describing the elements in the data base structure (Stair 1984):

Characters - the smallest single component, either alpha, numeric or special

Fact - assembled from characters, facts are words or numbers

Record - a collection of related facts

File - a collection of related records

With regard to the production rate observational data, facts are the observed production rates and the CPIFs. A record would consist of all facts relating to a single observation. A data file might consist of all observations of a specific activity. An illustration of this arrangement is given in Figure 7.

Although there are several possible logical arrangements of data elements, a relational data base structure is best for production rate data. The relational data base structure relates data in a tabular form. In its simplest form the relational data base model organizes data into a two dimensional table. Each row of the table is a record of information. Each column represents a specific class of facts.

The relational data base structure allows efficient access to the information in the form of data queries. Suppose, for example, we wish to review all of our production rate observations taken from a specific type of project. A query to the data base is made after stipulating the selection criteria. The resulting report

Observation Number Rate (Cys) Work (Range) (Range) Project (Range) Project (Range) Weather (Type (Range)) Materia (Type (Range)) A Record 3 600 032487 2 NC 3 F SC A Record 3 600 032487 2 RC 2 R SC 5 928 052687 3 RC 2 F SC 6 1871 052687 3 RC 3 F SC 7 1924 071487 4 NC 4 F SC 8 1785 071787 3 NC 4 F S 9 1110 090887 2 RC 1 F S 10 1002 091187 2 RC 1 F S 11 425 092487 1 1 5 F SC 12 7 1 1 7 <th></th> <th></th> <th></th> <th></th> <th>rentify: 02469 Ceneral Excavation</th> <th>OCILCIAI</th> <th>Excavation</th> <th></th> <th></th> <th></th>					rentify: 02469 Ceneral Excavation	OCILCIAI	Excavation			
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1229 100587 3 RC 2 F		11	425	092487	-	1	5	п	SC	Г
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A File —

Figure 7. - Illustration of the Basic Data Structure for Production Rate Observations

is a list of all observations made from the specified type of project.

The relational data base structure also allows for efficient statistical analysis of the data. Statistical and regression procedures which will be used to produce production rate predictions require a relational data organization.

Data Base Management Systems

The Data Base Management System is the software used to store and access the data. Access to the data base may be made directly through the DBMS or through an application program. In general, all data storage, retrieval and manipulation is controlled by the DBMS. Figure 8 presents a schematic illustration of the function of a DBMS.

Observational data records are entered into the data base usually through menu driven DBMS software. The production rate prediction model accesses the observational data through the DBMS. Production rate analysis and prediction data generated by the model are also stored in the data base. Each organization is likely to custom tailor the distribution of production rate information reports on the basis of its particular needs.

Many data base management systems are available on the commercial market. These software packages can be provided for the microcomputer, mini computer and

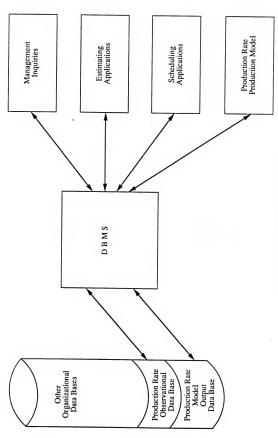


Figure 8. - Schematic Illustration of the DBMS

mainframe environments. Hardware is usually not a prime consideration. However, since the DBMS and production rate prediction model may not be part of the same application package, software compatibility is essential.

Use of a central data base has several advantages. The various functional users of the data have efficient access to the core of organizational information.

Centralization also prevents redundancy of data storage. Information is input and stored only once.

In spite of these advantages, many organizations in the construction industry do not use a centralized DBMS. Data storage and management is frequently organized by function. Each functional segment operates with its own application software and data storage. The resulting organizational arrangement can be described as a matrix. Figure 9 presents a schematic illustration of a typical matrix data storage organization.

The production rate prediction model can be designed to operate in a matrix type organizational environment. In this case, the production rate data and modeling application software are operated as a separate function within the organization.

Summary

The storage and management of production rate data are important to the efficient use of the production rate prediction model. Large quantities of observational data

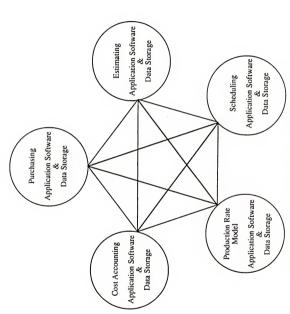


Figure 9. - Schematic Illustration of a Matrix Data Base Arrangement

must be stored and accessed. A relational data storage system is best suited for product rate data. Each record in the data base consists of a single observation of production.

A centralized data storage arrangement which is managed by DBMS software appears to be most desirable. However, the production rate modeling system can operate as a separate functional unit.

CHAPTER 5

MODEL DEVELOPMENT

Introduction

Modeling is a technique for defining and explaining relationships among various sets of variables. Usually, there will exist a dependent variable of interest which the model attempts to explain in terms of independent variables. In the case of construction production rates, we want to explain production rates as a function of various influencing factors. Additionally, we would like to predict future production rates, given a specific set of influencing factors.

The previous chapters have included a discussion of data collection and data base management considerations. The next step in the design of the production rate modeling system is the development of the model. Details of the statistical tools used in model design will be covered in the next chapters. There are, however, several general modeling concepts which should be explained prior to undertaking formal statistical procedures.

This chapter will present the basics of modeling theory and discuss various approaches to model construction. In addition, a few of the most common pitfalls will be noted.

Modeling Theory

Modeling is an attempt to describe an actual process in terms of input and outcome. Figure 10 illustrates a typical process. There will exist certain input variable or conditions and there will exist an outcome or result.

Usually, we are interested specifically in the outcome.

Therefore, modeling begins with an examination of the process to be modeled. This examination will produce three fundamental elements (Box, Hunter and Hunter 1978):

- 1. Indentification of the input variables
- 2. Indentification of the resultant variables
- 3. Formulation of the relationship among variables.

 Often many possible models might be formulated. However, the researcher will choose trial models which are considered to be plausible based upon knowledge of the process of interest.

Deterministic and Probablistic Models

Deterministic models hypothesize an exact relationship between variables. Many examples of deterministic models exist in science and engineering. Ohms law is a classic example of a deterministic model. The relationship between current, voltage and resistance is exactly defined by the model.

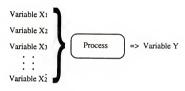


Figure 10. - Illustration of a Process to be Modelled

However, many real life processes can not be adequately modeled by deterministic models. We find that there will often exist a random error component. Therefore, a probablistic model will provide the best description of actual processes. In practice, the probablistic model consists of a deterministic component and a probablistic component. A typical probablistic model might be described as follows:

Outcome = Determinist Component + Probablistic component
The probablistic component of the model accounts for random
errors which cause variation in the expected outcome. Also,
in most cases, we realize that there may be unknown variables
effecting the outcome. The variation causes by unidentified
variables is included in the probablistic component.

Causation and Correlation

The distinction between causation and correlation is absolutely necessary. Correlation between variables can be used for predictions. However, correlation provides little information about the process. If we wish to optimize or change the process, we need to be concerned with causation.

Box and Hunter prodive a very good example of the difference between correlation and causation (Box and Hunter 1978). This example concerns the population statistics for Oldenburg, a European town famous for the storks which nest on the roofs of the houses. Scientific observations over a seven year period clearly showed a correlation between the

population of the town and the number of storks. As the number of storks increase so did the number of babies.

Correlation clearly existed. However, it is unlikely that the increase in storks caused the increase in babies.

In fact, we often find that two variables, X and Y, are correlated because of their direct relationship with a third variable, Z. Knowing only X and Y, we can make predictions about the change in one with respect to the other. However, we can not identify the cause behind the relationship unless we identify the third variable.

In the Oldenburg example, the third variable is obviously time. Both the number of storks and babies were directly related to the passage of time over the seven year period.

Modeling Procedure

Modeling is an iterative process. First, a preliminary model is hypothesized based upon examination of the process. The model is then tested for adequacy. Modifications are made and the revise model is tested once more. The procedure is rather continuous. Figure 11 presents a schematic illustration of the modeling procedure.

The objective or goal of the model should be stated clearly at the start of the process. Each iteration of the modeling procedure should bring the model closer to the objective. If the objective is to make predictions about a dependent variable, then correlation is the central issue.

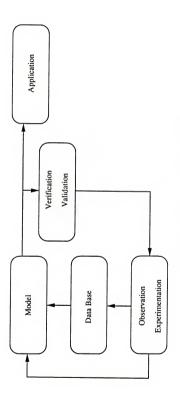


Figure 11. - Schematic Diagram of the Modeling Process

Variables may be included in the model on the basis of their correlation with the dependent variable.

If on the other hand, we are primarily interested in producing a model which reflects the actual process, then causation is the determining criteria. A model will be developed on the basis of how well it reflects the underlying relationships whether or not the predictive precision is optimized.

Another consideration in model development is that independent variables are sometimes not independent. That is, they are related to each other. Using independent variables which are correlated will cause problems with model precision. Therefore, model formulation should attempt to avoid the use of highly correlated independent variables.

Summary

The modeling process involves recognition of the various factors or variables which are involved. Based upon an examination of the experimental data and knowledge about the process, an attempt is made to describe the process in terms of the identified factors. The trial model is tested for adequacy and revisions are made until the model is judged successful.

Care must be taken to avoid non-independent variables.

Also, the distinction between causation and correlation should be clearly understood.

CHAPTER 6

EXPLORATORY DATA ANALYSIS

Introduction

Exploratory Data Analysis (EDA) is a relatively new area of applied statistical analysis. John Tukey's book in 1977, Exploratory Data Analysis, presented the first comprehensive treatment of the subject (Velleman and Hoaglin 1981). The objective of EDA is to improve the efficiency of the research process. EDA procedures allow the researcher to detect features in the data which may be unnoticed in traditional analytical techniques. EDA is particularly useful in model development by visually revealing the behavior of the data.

In general, EDA procedures concentrate on the following three analytical techniques:

- Visual Displays revealing the nature of the data.
- Residuals analysis of the lack of fit between the model and the data.
- Resistance protecting the model from the influence of outliers.

This chapter will present several EDA techniques which are particularly appropriate for evaluating construction production rate data. A thorough examination of the data coupled with a complete understanding of the underlying process provides the most successful approach to model development. Correctly applied EDA will assist in matching the mathematical model to the true process.

Stem and Leaf Plots

Stem and leaf plotting is a technique for visually displaying the data. Data points are laid out according to certain stem and leaf rules to form a picture of what the batch of data looks like.

Examination of the data display can provide important insight into the overall data pattern. The stem and leaf visual display may provide the following information (Velleman and Hoaglin 1981):

- 1. What the range of data values are.
- 2. Where most of the values are concentrated.
- 3. What the shape of the data distribution is.
- 4. Whether there are gaps where no values exist.
- 5. Whether or not there are outlying values.

This preliminary information can greatly assist the researcher in getting acquainted with the research data.

Stem and leaf plots are constructed by ordering the data values in accordance with their digits. Each value is split into leading digits called stems and trailing digits called leafs. For example, a data value such as 63128 might be divided into stem and leafs as follows:

Stem Leafs 63 1

Note that only the first digit of the trailing digits is used to represent the leaf portion. The choice of where to split the data value depends upon the range and distribution of the values. The idea is to plot the data points over a range which best depicts the behavior of the data.

For example, Figure 12 is a stem and leaf display for the data given in Table 6. The data consist of construction production rate observations of structural steel erection. The values represent daily production expressed as a ratio of expected production. The research data were collected from three commercial building project sites in Pennsylvania.

In Figure 12, the stem and leaf display has been constructed by using the first digit of the value as the stem. The first digit of the trailing digits then becomes the leaf. Within the range of data values, all possible stems are listed whether or not values actually occurred. Each value is then added to the display by adding its leaf to the appropriate stem.

We can see from stem and leaf plot that the concentration of data values appears at the 0 and 1 stems. Sometimes it is helpful to spread out the plot in order to obtain a wider display of the data. This can be done by

Table 6. - Production Rate Data for Steel Errection

No.	Calendar Date	Activity	Performance Ratio	Temperature (°F)	Relative Humidity (%)
1	February 05	Steel	0.79	41.3	71
2	February 06	Steel	0.65	33,1	95
m	February 10	Stee1	0.80	27.9	67
4	February 11	Steel	1.95	28.8	73
2	February 12	Steel	0.64	28.5	29
9	February 13	Steel	1.01	24.1	64
7	February 14	Steel	1.33	17.0	09
8	February 20	Steel	0.94	37.0	75
6	February 24	Steel	0.77	32.3	56
10	February 25	Steel	1.49	26.6	40
11	February 26	Steel	0.62	30.2	5.4
12	February 27	Steel	1.94	27.3	59
13	February 28	Steel	0.81	29.5	54
14	March 03	Steel	1.18	37.7	44
15	March 04	Steel	5.13	20.3	85
16	March 05	Steel	0.62	38.5	7.0
17	March 06	Stcel	1.34	30.8	80
18	March 07	Steel	4.30	11.6	47
19	March 10	Steel	2.40	52.0	40
20	March 11	Steel	3.25	36.4	63
21	March 12	Steel	3.30	36.5	09
22	March 13	Steel	1.56	37.0	8.1
23	March 14	Steel	1.55	40.8	. 80
24	March 17	Steel	2.27	37,3	22.8
25	March 18	Steel	1.56	45.0	94

Stems	Leaves
0	76869686
1	90374913555
2	4 2
3	2 3
4	3
5	1

Figure 12. - Stem and Leaf Display of the Data from Table 6.

using multiple lines per stem. Each stem value is listed on two consecutive lines. Leaf values from 0 to 4 are posted to the first line. Leaf values from 5 to 9 are posted to the second line.

Figure 13 is a stem and leaf display of the same data used in Figure 12, however, multiple lines have been used. In this case, the display reveals more detail concerning the data distribution.

Figure 13 also contains a depth value which has been added to the left of the stem column. The depth number represents the number of values which lie either on that line or on a line closer to the nearest end of the data distribution. Usually, the middle line shows, as a depth value, the number of values listed on that line in parentheses. If the plot contains an even number of data lines, no middle line exists. In this case, the depth values on either side of the middle are listed in the usual manner.

The stem and leaf plots closely resemble another commonly used display technique called the frequency histogram. In the histogram, data values are represented by equal spaces on bars. The bars are plotted together in a graph which depicts the shape of the data distribution.

Histograms do not provide information about the individual data value. The stem and leaf plot uses the actual data values to construct the display. Therefore, the researcher has immediate access to the data.

1 9 represents 1.9					
	0				
9	0	768697686			
14	1	03413			
19	1	99555			
21	2	4 2			
	2				
4	3	2 3			
	3				
2	4	3			
	4				
1	5	1			
	5				

Unit = 1.0

Figure 13. - Stem and Leaf Display of the Data from Table 6 Using Multiple Lines.

Nevertheless, histograms are useful when the data batch contains a large number of observations. When, for instance, several hundred values are involved, the stem and leaf display provides a level of detail which would be difficult to analyze. The histograms are a better choice for displaying large data samples.

For the data given in Table 6, Exploratory Data Analysis using stem and leaf displays provides a great deal of useful information about the data. We see that the data values are generally concentrated in the range of 0.5 to 1.9, which includes 19 of the 25 observations. The range of 0.5 to 0.9 contains the largest number of values. The data is skewed to the right with the tail stretching to a high value of 5.1. The higher values are more spread out than the lower values.

Boxplots

The boxplot is another important EDA tool. The boxplot is a graphical technique which is particularly useful in examining the tails of the data distribution. Often it is the data values which are spread out significantly from the center which are of most interest. We would like to understand what circumstances and what factors resulted in the large variance from the mean.

The concept of depth is important to the development of the boxplot technique. If the data values are arranged in an ordered sort from lowest to highest, the depth of each data value will be how far it is from the closest end of the batch. The central most values have the greatest depths. The lowest depths occur at the extremes.

The boxplot graph is constructed after determining certain key data characteristics. These descriptive characteristics are listed as follows:

Median - If we are dealing with a data batch containing an odd number of data values, there will exist one value with the greatest depth. If the batch contains n values, then one half of the n-1 values will be less than median and one half will be greater than the median.

If the batch contains an even number of observations, then the median is defined by convention as the average

of the two middle points.

Hinges - The median divides the data batch into two halves. The hinge also splits each of the halves.

Hinge Spread - The difference between the upper and lower hinge values is the hinge spread.

Inner Fences - The inner fence is defined as the
 lower hinge - (1.5 x Hinge Spread)

and the upper hinge + (1.5 x Hinge Spread)

Outer Fence - The outer fence is defined as the lower hinge - (3.0 x Hinge Spread) and the upper hinge + (3.0 x Hinge Spread)

The fences are used to distinguish outlying data values.

Construction of the boxplot begins by building a box from hinge to hinge. A line is placed across the box to indicate the position of the median. A dashed line, or whisker, is now drawn from each hinge out to the inner fence. Values outside the fence are shown individually.

Figure 14 presents a boxplot of the data given in Table 6. Only a brief examination of the boxplot display provides useful information about the data batch. We can see that the median value is around 1.50 and that the hinge spread is about 1.10. The data is not symmetrically distributed. The median occurs in the upper half of the box. The upper whisker is much longer than the lower whisker. The two values outside the upper fence are clearly distant from the main data grouping. These high values probably deserve additional investigation to determine what factors may have resulted in the increased production.

Many of the commercially available statistical analysis computer software programs can provide computer generated EDA outputs.



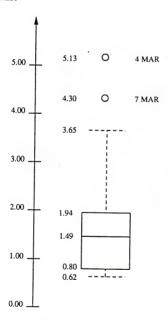


Figure 14. - Boxplot for the Production Rate Data Given in Table 6

Summary

The model development process begins with a thorough analysis of the observational data and hopefully an understanding of the underlying process. EDA provides simple analytical tools for learning the nature of the data. This preliminary examination of the data provides guidance for designing additional data collection methods and suggest relationships to be accounted for in the model development.

Stem and leaf plots provide a visual display of the data with the advantage of using the data values in the display. Boxplots also provide a graphical display of the data and are particularly useful in examining outlying values.

EDA techniques generally should be a prerequisite to the application of more advanced statistical procedures. Chapter 7 will cover additional statistical procedures which are applicable to analysis and modeling of construction production rate data.

CHAPTER 7

STATISTICAL ANALYSIS PROCEDURES

Introduction

Inferential statistics generally begins with a population of interest. In our case, the population consists of all production rates experienced by an organization within an established period of time. We would like to be able to make certain inferences about the general population using only a sample of the population. Our sample of the population consist of production rate observations collected from field sampling. Statistics furnishes the tools for establishing inferences about the population based upon samples.

Additionally, statistics provides a technique for developing a mathematical model representing the process of interest. In this case, we want to describe the dependent variable, production rate, as a function of the various productivity, influencing factors. Once established, this mathematical model can be used to predict future production rates, given the influencing factors.

This chapter will introduce basic statistical concepts which will provide the foundation for developing the prediction model. The least-squares method of matching the general linear model to the data will be presented. The fundamental assumptions upon which the statistics are based will be given and related to construction production rate data. The specific steps for applying the regression technique will be given. Also, a discussion of pitfalls to be avoided will be included.

The purpose of this chapter is not the development of complete statistical theory. Rather, the purpose is to present statistical tools which are important to the model building process and to explain relevant theoretical assumptions.

The General Linear Model

Application of statistical analysis to the problem of matching a mathematical model to research data begins with a single general model. This single model, called the general linear model, can be expressed as follows (Ott 1988):

$$Y = \beta_0 + \beta_1 X_1 = \beta_2 X_2 \dots + \beta_k X_k + \epsilon$$

In this model, the dependent variable is represented by Y. The S's represent the independent variables. The β 's are parameter estimates of the independent variables. The random error associated with the model is represented by ϵ .

The general linear model describes as an equation the relationship between the dependent variable of interest and other variables which affect the value of the dependent variable. Since this is a probablistic model, a random error term is also included. This random error term accounts for all unexplained and unpredictable factors which may influence the value of the dependent variable. However, we will assume that the average value of ϵ for a given value of X is equal to 0.

It is also important to understand that the general linear model can include both quantitative and qualitative independent variables. Dummy variables are formed by representing the X's as 1 and 0 are used to incorporate qualitative independent variables into the model.

Because we have assumed that the mean value of the random error term is equal to 0 and the values for β are constants, the expected value for Y or mean value of Y becomes an equation which describes a line. Plotting the expected value of Y, E(Y), produces a line which traverses the plotted actual values of Y. Points which lie on the line represent the expected value of Y at given values of the independent variables. If our linear model is the simple equation

$$Y = \beta_0 + \beta_1 X_1 + \epsilon$$

then the expected value of Y would be equal to β_0 + $\beta_1 X_1$. Figure 15 presents an illustration of this concept. The actual observed values of the dependent variable have been

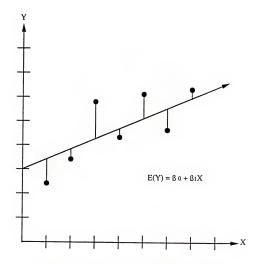


Figure 15. - Example of Plotting the Linear Model Equation

plotted against observed values of the single independent variable. The predicted value of Y has also been plotted as the equation $Y = \beta_0 + \beta_1 X_1$. For each actual value of Y, there exists some error or difference between the actual value and the predicted value. In general, we would like to obtain an equation which best fits the data, and reduced the total amount of error between the model and the data.

Regression and Inference

Least Squares Method

The statistical technique used to determine the model which best fits the data is called the least squares method. The predicted value of Y is represented by Yh. For each Yh there exists a difference or prediction error between Yh and the actual value of Y. This prediction error, Y - Yh, is called the residual. The least squares method develops a prediction equation which minimizes the sum of the squares of the prediction errors.

Therefore, we are seeking estimates of the β values which result in a minimum $\Sigma(Y-Yh)^2$. Using calculus, we find that the following relationships exist (Ott 1988):

$$\beta h_1 = \underline{Sxy}$$
 and $\beta h_0 = Y - \beta h_1 x$

where

$$Sxx = \Sigma (x - \overline{x})^2 = \Sigma x^2 - \underline{(\Sigma x)^2}$$

Sxy =
$$\Sigma$$
 (x - \overline{x}) (y - \overline{y}) = Σ xy - $\underline{(\Sigma x)}$ (Σ y) and n = number of values

It is common in statistical analysis to view this relationship in terms of the variability of the process. In other words, variance can be described as follows

$$\Sigma (y - \overline{y})^2 = \Sigma (yh - \overline{y})^2 + \Sigma (y - yh)^2$$

or

total variability unexplained variability explained + variability variability

The least squares approach can also be applied to the solution of models which include multiple variables and quadratic terms. The principle is the same. The solution involves the simultaneous resolution of multiple equations. Calculations are substantially more complex and warrant the use of computers.

Confidence and Prediction Intervals

Recall that one of our main objectives was to be able to make predictions of future production rates. It might be useful if we could also determine the accuracy of our predictions in advance. Statistics provides a technique for establishing the accuracy of our predictions.

When we are trying to estimate the mean value of ${\tt Y}$

$$E(Y) = \beta_0 + \beta_1 X_{12}$$

where X_2 is the value of X_1 at the point of interest. We use estimates of β_0 and β_1 to estimate Y as follows

$$Y = \beta_0 + \beta_1 X_{12}$$

so the source of error for our estimate of Y is β_{O} and β_{1} .

The variance for the estimate of E(Y) can be expressed as follows (Scheaffer and McClave 1986, 373):

$$\sigma^2$$
 = E ([Yh - E (Y)]²) = σ^2 [$\frac{1}{n}$ + $(\frac{X_p - x}{SSxx})^2$]

where σ^2 = variance of Y

Yh = predicted value of Y

E(Y) = expected value of Y

n = number of values

 x_p = value of a particular x

 \overline{X} = mean value of X

 $SSxx = \Sigma (x - \overline{x})^2$

Therefore, the confidence interval for the estimate value of Y is expressed by the following equation (Ott 1988, 356)

$$Y \pm t\alpha/2$$
 $S_E \sqrt{\frac{1 + (x - x)^2}{Sxx}}$

where $t\alpha/2 = t$ test statistic at $\alpha/2$

 $\alpha/_2$ = selected confidence interval probability.

n = number of values

 $S_{\rm E}$ = sample variance

 $Sxx = \Sigma (\overline{x} - x)^2$

This interval defines our confidence in the predictions for the mean value of Y. For instance, if we had selected an α of .05, we would expect the actual mean value of Y to fall within this interval 95% of the time.

Now, consider the case where we are interested in estimating a particular value of Υ .

$$Y_2 = \beta_0 + \beta_2 X_2 + \epsilon_2$$

Note that the equation now includes the error term. The source of error for prediction of a particular value are β_0 and β_2 and ϵ_2 . Therefore, the variance now includes an additional term and is expressed as follows (Scheaffer and McClave 1986, 373):

$$\sigma^{2}(Y_{p} - Yh) = E [(Y - Y_{p})^{2}] = \sigma^{2} + \sigma^{2}Y$$

$$= \sigma^{2} [1 + \frac{1}{n} + \frac{(X_{p} - \overline{X})}{SS_{xx}}]$$

The confidence interval for predicting a particular value of Y is now defined by the following equation (Ott 1988, 358):

$$Y \stackrel{+}{-} t\alpha/2 S_E$$
 [1 + $\frac{1}{n}$ + $\frac{(x - x)^2}{Sxx}$]

It should be noted at this point that the confidence interval for the prediction of the mean value of Y is narrower than the interval for the prediction of a particular value of Y. Figure 16 illustrates this concept. In the figure, the simple equation

$$E(Y) = \beta_0 + \beta_1 X_1 + \epsilon_1$$

has been plotted. Both the mean value and particular value confidence intervals also have been plotted.

Obviously, the usefulness of the production rate prediction model depends largely upon the accuracy of the

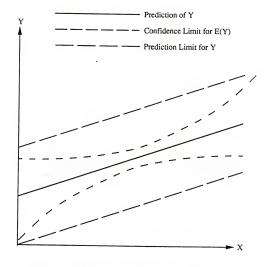


Figure 16. - Confidence and Prediction Intervals for E(Y) and (Y)

predictions. Statistical confidence intervals provide an important measure of the accuracy of the production rate model.

From the equations for the confidence and prediction intervals, several general observations may be made.

Specifically these points are as follows:

- The width of the interval will decrease as n increases. Including more observations improves the precision of the estimates.
- 2. The quantity $(x-\overline{x})^2$ is smaller as we approach the mean value of x. Therefore, the estimate precision is better towards the center of the x region.
- 3. $Sxx = \sum (x \overline{x})^2$ will increase as the spread of values for x increases. Therefore, within limits, the estimate precision is improved by increasing the ranges of X values.

These observations should be considered when designing the field sampling system.

Fundamental Assumptions

The general linear model and our solution to the model using the least-squares method are based upon specific fundamental assumptions concerning the population of interest. The validity and precision of predictions from the model are dependent upon whether or not the

initial assumptions are true. Therefore, it is important to recognize and understand what these assumptions are.

Four initial assumptions concerning variance make up the foundation of our approach to the method of least squares. These assumptions are listed as follows:

- 1. The random error term ϵ is assumed to have a normal probability distribution.
- 2. The random error term ϵ is assumed to have a mean equal to 0.
- 3. The random error term ϵ is assumed to be constant over all values of X.
- 4. The random error term ϵ is assumed to be independent among different observations.

The validity of these assumptions generally is tested most readily by examining plots of the residuals plotted against the variables used in the model. The least squares method is fairly robust with regard to the assumption of normality. Useful results can be obtained even using skewed populations.

However, the assumptions concerning ϵ having a mean value of 0 and being homogeneous for all values of X, are critical. In some cases, transformations of the input data may improve the validity of the assumptions. A great deal of statistical research has been done in this area and several advanced techniques have been developed (Draper and Smith, 1981).

Multiple Regression Steps

Step 1: Variable Selection

Choosing potential variables which may be reasonably expected to affect the dependent variable is an important part of the regression procedure. The final results of the model will depend to a great extent upon the validity of the selected variables. In this step of the regression process; it is absolutely essential to obtain the expertise of persons experienced in the working of the process to be modeled. This concept is made by (Ott 1988, 541) as follows:

The input of a person knowledgeable in the subject matter field is a valuable source of advice on reasonable (independent) variables that could influence the response (dependent variable) of interest.

For example, in highway construction, experienced field personnel, such as project superintendents and field engineers, are likely to provide the most accurate information concerning influencing factors for specific work activities. Skillful questioning by the researcher can produce a list of potential influencing factors for each activity of interest. The idea is to put together a list of variables which are related to the dependent variable (production rate) and not to one another.

When adequate computer resources are available, trial regressions should commence with all possible variables included in the model. The result of each model is

evaluated statistically. The model providing the most desirable result is selected.

There are, however, several different statistical criteria for evaluating regression models. One criterion is the \mathbb{R}^2 statistic. The coefficient of determination, \mathbb{R}^2 , is defined as the portion of variability of the independent variable which is explained by the model. \mathbb{R}^2 is calculated as follows (Ott 1988, 490):

$$R_{y}^{2} = \frac{Syy - SSE}{Syy}$$

where

$$Syy = \Sigma Y_2^2 - (\Sigma Y_2)_2$$

and

$$SSE = \Sigma (Y_2 - Y_2)^2$$

One of the best criterion for model selection is the Cp statistic (Mallows 1973). The Cp statistic has been shown to provide a balance of both overfitting and underfitting. The Cp method gives a model with the best estimate precision. The Cp statistic is defined as follows (Ott 1988, 545):

$$Cp = \frac{SSEp}{S_{\epsilon}^2 - (n - 2p)}$$

where SSEp is the sum of squares for the error model

with p parameters included

and S_{ε} is the mean square error from the regression equation with the largest number of independent variables.

The Cp theory states that the best model is obtained at the point where the value of Cp approaches P. Figure

17 provides a plot of Cp vs P for a typical model selection procedure. The best model is the model where Cp first approaches the value of P.

Step 2: Refining the Model

The initial model formula will likely be a lower order linear equation of the form Y = β_0 + $\beta_1 X_1$ + $\beta_2 X_2$ + $\beta_3 X_3$. Some relationships between the dependent variable and the parameters can best be described by the addition of a quadratic term to the equation. An examination of a plot of the residuals verses the parameter values will indicate whether a quadratic term is needed. A plot of residuals verses X2 which shows a curved pattern reveals the need

for a quadratic term of the form $\beta_2 X_2^2$.

Much of the model refinement amounts to a trial and error process guided by knowledge of the underlying process and residual analysis.

Step 3: Verifying Statistical Assumptions

After identifying the independent variables and formulating the model equation, the next step is to verify the original statistical assumptions. These original assumptions, which were declared previously in this chapter, concern the variance of the error term.

Verification of assumptions may be directly confirmed by examination of residual plots.

If step 2 has been successfully completed, the assumption of zero expectation of the error term should

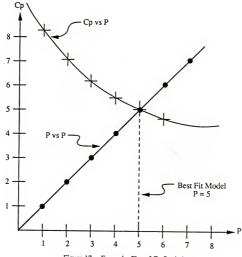


Figure 17. - Example Plot of Cp Statistic

prove correct. If mean value of the error term is not zero, the model does not adequately represent the process being modeled.

The assumption of constant variance can be checked by examining a plot of residuals verses the predicted value of the dependent variables. The assumption is correct if the residual plot shows a random scattering of point for all values of variables. If, however, the range of residuals in much different at different levels of the X variable, heterogeneous variance is suggested.

Verification of assumption number three, that the distribution of the value of the error term is normally distributed, is done by plotting a frequency histogram of the residual values. Any skewedness will be detected in the histogram plot.

The final assumption is that the error terms are independent from one observation to another. If the time sequence of observations is known, a plot of the residuals verses time will show if adjacent residual in time appear to be similar. Additionally, the Durbin-Watson formal test may be performed to check for serial correlation (Durbin and Watson 1951).

The consequences of non-validity of assumptions depend upon which assumption is violated. The least squares method is rather robust with regard to the assumption of normality. Useful estimates can be obtained even with skewed distributions.

However, the assumption of constant variance is more critical. A heterogeneous variance will effect the accuracy of the least squares estimates. In other words, the precision of the model is reduced. Also, the width of the prediction interval for individual values of Y may be inconsistent. The width of the interval may depend upon the range of variance at the prediction point (Ott 1988).

Transforming the input data into another format, such as a logarithmic value, may eliminate heterogeneous variance problems.

Summary

Statistical tools are an integral part of the model development system. Using the least squares method, a regression equation can be developed from the sample data. Statistics also allows for the development of confidence and prediction intervals for model estimates of the dependent variable.

step 1: Variable Selection

step 2: Refining the Model

step 3: Verification of Statistical Assumptions Figure 18 presents a flow diagram of the regression procedure.

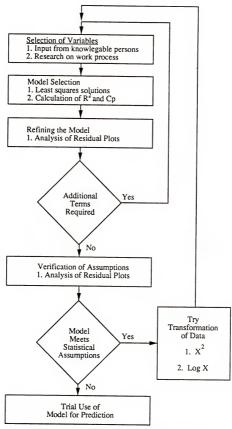


Figure 18. - Schematic Flow Chart of Regression Process

In the next chapter, these statistical methods will be applied to developing a production rate model for highway construction.

CHAPTER 8

MODEL CONSTRUCTION: CASE HISTORY

Introduction

Previous chapters have presented a review of various data collection and theoretical modeling techniques. This previous information was compiled as background knowledge for the actual problem of modeling construction production rates.

This chapter will cover the experimental application of the production rate influencing factor theory to the development of an actual predictive model. Using the techniques previously discussed, production rate models are developed for several highway construction activities. The research methodology and modeling procedure will be presented with a critical evaluation of the results.

Objective

The purpose of this research was to determine the validity of the theoretical factorial model for construction production rates. The objective of the

models was to provide more precise predictions of future production rates.

Research Methodology

Research Procedure

This investigation was made in connection with a study undertaken by the Department of Civil Engineering, University of Florida, at the request of the Florida Department of Transportation (FDOT), (Herbsman and Ellis 1988). The purpose of the research study was to examine production rates currently used by the Florida Department of Transportation and to make recommendations for revisions where appropriate.

The current investigation involved four distinct phases which are listed as follows:

- 1. Preliminary selection of Variables
- 2. Collection of Data
- Model Development
- 4. Model Testing.

Each of these steps will be covered separately in the following sections.

Preliminary Selection of Variables

The first phase of the study consisted of developing a preliminary list of Construction Production Rate

Influencing Factors. This identification of CPIF's was required prior to designing the data collection system.

It is obviously necessary to target variables of interest before undertaking data collection.

Information about potential influencing factors was obtained from two primary sources. First, structured interviews were conducted with knowledgeable persons working in the highway construction industry. These people included contractor superintendents and FDOT field engineers. Secondly, direct observations were made of the actual work activities by the author.

Five construction activities were selected as being representative of the type of work included on a typical highway construction project. These five activities are:

- 1. Clearing and Grubbing
- Excavation
- 3. Base Installation
- 4. Asphalt Pavement
- Storm Drainage

Based upon the preliminary investigations, a list of factors was developed for each of these activities. This list includes a number of project and environmental items which are applicable to each activity. In addition, each of the individual activities also was assigned activity factors applicable only to that activity.

Figure 19 presents the list of general factors with explanations. Figure 20 presents the activity related factors chosen.

Total Price Type of Project Local Condition	Explanation Total amount of activity work in project Total contract price for project General category of the project Site Conditions	: New Construction Recontstruction Bridge Intersection Improvement Signalization : Urban Rural Limited Access
Traffic Conditions	Traffic volume on roadway	: Light Medium Heavy

Figure 19. - List of General Factors

Activity	Factor	Explanation	
Clearing and Grubbing	Level of Clearing	Degree of Clearing Required	: Light – Brush Medium – Brush and Small Trees Heavy – Large Trees and Brush
Excavation	Type of Excavation	Type of Excavation	: Lateral Ditch Regular Subsoil
	Type of Material	Type of Material to be excavated	: Sand Rock Muck
Base	Type of Material	Type of Material to be Installed	: Limerock Shell Sand Clay Soil Cement Asphali
Asphalt	Small Areas	Installation of Small Areas	ie:Intersections, Drives ect.
Storm Drains	Depth Diameter	Depth of Installation Diameter of Pipe	

Figure 20. - List of Activity Factors

It should be noted that this particular model has been designed to be used by an owner such as the FDOT. Therefore, organizational factors related to the contractor were not included in the model. Prior to bid award, the owner has no way of knowing who the contractor will be. Consequently, contractor related factors are of little use in pre-bid predictions of production rates. Collection of Data

After variable selection, a data collection system was developed. Observations of production rates and factorial values were obtained from FDOT construction projects. Projects were selected on a stratified random sample basis. This means that an conscious attempt was made to obtain observations for each work activity of interest. However, within the category projects were selected randomly.

Observations were made by FDOT field engineers assigned to the projects. A data collection form was designed for recording and reporting the field observations. The final design of the form required numerous discussions with FDOT field personnel to insure that the instructions and wording would be clear to the persons recording the data. Copies of the data collection forms are provided as Appendix A.

A total of 60 projects were observed. Table 7 presents a description of the sample data base.

Table 7. - Description of Data Base

Work Activity	Number of Observations	Number of Variables Per Observation
Clearing and Grubbing	96	18
Excavation	113	21
Base Installation	151	18
Asphalt Pavement	188	16
Storm Drains	97	17

Because of the size of these data sets, they have been included as Appendix B rather than included in the text.

Originally, the raw data were entered into a spread sheet data base. Later, the spread sheet data was translated and reformatted as a SAS data set. This transfer from one software system to another required a considerable amount of labor. Inputing directly into the SAS system is recommended for future research.

The data sets enclosed in the Appendix B are copies of the SAS data sets. $\label{eq:BAS} % \begin{subarray}{ll} \end{subarray} % \begin{subarra$

The statistical analysis procedures used for regression require quantitative variables. Therefore, the qualitative variables have been transformed into binary form.

For example, consider the following observations for the Traffic variable.

<u>Obs</u>	Traffic
1	L
2	м
3	н
4	н
5	L

When transformed the data set has the following form:

<u>Obs</u>	Traffic-L	Traffic-M	Traffic-H
. 1	1	0	0
2	0	1	О
3	0	0	1
4	0	0	1
5	1	0	О

Binary form allows for analysis of qualitative factors.

Computer Software and Hardware

Raw data were originally entered into a LOTUS spread sheet data base. Subsequently, the LOTUS data were transferred to a SAS system. Data base management and manipulation was performed using Base SAS software for personal computers. Statistical analysis was performed using SAS/STAT software for personal computers. A copy of all source codes used is enclosed as Appendix D.

The computer hardware consisted of an IBM OS/2 Model/50. Data handling and statistical routines were reasonable efficient in the PC environment. Statistical processing of typical data sets was performed in less than 20 minutes.

The SAS system is available for both mini and main frame environments. Depending upon the expected size of the data base, some users might consider moving up from the PC environment.

Model Development

Model development was accomplished with the aid of the SAS Proc Reg procedure which performs advanced regression procedures. This software procedure is a least squares regression technique with many diagnostic options.

Preliminary model selection was made on the basis of Mallow's Cp statistic. A regression of all possible models was run and the Cp statistic was computed for each model. The selected model was the model where Cp was approximately equal to the number of parameters in the model.

Complete copies of all regression procedures computer output are enclosed as Appendix C.

An example of the Cp-P selection criteria is presented in Table 8, which includes the Cp statistic values for all trial models used for the Clearing and Grubbing activity.

The model selected for Clearing and Grubbing was
Model Number 13 which resulted in a Cp of 13.06 and a P of
13. Recall that Mallow's theory defines the best fitted
model as occurring when Cp is approximately equal to P.

The preliminary model selected for Clearing and Grubbing is presented in Figure 21.

The same selection procedure was carried out for each of the five activities.

Table 8. - Listing of Cp Values for Trial Models for Clearing and Grubbing

Mallows Coefficient of Determination R2	Number of Parameters P	Model Number
48.75 0.156	1	1
41.09 0.212	2	2
1.56 0.465	3	3
1.15 0.470	4	4
1.85 0.478	5	5
1.28 0.493	6	6
3.08 0.494	7	7
4.91 0.495	8	8
6.59 0.497	9	9
8.29 0.499	10	10
9.57 0.503	11	11
11.16 0.505	12	12
13.06 0.506	13	13
15.00 0.506	14	14
1 -		

Source	Sum of Squares			
Model Error Total	305.22 308.40 613.63	R ² Cp	=	5.71 0.497 13.00 13.00

<u>Variable</u>	Parameter Estimate	<u>F</u>
Production Rate = Intercept	-1.56176250	0.54
Total Quantity	0.00000019	1.33
Reconstruction	0.76935595	0.79
Bridge	0.46724565	0.12
Intersection	1.26508184	0.97
New Construction	0.64066488	0.22
Rural	-1.26460744	1.75
Limited	1.32878210	0.45
Medium Traffic	-1.12675576	0.71
Heavy Traffic	0.08239762	0.00
Total Quantity ²	-0.00049047	20.15
Medium Clearing	1.05844360	1.17
Heavy Clearing	2.18553138	2.97

Figure 21.-Preliminary Model Selected for Clearing and Grubbing

The next step was to examine the residual plots of the preliminary models. The purpose of residual analysis is to verify the fundamental statistical assumptions. Analysis of the plot of the residuals versus the dependent variable and independent variables detected a problem with our assumption of homogeneous variance. Figure 22 is the residual plot of residual versus production rate for clearing and grubbing. Figure 22 clearly indicates an increase in variance as the dependent variable, production rate, increases.

Figures 23, 24, and 25 give the residual plots for the independent variables Total Quantity, Total Quantity², and Price respectively. Analysis of these plots also indicates heterogeneous variance to a lesser degree.

A logarithmic transformation of the data was performed as a trial remedy for the variance problems. This was accomplished by transforming the input data set values into their Log base e components. The form of the transformation was

Transformed Y = Log Y

Following transformation of the data, the model selection process was repeated using the transformed data. The model selection routine resulted in a new preliminary model which now included logarithmic variables. In general, the $\rm R^2$ values were substantially improved. For example, the $\rm R^2$ value for Clearing and Grubbing increased from 0.506 to a new value of 0.732. This improvement in

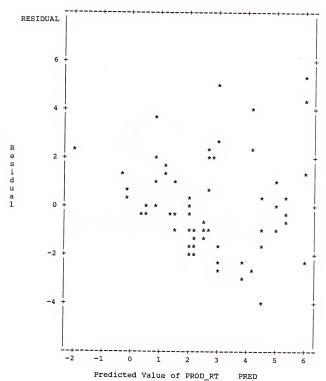


Figure 22.-Residual Plot of Production Rate Variable for Clear and Grubbing

PREDICTION MODEL FOR CLEAR AND GRUBB
Plot of YRESID*TOT_QTY. Symbol used is '*'.

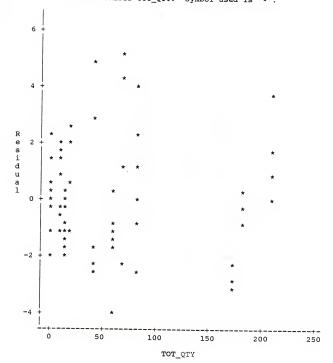


Figure 23.-Residual Plot of Total Quantity Variable for Clear and Grubbing

PREDICTION MODEL FOR CLEAR AND GRUBB

Plot of YRESID*TOT_QTY2. Symbol used is '*'.

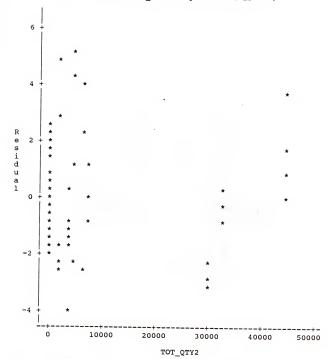


Figure 24.-Residual Plot of Total Quantity² Variable for Clear and Grubbing

PREDICTION MODEL FOR CLEAR AND GRUBB

Plot of YRESID*PRICE. Symbol used is '*'.

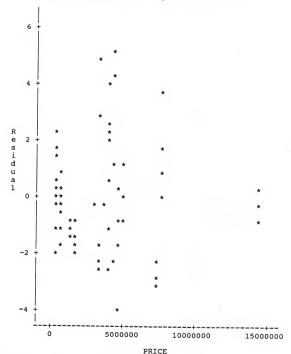


Figure 25.-Residual Plot of Price Variable for Clearing and Grubbing

 ${\mathbb R}^2$ is because the transformed input data now more closely matched the linear model upon which the regression procedure was based.

Analysis of the residual plots using the transformed data, indicated homogeneous variance across all variables. Figures 26, 27, and 28 present the residual plots for Clearing and Grubbing using transformed data. Data transformation solved the variance problem and improved the models precision.

Copies of the residual plots for all five activities are included in Appendix C. All activities experienced model improvement with logarithmic transformation.

Preliminary testing of the models suggested by the Cp procedure indicated problems when certain levels of a classification variable were dropped from the model and other levels were retained. Therefore, final models used were adjusted to contain all levels of classification variables, providing sufficient observations existed. This resulted in a small decrease in \mathbb{R}^2 , however, the utility of the models was greatly improved.

The final step in the regression procedure was to calculate the parameter estimates for the final model variables. Additionally, confidence intervals and prediction intervals for the observations were calculated.

Figures 29, 30, 31, 32, and 33 present the statistical results for the final prediction models. The highest \mathbb{R}^2 obtained was 0.69 for Clearing and Grubbing and

PREDICTION MODEL FOR CLEARING AND GRUBBING

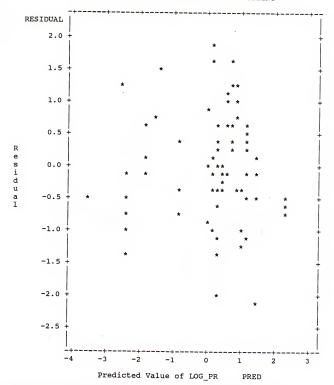


Figure 26.-Residual Plot of Production Rate Variable for Clear and Grubbing Using Transformed Data

PREDICTION MODEL FOR CLEARING AND GRUBBING Plot of YRESID*LOG_TQ. Symbol used is '*'.

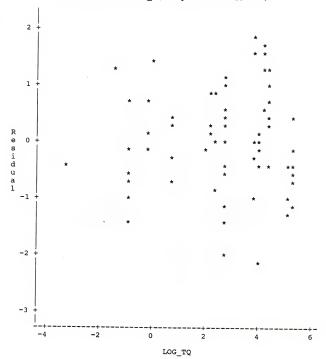


Figure 27.-Residual Plot of Total Quantity Variable for Clear and Grubbing Using Transformed Data

PREDICTION MODEL FOR CLEARING AND GRUBBING Plot of YRESID*LOG_PRI. Symbol used is '*'.

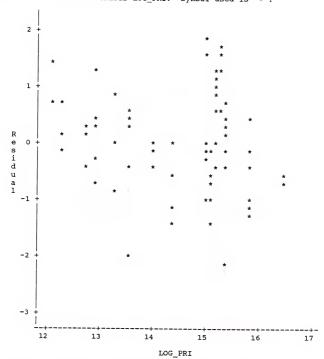


Figure 28.-Residual Plot of Price Variable for Clear and Grubbing Using Transformed Data

Source	Sum of Squares	F	=	14.18
Model Error Total	133.838 59.778	R ²	=	0.691

<u>Variable</u>	Parameter Estimate	I
Production Rate = Intercept	-1.181892	-2.443
LOG Total Quantity	0.567505	4.895
Reconstruction	0.692154	1.584
Bridge	0.705082	1.137
Intersection	0.122397	0.212
New Construction	0.330528	0.532
Light Traffic	0.283303	0.427
Medium Traffic	0.054329	0.140
Medium Clearing	-0.244324	-0.514
Heavy Clearing	-0.021495	-0.039
Rural	-1.139281	-2.879
Urban	-0.578627	-1.417
Limited	-0.259863	-0.367

Figure 29.-Final Model for Clearing and Grubbing

Bource	sum of Squares			
Model Error Total	167.931 75.159 243.090	R ²	=	14.3 0.691

<u>Variable</u>	Parameter Estimate	<u>T</u>
Production Rate = Intercept	5.755543	4.988
Log Total Quantity	0.437740	6.493
Reconstruction	-2.554510	-2.624
Intersection	-3.820465	-3.675
New Construction	-1.786693	-1.795
Signalization	-2.846023	-2.350
Rural	-0.600389	-1.547
Urban	0.442833	1.126
Light Traffic	1.242225	1.872
Heavy Traffic	-0.943232	-0.752
Medium Traffic	0.209213	0.396
Lateral Ditch	0.122206	0.152
Regular Excavation	-0.339945	-0.641
Sand Soil	-0.733178	-2.026
Rock Soil	-0.569347	-0.771
Muck Soil	-0.058412	-0.087

Figure 30.-Final Model for Excavation

Source	<u>sum or squares</u>		
Model Error Total	111.706 167.785 279.491	F R2	= 6.094 = 0.400

<u>Variable</u>	Parameter Estimate	T
Production Rate = Intercept	3.557789	2.381
Log Total Quantity	0.333261	3.808
Reconstruction	1.592424	1.328
Bridge	2.434882	1.500
Intersection	0.394522	0.298
New Construction	1.687546	1.280
Signalization	0.931067	0.757
Rural	-1.062293	-1.693
Urban	-1.356593	-1.929
Light Traffic	0.710581	1.375
Heavy Traffic	-0.402573	-0.956
Sand - Clay	0.435642	0.540
Limerick	-0.697203	-1.142
Asphalt	0.175503	0.264

Figure 31.-Final Model for Base

Model Error Total	179.389 86.279 265.669	F = 27.549 $R^2 = 0.675$
<u>Variable</u>	Parameter Estimate	I
Production Rate = Intercept	1.197071	1.184
Log Total Quantity	0.558623	10.189
Reconstruction	0.611475	1.007
Bridge	1.194745	1.824
Intersection	0.153371	0.233
New Construction	0.070499	0.104
Rural	0.423256	-1.130
Urban	0.199363	-0.484
Light Traffic	0.506167	0.593
Heavy Traffic	-0.465685	-0.549
Medium Traffic	-0.274218	-0.062
Limited	-0.274218	-0.567
Small Areas	-0.221864	01.286

Sum of Squares

Source

Figure 32.-Final Model for Asphalt Pavement

Source	Sum of Squares	
Model Error Total	53.303 37.816 91.119	$F = 8.105$ $R^2 = 0.5850$
<u>Variable</u>	Parameter Estimate	T
Production Rate = Intercept	2.830616	2.997
Log Total Quantity	0.286849	3.728
Reconstruction	-0.128761	-0.252
Intersection	-0.219912	-0.290
New Construction	-0.191264	-0.278
Signalization	-1.298789	-2.153
Rural	-0.146479	-0.313
Urban	-0.115760	-0.289
Heavy Traffic	-0.002649	-0.003
Medium Traffic	0.223525	0.273
Light Traffic	-0.461404	-0.473
Diameter	-0.029787	-2.750

Figure 33.-Final Model for Storm Drains

0.026092

0.280

Depth

the lowest was 0.40 for Base Installation. Recall that R^2 is the portion of the data variability accounted for by the model. Therefore, the final models account for approximately 40 to 70 percent the total variability. The large F values for the models indicate that the models are statistically highly significant.

 ${\tt A}$ complete print out of the confidence and prediction intervals is included in Appendix C.

It should be noted that the final models include some variables with rather high probabilities of not effecting the dependent variable. These variables were not removed from the model because prediction accuracy was the primary objective of the model. If efficiency is also a consideration, then variables with a high probability of a greater T test statistic might be removed.

Furthermore, the model produced is a predictive model. That is, the parameter estimates were developed on the basis of improving the model's overall prediction precision. Taken individually they do not necessarily represent the exact contribution of the variable.

 $\ensuremath{\mathtt{A}}$ summary of the regression procedure is given in Figure 34.

- Step 1 Perform regression for all possible models.

 Select preliminary model on basis of Cp.
- Step 2 Analyze residuals for selected model.

 Heterogenous variance indicated.
- Step 3 Perform log transformation of the data.
- Step 4 Perform regression for all possible models.

 select preliminary model on basis of cp.
- Step 5 Analyze residuals for selected model.

 Variance acceptable.
- Step 6 Produce parameter estimates, confidence intervals, and prediction intervals for final model.
- Figure 34.-Summary of Regression Procedures Used in Model Development

Model Verification

Trial Procedure

Test data observations were obtained from two different projects for each of the five activities modelled. The test data sets contained the same type of factors measured in the original productivity survey. The test data were collected and recorded in the same manner as the model data base. None of the test observations were used in model development.

Using the factorial data from the test observations, a predicted mean production rate was calculated using the model previously developed. Actual production rate observations were compared to the predicted values.

Tables 9 through 20 present the prediction calculations for the different activities. The factorial data for the storm drain activity varied from observation to observation, therefore, several predictions were made for storm drain production rate. However, the factorial data were constant for the other activities for all observations. This resulted in a single prediction for average production rate.

The results of the actual versus prediction comparisons are presented in Table 21.

Generally, the precision of the models appeared related to \mathbb{R}^2 the coefficient of determination. Activity models with the highest \mathbb{R}^2 resulted in the highest estimate precision. This seems to be in agreement with

Table 9. - Calculation of Prediction Value for Clearing and Grubbing Test $\mathbf{1}$

TEST 1

Activity: Clearing And Grubbing

FDOT Project: 1520-3610

1320-3610				
Factor	Parameter Estimate	Observed Variable Value	Transformed Variable Value	PR Factor
Intercept Log Total Quantity	-1.182 0.568	1 57.91	-1.182 4.058890081	-1.182 2.305
Reconstruction New Bridge Intersection New Construction Signalization Light Medium Heavy Medium Clearing Heavy Clearing Rural Urban Limited	0.692 0.705 0.122 0.331 0.000 0.283 0.054 0 -0.244 -0.201 -1.140 -0.579 -0.260	1 0 0 0 0 1 0 0 0 0 1 1 0 0		0.692 0.000 0.000 0.000 0.283 0.000 0.000 0.000 -0.201 -1.140 0.000 0.000 0.000 0.000

Predicted Mean Production Rate (Log)

0.757 2.133

Predicted Mean Production Rate

Acres/Day

Table 10. - Calculation of Prediction Value for Clearing and Grubbing Test 2

TEST 2 Activity: Clearing And Grubbing

FDOT Project: 60060-3507

Factor	Parameter Estimate	Observed Variable Value	Transformed Variable Value	PR Factor
Intercept Log Total Quantity	-1.182 0.568	1 1.54	-1.182 0.431782416	-1.182 0.245
Reconstruction New Bridge Intersection New Construction Signalization Light Medium Heavy Medium Clearing Heavy Clearing Rural Urban Limited	0.692 0.705 0.122 0.331 0.000 0.283 0.054 -0.244 -0.201 -1.140 -0.579 -0.260	0 1 0 0 1 0 1 0 1 0		0.000 0.705 0.000 0.000 0.000 0.000 0.000 0.000 -0.201 -1.140 0.000 0.000 0.000 0.000

Predicted Mean Production Rate (Log)

-1.290 0.275

Predicted Mean Production Rate

Acres/Day

Table 11. - Calculation of Prediction Value for Excavation Test 1

TEST 1

Activity: Excavation

FDOT Project: 2010-3523

Factor	Parameter Estimate	Observed Variable Value	Transformed Variable Value	PR Factor
Intercept Log Total Quantity	5.755 0.438	145475	5.755 11.88775952	5.755 5.203
Reconstruction New Bridge Intersection New Construction Signalization Light Medium Heavy Rural Urban Limited Lateral Ditch Excay	-2.550 0.000 -3.820 -1.790 -2.846 1.242 0.209 -0.943 -0.600 0.442 0.000 -0.579	1 0 0 1 0 1 0 0		-2.550 0.000 0.000 -1.790 0.000 1.242 0.209 0.000 0.000 0.442 0.000
Regular Excav Sand Soil Rock Soil Muck Soil	-0.260 -0.733 -0.569 -0.058	1 1 0		-0.260 -0.733 0.000 0.000

Predicted Mean Production Rate (Log)

7.518

Predicted Mean Production Rate

1840.831 CY/Day

Table 12. - Calculation of Prediction Value for Excavation Test 2

TEST 2

Activity: Excavation

FDOT Project: 70220-3429

Factor		T		
Factor	Parameter Estimate	Observed Variable Value	Transformed Variable Value	PR Factor
Intercept Log Total Quantity	5.755 0.438	1 116329	5.755 11.66417766	5.755 5.105
Reconstruction	-2.550	1		2.550
Intersection New Construction Signalization	-3.820 -1.790 -2.846	0 0 0		0.000
Light Medium Heavy	1.242 0.209 -0.943	0 1 0		0.000 0.209 0.000
Rural Urban	-0.600 0.442	0		0.000
Lateral Ditch Excav	-0.579	0		0.000
Regular Excav Sand Soil Rock Soil Muck Soil	-0.260 -0.733 -0.569 -0 058	1 1 0 0		-0.260 -0 733 0.000 0 000

Predicted Mean Production Rate (Log)

7.526

Predicted Mean Production Rate

1.520

1855.873 CY/Day

Table 13. - Calculation of Prediction Value for Base Test 1

Activity: Base

FDOT Project: 11140-3507

Factor	Parameter Estimate	Observed Variable Value	Transformed Variable Value	PR Factor
Intercept Log Total Quantity	3.558 0.333	1 7701	3.558 8.949105469	3.558 2.980
Reconstruction Bridge Intersection New Construction	1.592 2.434 0.395 1.687	1 0 0		1.592 0.000 0.000 0.000
Signalization Light Heavy	0.931 0.711 -0.402	0		0.000 0.000 0.150
Rural Urban Sand-clay	5 -1.062 -1.357	0 1 0		0.000 -1.062 0 000 0.000
Limerock Asphalt	-0.579 -0.260	1 0		-0.579 0.000 0.000 0.000

Predicted Mean Production Rate (Log)

6.639

Predicted Mean Production Rate

764.370 SY/Day

Table 14. - Calculation of Prediction Value for Base Test 2

Activity: Base

FDOT Project: 36090-3506

Factor	Parameter Estimate	Observed Variable Value	Transformed Variable Value	PR Factor
Intercept Log Total Quantity	3.558 0.333	1 76799	3.558 11.24894689	3.558 3.746
Reconstruction Bridge Interjection New Construction Signalization Light Heavy Rural Urban Sand-clay Limerock Asphalt	1.592 2.434 0.395 1.687 0.931 0.711 -0.402 5 -1.062 -1.357 -0.579 -0.260	0 0 0 1 0 1 0		1.592 0.000 0.000 0.000 0.711 0.000 -1.062 0.000 0.000 -0.579 0.000 0.000

Predicted Mean Production Rate (Log)

7.966

Predicted Mean Production Rate

2881.019

SY/Day

Table 15. - Calculation of Prediction Value for Asphalt Pavement Test 1

MODEL PREDICTION OF MEAN PRODUCTION RATE

TEST 1

Activity: Asphalt

FDOT Project: 36090-3506

Factor	Parameter Estimate	Observed Variable Value	Transformed Variable Value	PR Factor
Intercept Log Total Quantity	1.197 0.559	1 35738	1.197 10.48396982	1.197 5.856
Reconstruction Bridge Intersection New Construction Light Medium Heavy Rural Urban Limited Small Areas	0.611 1.195 0.153 0.070 0.506 -0.051 -0.466 -0.423 -0.199 -0.274 -0.579	1 0 0 0 1 0 0 1 0 0		0.611 0.000 0.000 0.000 0.506 0.000 -0.423 0.000 0.000

Predicted Mean Production Rate (Log)

7.748

Predicted Mean Production Rate

2316.268 Tons/Day

Table 16. - Calculation of Prediction Value for Asphalt Pavement Test 2

TEST 2

Activity: Asphalt

FDOT Project: 36090-3506

Factor	Parameter Estimate	Observed Variable Value	Transformed Variable Value	PR Factor
Intercept Log Total Quantity	1.197 0.559	1 1311	1.197 7.178545483	1.197 4.010
Reconstruction Bridge Intersection New Construction Light Medium Heavy Rural Urban Limited Small Areas	0.611 1.195 0.153 0.070 0.506 -0.051 -0.466 -0.423 -0.199 -0.274 -0.579	0 1 0 0 0 1 0 0		0.000 1.195 0.000 0.000 0.000 -0.051 0.000 0.000 -0.199 0.000

Predicted Mean Production Rate (Log)

Predicted Mean Production Rate

6.151 469.391

Tons/Day

Table 17. -Calculation of Prediction Value for Storm Drains Test 1, Observations 1 and 2

TEST 1 Obs. 1, 2 Activity: Storm Drain

FDOT Project: 02010-3523

Factor	Parameter Estimate	Observed Variable Value	Transformed Variable Value	PR Factor
Intercept Log Total Quantity	2.831 0.287	1 1026	2.8306 6.933423025	2.831 1.989
Reconstruction	-0.129	1		-0.129
Intersection New Constriction Signalization Light Medium Heavy Rural Urban Diameter Depth	-0.220 -0.191 -1.299 -0.461 0.224 -0.003 -0.146 -0.116 -0.030 0.026	0 0 0 1 0 0 1 30		0.000 0.000 0.000 0.000 0.000 0.224 0.000 0.000 -0.116 -0.891 0.131

_			- 1		
	Predicted Mean	Production	Rate	(Log)	4.038
	Predicted Mean	Production	Rate		56.696

Table 18. - Calculation of Prediction Value for Storm Drains Test 1, Observation 3

Activity: Storm Drain

FDOT Project: 02010-3523

Factor	Parameter Estimate	Observed Variable Value	Transformed Variable Value	PR Factor
Intercept Log Total Quantity	2.831 0.287	1 1026	2.8306 6.933423025	2.831 1.989
Reconstruction	-0.129	1		-0.129
Interjection	-0.220	0		0.000
New Construction	-0.191	0		0.000
Signalization	-1.299	Ö		0.000
Light	-0.461	Ö		0.000
Medium	0.224	1		0.224
Heavy	-0 003	0		0.000
Rural	-0.146	0		0.000
Urban	-0.116	1		-0.116
Diameter	-0.030	30		-0.891
Depth	0.026	6		0.157

Predicted Mean Production Rate (Log) 4.064

Predicted Mean Production Rate 58.195
LF/Day

Table 19. -Calculation of Prediction Value for Storm Drains Test 1, Observations 4 and 5

TEST 1 Obs. 4, 5 Activity: Storm Drain

FDOT Project: 02010-3523

Factor	Parameter Estimate	Observed Variable Value	Transformed Variable Value	PR Factor
Intercept Log Total Quantity	2.831 0.287	1 1026	2.8306 6.933423025	2.831 1.989
Reconstruction	-0.129	1		-0.129 0.000
Intersection New Construction Signalization Light Medium Heavy Rural Urban Diameter Depth	-0.220 -0.191 -1.299 -0.461 0.224 -0.003 -0.116 -0.030 0.026	0 0 0 1 0 0 1 15	-	0.000 0.000 0.000 0.000 0.000 0.224 0.000 0.0116 -0.446 0.078
		-		0.070

Predicted Mean Production Rate (Log) 4.431

Predicted Mean Production Rate 84.016
LF/Day

Table 20. - Calculation of Prediction Value for Storm Drains Test 2

TEST 2 Activity: Storm Drain

FDOT Project: 48731-3604

Factor	Parameter Estimate	Observed Variable Value	Transformed Variable Value	PR Factor
Intercept Log Total Quantity	2.831 0.287	1 920	2.8306 6.82437367	2 831 1.957
Reconstruction	-0.129	0		0.000
Intersection	-0.220	1		0.000 -0.220
New Construction Signalization	-0.191	0		0.000
Light	-1.299 -0.461	0		0 000
Medium	0.224	0		0 000
Heavy	-0.003	1		0 224
Rural	-0.146	0		0 000
Urban	-0.146	0		0.000
Diameter	-0 030	1 1		-0 116
Depth	0.026	18		-0 535
pepen	0.026	2.5		0.065

Predicted Mean Production Rate (Log)

4.206

Predicted Mean Production Rate

67.113 LF/Day

Table 21. - Summary of Model Verification Testing

Activity		Actual	Predicted	Actual	Predicted
Units	i	Production	Production	Production	Production
Test No.	Obs.	Rate	Rate	Rate	Rate
	No.		1400	MEAN	
Project No.				MEAN	MEAN
Clear and	1	3.44	2.13	3.34	2.13
Grub	2	2.13	2.13	1	
	3	2.82	2.13		1
Acres/Day	4	4.96	2.13		
	5	3.37	2.13		
Test 1	1	0.17	0.28	0.31	0.28
01520-3610	1 2	0.23	0.28	0.31	0.20
	3	0.66	0.28	1	
Test 2	4	0.15	0.28	1	
60060-3507	5	0.33	0.28		
-	1	1800			
Excavation	2	1548	1840	1282	1840
cy/Day	3	1428	1840		
	4		1840		
Test 1		732	1840		1
02010-3523	5	900	1840		
	1	1296	1856	1781	1856
Test 2	2	2136	1856		
70220-3429	3	1968	1856		i
	4	1608	1856	1	
	5	1896	1856	l	
Base	1	767	764	1387	764
sy/Day	2	1600	764		
	3	2767	764	1	
Test 1	4	1533	764	1	
11140-3507	5	267	764	1	
	1	2172	2881	4117	2881
Test 2	2	3164	2881	411/	2881
36090-3506	3	6422	2881		
20030-2200	4	5194			
	5	3635	2881		
			2881		
Asphalt	1	2022	2316	1993	2316
	2	2213	2316		
Pavement	3	1052	2316		
Tons/Day	4	2320	2316		
	5	2359	2316		
Test 1	1	261	469	207	469
36090-3506	2	106	469		102
	3	122	469		
Test 2	4	274	469		
02010-3523	5	274	469		
	1	160	57	110	68
Storm	2	56	57	110	68
Drains	3	160	58		
LF/Day	4	104	84		
	5	72	84		
Test 1	1	85			
02010-3523	2		67	173	67
	3	104	67	i	
Cest 2		180	67		
18731-3604	4	400	67	1	
	5	94	67		

the statistical fundamentals which were used to derive the models.

The models all appeared to provide reasonable prediction of actual production rates. In some cases the precision of the prediction was surprisingly good. However, it must be remembered that these are probabilistic models and as such can never make exact predictions. The reader is encouraged to review the listing of predicted and actual values of each observation used in the input data sets. This information is provided with the SAS regression output as Appendix C. Reviewing the complete list of observations provides a better feel for the possible range of variance between actual and predicted values.

Summary

This chapter presented an example of a trial application of the production rate modeling system to actual highway construction projects. A total of 60 projects were surveyed throughout the state of Florida. The data base used for model development contained 645 observations with measurements of 30 distinct influencing factors. From this data base production rate models were developed for five typical construction activities.

The model selection and regression solutions were performed with the assistance of computer software.

Following model development, each of the five models was checked with test data obtained from highway

construction projects. Test predictions indicated the models were producing reasonable output.

The next and final chapter will summarize the production rate modeling system and review important points recognized during this study. Also, a number of areas which present opportunities for future research will be discussed.

CHAPTER 9

SUMMARY AND CONCLUSIONS

Research Summary

Problem Statement

Production rate information is essential to many construction management functions. Estimating, planning, scheduling and resource management all depend upon production rate data. Inaccurate production rate information results in costly erroneous decisions by management.

In spite of the importance of accurate, timely production rate values, predicting construction productivity can be difficult. There are many factors which influence construction work rates. These many factors are subject to change and are as dynamic as the construction process itself. Each new project presents a seemingly new set of influencing factors. Traditional prediction methods, such as using historical averages, often provide misleading information.

Research Objective

The fundamental hypothesis of this study is that the variance in construction production rates results from a

large number of influencing factors. By identifying and measuring these influencing factors much of the variance can be explained. Using a data base of specifically structured field observations, a model for predicting future production rates can be developed.

The purpose of this research was to develop a factorial modeling system for improving the accuracy of production rate predictions, or more specifically to address each phase of the modeling system and to present those techniques which are most appropriate for use with construction production rate data. Finally, the modeling procedure was to be demonstrated with actual highway construction production rate data.

Summary

The production rate modeling system encompasses many considerations. Development must begin with an analysis of the construction process. Understanding the underlying process to be model is an essential prerequisite. Work activities must be identified and standards for production rate measuring must be established. The next step involves developing a list of preliminary construction production rate factors. The input of experienced field personnel is mandatory in identifying influencing factors. Design and implementation of a data collection system follows the preliminary studies. Development of the prediction model involves application of statistical regression procedures to the data base of observational

data. Verification and model testing conclude the modelling system.

Figure 35 presents a schematic flow chart of the modeling system. Because of the dynamic nature of the construction process, the production rate modeling system should be a continuous process. As new observational data is obtained, the model is updated to include the latest information.

Concusions

Validity of the Factorial Model

Discussion of the subject of modeling construction production rates was begun with the concept of the factorial model. That is that the production rate observed for a given activity is the combined result of a number of influencing factors. Identification and quantification of the influencing factors will allow for more precise predictions of production rates. The factorial model concept is a valid and useful approach to understanding and predicting construction production rates.

Need for a Comprehensive System

An organizational model for predicting construction production rates consists of a system with several components. These component modules include data collection, data management, factor selection, statistical

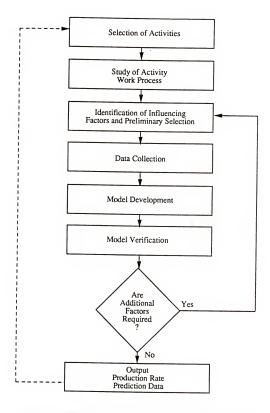


Figure 35. - Schematic Flow Chart of the Production Rate Modeling System

model development and reporting of output. Attention must be given to each of these areas.

Characteristics of Production Rate Data

Construction production rate data possesses several unique characteristics. First, the data are highly variable. Research also indicates that the data are typically non-normal with a pronounced skew to the higher values. Finally, analysis of the data collected in this study shows heterogeneous variances for the random error terms.

Statistical Modeling Procedures

Successful modeling of construction productions rates requires the careful selection and screening of influencing factors. Appropriate sample size can be estimated as approximately four times the number of independent variable combinations. This will allow sufficient data for both modeling and estimating the error component.

Heterogeneous variance problems were solved in the demonstration model by using logrythmic transformations. Even though the data were clearly not normally distributed, the least squares regression procedures did produce useful results.

Results of Model Demonstration

The application of the modeling system to an actual construction environment provided several interesting results. The model was successful in explaining a

significant portion of the overall variation. Much of the unexplained variation undoubtedly results from influencing factors which were not included in the model.

Organizational factors, for example, were not included. The owner did not know in advance which contracting organization would be performing the work. If the modeling system was applied within the context of a construction contracting organization, organizational factors could be included in the model. This certainly would greatly improve the prediction precision.

Of the influencing factors selected for inclusion in the demonstration, model, the total quantity of work for the activity appeared to be the largest affect. Projects with larger volumes of work experienced higher work rates. Perhaps a larger volume of work encourages the contractor to commit more resources to the work effort.

Applicability to Other Forms of Construction

This study concentrated on highway construction. However, there is no reason to believe that the factorial modeling concepts would not be completely appropriate for other construction categories such as building construction. The principles are the same. The only difference is that the influencing factors will be unique to the particular work setting.

Recommendations for Future Research

Development of a Reliable Listing of Influencing Factors

A great deal of basic research needs to be done in identifying and categorizing influencing factors for various construction activities and construction settings. If reliable listing of influencing factors were available, model development and initial data collection would be expedited. At this point, the modeling system must begin with exploratory procedures.

Expert Systems to Assist in Factor Section and Model Development

The process of factorial review and selection, and model development are prime candidates for expert systems. The proper application of current artificial intelligence technology to the production rate modeling system would significantly improve the cost-benefit ratio.

Advanced Statistical Methods

Even though acceptable results were obtained with the general linear model, many non-parametric statistical procedures have been developed. Different statistical procedures need to be tried and the results compared. Application of non-parametric and messy data techniques may provide additional model precision.

APPENDIX A EXAMPLE OF DATA COLLECTION FORMS



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GENERAL INSTRUCTIONS

- Select at least three projects. Try to pick different types of jobs such as new construction vs. reconstruction. Also, try to select jobs with different locations such as urban vs rural.
- The information required consist of one page of general information about the project and one survey page for each different work activity. (Additional forms have been enclosed for the EXCAVATION category because it may be that a single project will involve more than one type of excavation.)
- Field engineers should record contractor production quantities for all of the work items which are included in the project.
- 4. Return the forms as soon as they are completed to:

UNIVERSITY OF FLORIDA DEPARTMENT OF CIVIL ENGINEERING 346 WEIL HALL GAINESVILLE, FLORIDA 32611 ATTN: RALPH D. ELLIS, JR.

IF YOU HAVE ANY QUESTIONS OR NEED ANY ADDITIONAL INFORMATION PLEASE, TELEPHONE:

RALPH D. ELLIS, JR. (904) 392-1085 OR 622-1085 SUNCOM



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PROJECT GENERAL INFORMATION (Please, see instructions on reverse side.)

1	PROJECT TITLE:	
۷.	. STATE PROJECT JOB NO.:	
3.	TOTAL CONTRACT PRICE OF THE JOB: \$	-
4.	. THIS PROJECT WOULD BE CATEGORIZED AS:	-
	RECONSTRUCTION OF AN EXISTING ROAD CONSTRUCTION OF A NEW ROAD	
	IMPROVEMENTS TO AN INTERSECTION SIGNALIZATION BRIOGE	
	OTHER	
5.	THIS PROJECT IS LOCATED INCOUNTY	
6.	LOCAL CONDITIONS:	•
	RURAL URBAN LIMITED ACCESS ROAD (INTERSTATE)	
7.	TRAFFIC CONDITIONS:	
	LIGHT MEDIUM HEAVY	
8.	FDOT RESIDENT ENGINEEROAT	E: _

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(Please, see Instructions on reverse side.)

WORK ACTIVITY: CLEARING and GRUBBING

	acres
OBSERVED PRODUCTION QUANTITIES:	
TE: QUANTITY: TE: QUANTITY: TE: QUANTITY: TE: QUANTITY: TE: QUANTITY:	acres NO. HOURS WORKED:
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OTHEROTHER	



WORK ACTIVITY: EXCAVATION

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(Please, see Instructions on reverse side.)

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WORK ACTIVITY: BASE CONSTRUCTION

1. STATE PROJECT JOB NO.: _____

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(Please, see instructions on reverse side.)

2. 3.	TO HORK IN THE JOB:
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4.	TYPE OF MATERIAL SANO CLAY LIMEROCK SHELL STABILIZEO SOIL CEMENT ASPMALTIC BASE
5.	FACTORS WHICH HAD AN EFFECT ON PRODUCTION: WEATHER (RAIN) TRAFFIC INSUFFICIENT MANPOWER OR EQUIPMENT
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PHASING OF WORK REQUIRED BY CONTRACT

OTHER ______OTHER ______

6. FOOT PROJECT ENGINEER _____



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FIELD OBSERVATIONS
(Please, see instructions on reverse side.)

	CT JOB NO.:		
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Please see instructions

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APPENDIX B DATA BASE OF ACTIVITY OBSERVATIONS

Glossary of Variable Names Used in Data Base

Project Number	=	FDOT Project Number
Production Rate	=	Daily Observed Production Rate
F1 .	=	Total Activity Work Quantity
F2	=	Total Project Price
F3	=	Project Type: Reconstruction
F4	=	Project Type: Bridge
F5	=	Project Type: Intersection
F6	=	Project Type: New Construction
F7	=	Project Type: Signalization
F8	=	Project Location: Rural
F9	=	Project Location: Urban
F10	=	Project Location: Limited Access
F11	=	Traffic: Light
F12	=	Traffic: Medium
F13	=	Traffic: Heavy
C1	=	Light Clearing
C2	=	Medium Clearing
C3	=	Heavy Clearing
	=	Regular Excavation
	=	Latteral Ditch Excavation
	=	Subsoil Excavation
	= .	Sand Soil
	=	Rock Soil
	=	Muck Soil
	=	Sand-Clay Base
	=	Limerock Base
	=	Asphalt Base
	=	Small Area Pavement
	=	Depth of Sewer
ST2	=	Diameter of Sewer

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39 1 0 0 0 0 1 0 0 0 1 0 0 0	38	1	0												
40 1 0 0 0 0 0 0 0 0 0 0	39	1	0												
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OBS	PRO	JEC: IBER	r					OUCTION ACRES,	ON RAT	ΓE		F1	1	F2
41 42 43 44 45 46 47	487 487 487 487 530 530	31-3 31-3 31-3 31-3 31-3 31-3 30-3	3604 3604 3604 3604 3604 3510					6.58 0.13 0.13 0.13 0.29 1.70	30 70 30 30 90		82.2 0.8 0.8 0.8 0.8 172.0	50 50 50 50 50	209 209 209 209	
51 52 53 54 55 56 57 58 59	530 530 570 570 570 570 570 570 570	30-3 30-3 30-3 30-3 30-3 30-3 30-3 40-3 4	3510 3510 3548 3548 3548 3548 3548 3561 3561					1.70 1.00 0.75 2.70 4.50 0.90 1.80 0.04 0.02 0.05	00 00 50 00 00 00 00 00 00	2	172.00 172.00 172.00 210.00 210.00 210.00 210.00 0.42 0.42 0.42	00 00 00 00 00 00 00 00 27 27	7205 7205 7205 7678 7678 7678 7678 3734 3734 3734	5002 5002 5002 8699 8699 8699 8699 203
OBS	F3	F4	F5	F6	F7	F8	F9	F10	F11	F12	F13	C1	C2	СЗ
41 42 43 44 45 47 48 49 50 51 55 55 55 55 55 56 60	1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	000000000000000000000000000000000000000	0 1 1 1 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 1 1 1 1 1 1 1 1 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 0 0 0 0 0 1 1 1 1 1 1 1 1 0 0 0	0 1 1 1 0 0 0 0 0 0 0 0 0 0			0 1 1 1 1 1 1 1 1 1 1 1 1 1 0 0 0 0 0	1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		0111110000000000000011111	0 0 0 0 0 0 1 1 1 1 1 1 1 1 1 0 0

OBS		JEC:	Г					DUCTION ACRES	ON RA	ΓE	F1		F	2
61 62 63 64 65 66 67 68 69 70 71 72 73	570 605 605 605 702 702 702 720 720	040-0 580-0 580-0 580-0 580-0 580-0 220-0 200-0	3603 3603 3603 3603 3603 3429 3429 3429 3429 3429 3529				,	0.03 0.19 0.50 0.57 0.57 5.00 6.00 5.00 2.64	30 90 30 50 70 70 90 90 90 90 90 90	. 8 8 8	0.42° 2.170 2.170 2.170 2.170 2.170 32.840 32.840 32.840 32.840 36.900 56.900		37342 4063 4063 4063 4063 18861 18861 18861 18861 18861 18861	203 333 333 333 333 118 118 118 118 118
75 76 77 78 79 80	720 720 780 791 791 791	02-3 02-3 02-3 10-3 70-3 70-3	529 529 527 510					0.50 4.82 3.55 0.01 2.40 0.40	0 50 .8 00	5	56.900 56.900 0.036 9.735 9.735	0 4	5405 5405 3486 5634 5634 5634	341 341 38 01
OBS	F3	F4	F5	F6	F7	F8	F9	F10	F11	F12	F13	C1	C2	C3
61 62 63 64 65 66 67 71 72 73 74 75 77 78 80	01111100000000000001111	00000000000000000000	000000000000000000000000000000000000000	0 0 0 0 0 0 0 0 0 0 0 0 1 1 1 1	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	011110000000000000000000000000000000000	1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 1 1 1 1 0 0 0 0 0	0 1 1 1 1 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 1 1 1 1 0 0 0 0 0	1 0 0 0 0 0 0 0 0 0 0 1 1 1 1 1	000000000000000000000000000000000000000	1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 1 1 1 0 0 0 0 0 0 0 0 0

OBS		JECT IBER	r					OUCTION	ON RAT	Έ	F1		F	2
81		190-3						1.86	50		14.974	ı	7966	300
82	791	190-3	3505					2.32			14.974		7966	
83		190-3						1.5			14.974		7966	
84		190-3						0.17	78		14.974		7966	
85		190-3						0.83	32		14.974		7966	
86		55-3						0.40	0		15.000		8079	
87)55 - 3						0.40	0		15.000		8079	
88		55-3						1.30	0		15.000		8079	
89		55-3						0.30	0		15.000		8079	70
90		55-3						0.70	0	:	15.000) 1	8079	70
91		60-3						3.20	0	:	16.000	4	0391	37
92		60-3						4.50	0		16.000	4	0391	.37
93		60-3						1.60			16.000	4	0391	.37
94		60-3						1.60			16.000	4	0391	37
		60-3						5.10		1	16.000	4	0391	37
96	932	30-3	504					0.25	0		0.250		4134	19
OBS	F3	F4	F5	F6	F7	F8	F9							
ODS	13	14	rJ	10	F /	18	ry	F10	F11	F12	F13	C1	C2	C3
81	1	0	0	0	0	0	1	0	0	0	1	0	1	0
82	1	0	0	0	0	0	1	ō	ō	ō	ī	ő	ī	ő
83	1	0	0	0	0	0	1	0	ō	ō	ī	ō	ī	ŏ
84	1	0	0	0	0	0	1	0	ō	ō	ī	ō	ī	Ö
85	1	0	0	0	0	0	1	0	ō	ō	ī	ő	ī	Ö
86	1	0	0	0	0	0	1	0	0	Ó	1	ō	ī	ŏ
87	1	0	0	0	0	0	1	0	o	ō	1	ō	ī	ŏ
88	1	0	0	0	0	0	1	0	0	0	1	ō	1	ō
89	1	0	0	0	0	0	1	0	0	0	1	ō	1	ō
90	1	0	0	0	0	0	1	0	0	0	1	0	1	ō
91	1	0	0	0	0	0	1	0	0	1	0	ō	0	ī
92	1	0	0	0	0	0	1	0	0	1	0	0	ō	1
93	1	0	0	0	0	0	1	0	0	1	0	0	0	ī
94	1	0	0	0	0	0	1	0	0	1	0	0	0	1
95	1	0	0	0	0	0	1	0	0	1	0	0	0	1
96	1	0	0	0	0	1	0	0	0	1	0	0	1	Ω

DATA SET FOR EXCAVATION

0 20		OJE MBE						PR		TION Y/DA	RAT Y	E		F1			F2	
1	02	010	-35	32						81.0	^		_					
			-35											838			625	
			-35							88.0				838			625	
			-35							77.0				838			625	
			-35 -35							50.0				838			625	
										00.0			2	838			625	
7			-35							34.0			100	930	3	185	151	.00
			-35						4	89.0	0		100	930			151	
8			-35							99.0			100	930	3	185	151	.00
9			-35							75.0			100	930	3	185	151	.00
10			-35						1	78.0	0		100	930	3	185	151.	.00
11			-35						21	93.0	0		13	525			100	
12			-35						28	56.0	0		13	525			100	
13	10	160	-35	25					24	82.0	0			525			100.	
14	10	160	-35	25						56.0				525			100	
15	10	160	-35	25						89.0				525			100.	
16	11:	140	-35	07						91.0				843			775.	
17	11:	140	-35	07						33.0				843			775.	
18	11:	140	-35	7						19.0								
			-35							91.0				843			775.	
			-35							85.00				843			775.	
			55.	• •					•	85.00	J		5	843		345	775.	00
OBS	п э																	
	r s	F4	F5	F6	F7	FR	FG	F10	E11	E12	E12	E-1	Ea	П.		ъ-		
	r 3	F4	F5	F6	F7	F8	F9	F10	F11	F12	F13	E1	E2	ЕЗ	E4	E5	E6	
1	1	F4 0	F5 0															
			0	0	0	0	1	0	0	0	1	1	0	0	1	0	0	
1 2	1	0	0	0	0	0	1	0	0	0	1	1	0	0	1	0	0	
1 2 3	1 1 1	0	0 0 0	0	0	0	1 1 1	0 0 0	0 0 0	0 0 0	1 1 1	1 1 1	0	0	1 1 1	0	0 0	
1 2 3 4	1 1 1	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	1 1 1	0 0 0	0 0 0	0 0 0	1 1 1	1 1 1	0 0 0	0 0 0	1 1 1	0 0 0	0 0 0	
1 2 3 4 5	1 1 1 1	0 0 0	0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0	0 0 0	1 1 1 1	0 0 0	0 0 0 0	
1 2 3 4 5 6	1 1 1 1 0	0 0 0 0	0 0 0 0	0 0 0 0 0	0 0 0 0	0 0 0 0 0	1 1 1 1 0	0 0 0 0	0 0 0 0	0 0 0 0 0	1 1 1 1 0	1 1 1 1 1	0 0 0 0 0	0 0 0 0 0	1 1 1 1	0 0 0 0 0	0 0 0 0 0	
1 2 3 4 5 6 7	1 1 1 1 0 0	0 0 0 0 0	0 0 0 0 0	0 0 0 0 0	0 0 0 0 0	0 0 0 0 0	1 1 1 1 0 0	0 0 0 0 0 0	0 0 0 0 0	0 0 0 0 0	1 1 1 1 0	1 1 1 1 1	0 0 0 0 0	0 0 0 0 0	1 1 1 1 1	0 0 0 0 0 0	0 0 0 0 0 0	
1 2 3 4 5 6 7 8	1 1 1 1 0 0	0 0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 1 1	0 0 0 0 0 0	0 0 0 0 0 1 1	1 1 1 1 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 1 1	1 1 1 1 0 0	1 1 1 1 1 1	0 0 0 0 0 0	0 0 0 0 0 0	1 1 1 1 1 1	0 0 0 0 0 0	0 0 0 0 0 0 0	
1 2 3 4 5 6 7 8 9	1 1 1 1 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 1 1 1	0 0 0 0 0 0 0	0 0 0 0 1 1 1	1 1 1 1 0 0	0 0 0 0 0	0 0 0 0 0	0 0 0 0 0 1 1 1	1 1 1 1 0 0	1 1 1 1 1 1 1	0 0 0 0 0 0 0	0 0 0 0 0 0 0	1 1 1 1 1 1 1	0 0 0 0 0 0	0 0 0 0 0 0 0 0	
1 2 3 4 5 6 7 8 9	1 1 1 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 1 1 1	0 0 0 0 0 0 0 0	0 0 0 0 0 1 1 1	1 1 1 1 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 1 1 1 1	1 1 1 1 0 0 0	1 1 1 1 1 1 1 1 1	0 0 0 0 0 0	0 0 0 0 0 0	1 1 1 1 1 1	0 0 0 0 0 0	0 0 0 0 0 0 0 0 0	
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1 2 3 4 5 6 7 8 9 10 11	1 1 1 0 0 0 0 0	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0	0 0 0 0 1 1 1 1	0 0 0 0 0 0 0 0 0	0 0 0 0 0 1 1 1 1 0	1 1 1 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 1 1 1 1 0	1 1 1 1 0 0 0 0 0	1 1 1 1 1 1 1 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	1 1 1 1 1 1 1	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0	
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1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	1 1 1 1 0 0 0 0 0 0 0 0	0000000000000	00000000000000	0 0 0 0 0 1 1 1 1 1 1 1	000000000000000000000000000000000000000	0 0 0 0 0 1 1 1 1 0 0 0	1 1 1 1 0 0 0 0 0 1 1 1 1	0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 1 1 1 1 0 0	1 1 1 1 0 0 0 0 0	1 1 1 1 1 1 1 1 0 0	0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0	1 1 1 1 1 1 1 1 0 0	0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0	
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	1 1 1 1 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 1 1 1 1 1 1 1 1	000000000000000000000000000000000000000	0 0 0 0 0 0 1 1 1 1 1 0 0 0 0	1 1 1 1 0 0 0 0 0 1 1 1 1	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 1 1 1 1 0 0	1 1 1 1 0 0 0 0 0 0	1 1 1 1 1 1 1 0 0	0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0	1 1 1 1 1 1 1 0 0	0 0 0 0 0 0 0 0 0 0 0	000000000000000000000000000000000000000	
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	1 1 1 1 0 0 0 0 0 0 0 0 0 0 1 1	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		0 0 0 0 0 1 1 1 1 1 1 1	000000000000000000000000000000000000000	0 0 0 0 0 1 1 1 1 0 0 0	1 1 1 1 0 0 0 0 0 1 1 1 1	0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 1 1 1 1 0 0	1 1 1 1 0 0 0 0 0	1 1 1 1 1 1 1 1 1 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	1 1 1 1 0 0 0 0 0 0 0 0 0 0 1 1 1 1	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 1 1 1 1 1 1 1 1	000000000000000000000000000000000000000	0 0 0 0 0 0 1 1 1 1 1 0 0 0 0	1 1 1 1 0 0 0 0 0 1 1 1 1	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 1 1 1 1 0 0 0 0	1 1 1 1 0 0 0 0 0 1 1 1 1	1 1 1 1 1 1 1 1 1 1 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 1 1 1 1 1 1	1 1 1 1 1 1 1 1 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	1 1 1 1 0 0 0 0 0 0 0 0 0 0 1 1	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		0 0 0 0 0 1 1 1 1 1 1 1 1 1 0 0	000000000000000000000000000000000000000	0 0 0 0 0 0 1 1 1 1 1 0 0 0 0 0	1 1 1 1 0 0 0 0 0 0 1 1 1 1 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 1 1 1 1 0 0 0 0 0	1 1 1 0 0 0 0 0 1 1 1 1 0 0	1 1 1 1 1 1 1 1 1 1 0 0 0 0	000000000000000000000000000000000000000	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	

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DATA SET FOR EXCAVATION

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OBS		OJE MBE						PRO		ION /DAY		Έ		F1		F	2	F3
21	10	005		0.7														
21			-35							1.30				568		339	858	0
23			-35							7.70				568		339	858	0
			-35							3.23				568		339		0
24 25			-35 -35							8.09				568		339		0
			-35 -35							3.19				568		339		0
27			-35 -35							2.00				829		369	359	1
			-35 -35							0.00				829		369		1
			-35 -35							6.00				118		465		1
			-35 -35							4.00				118		465		1
31			-35 -35							5.00				118		465		1
32			-35 -35							4.00				118		465		1
33			-35 -35							3.00				118		4655		1
			-35							1.00				341		997		0
			-35							7.00				341		9974		0
			-35							3.00				341		9974		0
			-35							9.00				341		9974		0
			-36							7.00				341		9974		0
			-36							4.00				546		1436		0
			-360							4.00				546		1436		0
-10	30.	,,,	300	,,					6.	2.00			-	546		1436	584	0
OBS	F4	F5	F6	F7	F8	F9	F10	F11	F12	F13	E1	E2	E3	E4	E5	E6		
21	0	0	0	1	0	1	0	0	0	1	1	0	0	0	1	0		
22	0	0	0	1	0	1	0	ō	ō	ī	1	ő	ő	ő	1	0		
23	0	0	0	1	0	1	ō	ō	ō	î	ī	ō	ő	ő	1	0		
24	0	0	0	1	0	1	0	0	ō	ī	ī	ō	ő	ő	ī	0		
25	0	0	0	1	0	1	0	0	ō	ī	î	ō	ő	Ö	1	0		
26	0	0	0	0	0	1	0	0	ō	ī	ō	ő	ĭ	1	ō	0		
27	0	0	0	0	0	1	0	ō	ō	î	ő	ő	ī	ō	0	1		
28	0	0	0	0	1	0	ō	1	ō	ō	1	ő	ō	1	0	ō		
29	0	0	0	0	1	0	0	1	ō	ō	î	ő	ő	ī	0	ő		
30	0	0	0	0	1	0	0	1	ō	ō	ī	ő	ő	ī	0	ő		
31	0	0	0	0	1	0	ō	ī	Ö	Ö	ī	o	ŏ	1	0	0		
32	0	0	0	0	1	0	0	1	ō	ő	ī	ő	ő	i	Ö	0		
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OBS		OJE						PRO		ION		E						
020									CY	/DAY				F1		F	2	F3
41		570							1	24.0	0			646		1436	584	0
42		570								62.0	0			646		1436		ő
43	46	040	-35	45						73.0				773		1825		ő
44	48	060	-35	06						00.0			268			0265		1
45	48	060	-35	06						00.0			268			0265		1
46	48	060	-35	06						00.0			268			0265		1
47	48	060	-35	06						00.0			268			0265		1
48	48	731	-36	04						02.0				404		2093		
49	48	731	-36	04						00.0				404		2093		0
50	48	731	-36	04						00.0				404		2093		0
51	53	030	-35	10						00.0				404 680				0
		030								80.0				680		2050		0
53	53	030	-35	10						00.0				680		2050		0
		030								00.0						2050		0
		030								00.0				680		2050		0
		020								23.3				680		2050		0
		020								23.3 11.6				231		2355		1
		020												231		2355		1
		020								58.4				231		2355		1
		020								46.0				231		2355		1
00	550	020	-33	19						91.5	2		- 2	231	- 2	2355	12	1
OBS	F4	F5	F6	F7	FΩ	FO	E10	E11	E1.0	T1 1								
				.,	10	19	rio	FII	F12	F13	EI	E2	E3	E4	E5	E6		
41	0	1	0	0	1	0	0	1	0	0	1	0	0	1	0	0		
42	0	1	0	0	1	0	0	1	0	0	1	0	0	1	0	0		
43	0	0	0	0	0	0	0	0	0	1	1	0	0	1	ō	ō		
44	0	0	0	0	1	0	0	0	0	1	1	0	0	0	ō	ō		
45	0	0	0	0	1	0	0	0	0	1	1	0	ō	ō	ō	ō		
46	0	0	0	0	1	0	0	0	0	1	1	0	ō	ō	ō	ō		
47	0	0	0	0	1	0	0	0	0	1	1	Ó	ō	ō	ō	ō		
48	0	1	0	0	0	1	0	0	1	0	ī	0	ō	1	ō	ő		
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50	0	1	0	0	0	1	0	Ó	ī	ō	ī	ő	ō	ī	ő	ō		
51	0	0	1	0	1	0	0	0	ī	o	ī	o	ō	ō	ŏ	Ö		
52	0	0	1	0	1	0	Ó	ō	ī	ō	ī	o	Ô	o	a	Ö		
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DATA SET FOR EXCAVATION

obs		OJE MBE						PRO		ION /DAY		E	F	1		F	2	F3
61		040								61.6			4	435	1	194	647	1
62		040							2	87.2	2		4	435	1	194	647	1
63		040							3	68.6	4		4	435	1	194	647	1
64		040							3	61.6	9		4	435	1	194	647	1
65	55	040	-35	25					2	89.1	8		4	435			647	ī
66	57	030	-35	48						00.0			310				699	ō
67	57	030	-35	48						51.0			310					
68	57	030	-35	48						81.0							699	0
		030											310			678		0
		030								81.0			310			678		0
		040								32.0			310			678	699	0
										88.0				331	3	954	939	1
		040								59.0			8	331	3	954	939	1
		040							5	47.0	0		8	331	3	954	939	1
		040								60.0	0		8	331	3	954	939	1
		040							2	17.0	0		8	331		954		1
76	57	080	-35	05					6	02.0	n		1.8	514		277		ī
77	570	080	-35	05						95.0				514		277		1
78	570	080	-35	05						17.0				514		277		
79	570	080-	-35	05						96.00								1
		080-								56.00				514		277		1
				-					5.	36.00	J		18	514	1.	277	510	1
OBS	F4	F5	F6	F7	F8	F9	F10	F11	F12	F13	E1	E2	ЕЗ	E4	E5	E6		
61	0	0	0	0	0	0	0	0	0	0	1	0	0	1	0	0		
62	0	0	0	0	0	0	ō	ō	ō	ō	ī	ő	0	ī				
63	0	0	ō	0	ō	ō	ō	ō	Ö	0	1	0	-		0	0		
64	0	0	ō	ō	ō	o	ō	Ö	Ö	o	1		0	1	0	0		
65	0	ō	ō	ō	ő	ō	ō	0	0			0	0	1	0	0		
66	ō	o	ĭ	ő	1	0	0	0	-	0	1	0	0	1	0	0		
67	ō	ő	ī	0	1				1	0	1	0	0	1	0	0		
68	0	0	1	0		0	0	0	1	0	1	0	0	1	0	0		
	-				1	0	0	0	1	0	1	0	0	1	0	0		
69	0	0	1	0	1	0	0	0	1	0	1	0	0	1	0	0		
70	0	0	1	0	1	0	0	0	1	0	1	0	0	1	0	0		
71	0	0	0	0	0	1	0	0	0	1	1	0	0	1	0	ō		
72	0	0	0	0	0	1	0	0	0	1	1	ō	ō	ī	ō	ō		
73	0	0	0	0	0	1	0	0	0	1	ī	ō	ō	ī	o	ō		
74	0	0	0	0	0	1	0	ō	ō	ī	ī	ō	ő	î	ō	ő		
75	0	0	0	ō	ō	ī	ō	ō	ő	ī	i	0	o	1	0			
76	ō	ō	ō	ō	ĭ	ō	ō	0	1	0	0					0		
77	0	ō	ō	ő	ī	0	0	0	1		-	1	0	1	0	0		
78	ō	ő	ő	0	1	0	0			0	0	1	0	1	0	0		
79	ō	ő	0	0	1	0	_	0	1	0	0	1	0	1	0	0		
80	0	0	0	0	1	0	0	0	1	0	0	1	0	1	0	0		
30	U	U	U	U	т	U	0	0	1	0	0	1	0	1	0	0		

F3

DATA SET FOR EXCAVATION

OBS		OJE MBE						PRO	DUCT	ION /DAY		E	F	1		F2	
81			-35						123	8.00			197	24	18	59693	3
82	61	080	-35	24					140	5.00			197			59693	
83			-35						153	9.13			197			59693	
84	61	080	-35	24						2.00			197			59693	
85	61	080	-35	24					137	2.00			197			59693	
86	72	002	-35	29						0.00			911			40541	
87	72	002	-35	29						0.00			911			40541	
88	72	002	-35	29						5.00			911			40541	
89	72	002	-35	29						5.00			911			40541	
90	72	002	-35	29						0.00			911			40541	
91	76	020	-35	18						7.00			68			27986	
92	76	020	-35	18						0.00			68			27986 27986	
93	78	010	-35	27						6.63			13			48638	
94			-35							7.30			13			48638	
95	79	170	-35	10						4.00			111			40038 63401	
96			-35							3.00			111			63401 63401	
97	79	170-	-35	10						1.00			111			63401 63401	
98			-35							4.00			111				
99			-35						12.	*.00						63401	
100			-350						22.	7.20			111: 34:			63401	
									22	7.20			34	/ 1	/	96699	
OBS	F4	F5	F6	F7	F8	F9	F10	F11	F12	F13	E1	E2	E3	E4	E5	E6	
81	0	0	0	0	1	0	0	0	1	0	0	0	1	0	0	1	
82	0	0	0	0	1	0	0	0	1	0	0	o	ī	ō	ō	ī	
83	0	0	0	0	1												
84	0	0			_	0	0	0	ī	0	ő	0			_	1	
85		-	0	0	ī	0	0	0					1	0	0	1	
86	0	ō	0	0					1	0	0	0	1	0	0	1	
	0	0	0	0	1	0	0	ō	1	0	0	0	1	0	0	1	
87	0	0	0 1 1	0	1	0	0	0	1 1 1	0 0 0	0	0	1 1 0	0 0 0	0 0 0	1 1 0	
87 88	0	0 0 0	0 1 1 1	0 0 0	1 1 0	0	0	0	1 1 0	0 0 0	0 0 0 1	0 0 0	1	0 0 0 1	0 0 0	1 0 0	
87 88 89	0 0 0	0 0 0 0	0 1 1	0	1 0 0	0 0 0	0 0 0	0 0 0	1 1 0 0	0 0 0 1	0 0 0 1 1	0 0 0 0	1 1 0 0	0 0 0 1 1	0 0 0 0	1 0 0 0	
87 88 89 90	0 0 0 0	0 0 0	0 1 1 1	0 0 0	1 0 0 0	0 0 0	0 0 0 0	0 0 0 0	1 1 0 0	0 0 0 1 1	0 0 0 1 1 1	0 0 0 0 0 0	1 1 0 0 0	0 0 0 1 1 1	0 0 0 0 0 0	1 0 0 0	
87 88 89 90	0 0 0	0 0 0 0	0 1 1 1	0 0 0 0	1 0 0 0	0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0	1 1 0 0 0	0 0 0 1 1 1	0 0 0 1 1 1 1 1 1	0 0 0 0 0 0 0	1 1 0 0 0 0	0 0 0 1 1 1 1 1 1	0 0 0 0 0 0	1 0 0 0 0	
87 88 89 90	0 0 0 0	0 0 0 0 0	0 1 1 1 1	0 0 0 0 0	1 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0	1 1 0 0 0 0	0 0 0 1 1 1 1	0 0 0 1 1 1 1 1 1 1 1	0 0 0 0 0 0 0 0	1 1 0 0 0 0	0 0 0 1 1 1 1 1 0	0 0 0 0 0 0 0 1	1 0 0 0 0 0	
87 88 89 90	0 0 0 0 0	0 0 0 0 0 0	0 1 1 1 1 1 0	0 0 0 0 0 0	1 0 0 0 0	0 0 0 0 0 0 1	0 0 0 0 0 0 0	0 0 0 0 0 0	1 1 0 0 0 0	0 0 0 1 1 1 1	0 0 0 1 1 1 1 1 1 1 1 1	0 0 0 0 0 0 0 0	1 1 0 0 0 0 0	0 0 0 1 1 1 1 0 0	0 0 0 0 0 0 0 1 1	1 0 0 0 0 0 0	
87 88 89 90 91 92 93	0 0 0 0 0 0	0 0 0 0 0 0 0	0 1 1 1 1 0 0	0 0 0 0 0 0	1 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0	1 1 0 0 0 0 0	0 0 0 1 1 1 1 1 1	0 0 0 1 1 1 1 1 1 1 1 1 1	0 0 0 0 0 0 0 0 0	1 1 0 0 0 0 0 0 0 0 0	0 0 0 1 1 1 1 0 0 1	0 0 0 0 0 0 0 1 1 0	1 0 0 0 0 0 0	
87 88 89 90 91 92 93	0 0 0 0 0 0 0	0 0 0 0 0 0 0 1 1 0	0 1 1 1 1 0 0	0 0 0 0 0 0 0	1 0 0 0 0 0 0	0 0 0 0 0 0 0 1 1	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0	1 1 0 0 0 0 0 0	0 0 0 1 1 1 1 1 1	0 0 0 1 1 1 1 1 1 1 1 1 1 1	0 0 0 0 0 0 0 0 0	1 1 0 0 0 0 0 0 0 0 0 0 0	0 0 0 1 1 1 1 0 0 1 1	0 0 0 0 0 0 0 0 1 1 0 0	1 0 0 0 0 0 0 0	
87 88 89 90 91 92 93	0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 1 1 1 1 0 0 0	0 0 0 0 0 0 0 0	1 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 1 1 1	0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0	1 1 0 0 0 0 0 0	0 0 0 1 1 1 1 1 1 1 1	0 0 0 1 1 1 1 1 1 1 1 1 1 1 1 1	0 0 0 0 0 0 0 0 0 0	1 1 0 0 0 0 0 0 0 0 0 0 0	0 0 0 1 1 1 0 0 1 1 1	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 0 0 0 0 0 0 0 0	
87 88 89 90 91 92 93 94 95	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 1 1 0	0 1 1 1 1 0 0 0 0	0 0 0 0 0 0 0 0 0	1 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 1 1 1	0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0	1 1 0 0 0 0 0 0 0	0 0 0 1 1 1 1 1 1 1 1 1 1	0 0 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0 0 0 0 0 0 0 0 0 0 0	1 1 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 1 1 1 1 0 0 1 1 1 1	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 0 0 0 0 0 0 0 0	
87 88 89 90 91 92 93 94 95 96 97 98	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 1 1 0 0	0 1 1 1 1 0 0 0 0	0 0 0 0 0 0 0 0 0	1 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 1 1 1 1 1 1 1	0 0 0 0 0 0 0 0 0 0 0 0	000000000000000000000000000000000000000	1 1 0 0 0 0 0 0 0 0 0	0 0 0 1 1 1 1 1 1 1 1	0 0 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	00000000000000	1 1 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 1 1 1 1 1 1 1 1 1 1 1	0 0 0 0 0 0 0 0 0 0 0 0 0	1 0 0 0 0 0 0 0 0 0 0	
87 88 89 90 91 92 93 94 95 96	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 1 1 0 0 0	0 1 1 1 1 0 0 0 0 0	000000000000	1 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 1 1 1 1 1 1 1 1 1	0 0 0 0 0 0 0 0 0 0 0 0	000000000000000000000000000000000000000	1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 1 1 1 1 1 1 1 1 1 1 1	0 0 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0 0 0 0 0 0 0 0 0 0 0	1 1 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 1 1 1 1 0 0 1 1 1 1	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 0 0 0 0 0 0 0 0	

F3

DATA SET FOR EXCAVATION

obs		OJE MBE						PRODUCTION RATE CY/DAY					F1			F2	
0BS 101 102 103 104 105 106 107 108 109 110 111 112	79 79 79 79: 79: 79: 79: 87: 87: 87:	190 190 190	-35 -35 -35 -35 -35 -35 -36 -36 -36	05 01 01 01 01 01 01 01				CY/DAY 374.37 1116.90 36.88 40.90 319.90 428.30 239.90 319.90 1400.00 1700.00 1000.00 600.00					F1 3471 3471 2185 2185 2185 2185 16263 16263 16263			796699 796699 796699 392641 392641 392641 392641 1807970 1807970	
OBS	F4	F5		_	F8	F9	F10	F11	F12	0.00 F13	E1	E2	162 E3		180 E5	D7970 E6	
101 102 103 104 105 106 107 108 109 110 111	000000000000000000000000000000000000000	0 0 0 0 0 0 0 0 0 0	000000000000	0 0 0 0 0 0 0 0 0 0	0 0 0 1 1 1 1 0 0 0	1 1 0 0 0 0 0 1 1 1	0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 1 1 1 1 0 0 0	1 1 0 0 0 0 0 1 1 1	1 1 1 1 1 1 1 1 1 1 1 1 1	0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0	1 1 1 1 1 1 1 1 1 1 1 1	0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	

OBS		JEC IBER	r				PROD	UCTION SY/D	N RATE AY	1	F1		F2	
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	NUM 0200 0200 0200 0200 0200 0200 0200 1000 1000 1001 1001 1001 1001	MBER 010-3 010-3 010-3 010-3 010-3 020-3 020-3 020-3 020-3 060-3 060-3	3517 3523 3532 3532 3532 3532 3513 3513 3513				PRODU	SY/Da 1024 1024 146 40 889 1293 1053 1053 1053 1046 388 4000 2400 6400 6400	AY .00 .00 .00 .00 .00 .00 .00 .00 .00 .0	14 14 14 10 10 10 10 10 10 10 10 10 10 10 10 10	1793 1793 1590 1590 1590 185 185 185 185 1793 1793 1793	177 177 177 177 3185 3185 3185 3185 3185 4319 4319 4319 4319	2002 7625 7625 7625 7625 7625 5151 5151 5151 5151 5151 5150 100 100	.00 .00 .00 .00 .00 .00 .00 .00 .00 .00
19	120	05-3 05-3 05-3	507					328. 363. 680.	60	4	243 243 243	339	858. 858. 858.	00
OBS	F3	F4	F5	F6	F7	F8	F9	F10	F11	F12	F13	В1	В2	В3
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	0 1 1 1 1 0 0 0 0 0	000000000000000000000000000000000000000	.00000000000000000000000000000000000000	000000000000000000000000000000000000000	000000000000000000000000000000000000000	000000000000000000000000000000000000000	1 1 1 1 0 0 0 0 0	000000000000000000000000000000000000000	000000000000000000000000000000000000000	0 0 0 0 0 1 1 1 1 1 0	0 0 1 1 1 1 1 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
16 17 18 19 20	0 0 0	0 0 0 0	0 0 0 0	1 0 0 0	0 0 1 1	0 0 0 0	1 1 1 1 1 1	0 0 0	0 0 0 0	0 0 0	1 1 1 1 1	0 0 0 0	1 1 0 0	0 0 1 1

OBS		JEC:	r				PROI	OUCTION SY/I		re	F1		F2	
21 22 23 24 25 26 27 28 29 30 3.1 32 33 34 35 36 37 38 39 40	120 120 165 165 165 300 300 300 350 350 350 350	005-0 005-0 120-0 110-0 110-0 30-0 30-0 30-0 30-0 30-0	3507 3534 3534 3605 3605 3605 3605 3506 3506 3506 3506					180 153 227 2501 2889 10923 3326 2389 2716 2323 1920 2409 1794 1794 2172 1936	0.45 3.74 1.00 7.00 1.00	. 11 11 12 55 55	4243 4243 26192 26192 26192 26192 26192 29391 9391 9391 9391 2960 8524 8524 8524 8524	13 12 12 12 12 14 14 14 14 14 16 16	33985 33985 33985 25068	58 59 59 30 30 30 30 30 30 44 44 42 55 55 55 55
OBS	F3	F4	F5	F6	F7	F8	F9	F10	F11	F12	F13	В1	В2	В3
21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38	0 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	000000000000000000000000000000000000000	000000000000000000000000000000000000000	110000000000000000000000000000000000000	0 0 0 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	111100000000000000000000000000000000000	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 1 1 1 1 0 0 0 0 0	1 1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	000000000000000000000000000000000000000	0 0 0 0 0 0 0 0 0 1 1 1 1 1 1	1 1 1 1 1 1 1 0 0 0 0 0 0 0

OBS		JEC BER	r				PRO	DUCTION SY/	ON RAT	ΓE	F1		F	2
41		50-3						2844	.00		19961		29974	176
42	353	50-3	3502					333			19961		29974	
43	353	50-3	3502					1422			19961		29974	
44	353	50-3	3502					1011			19961		29974	
45	353	50-3	3502					127			19961			
46		60-3						1024			19961	•	29974	1/6
47		60-3												•
48		60-3						1024.			•			•
49		70-3						1024.						•
50		70-3						253.			4706		1436	
51								353.			4706		1436	84
		70-3						232.			4706		1436	84
52		70-3						174.	.00		4706		1436	84
53		70-3						140.	.00		4706		1436	
54		10-3						2250.	.00		22960			
55	370	10-3	512					2600.	.00		22960			•
		10-3						2900.			22960			•
57	370	10-3	512					1980.			22960			•
58	460	40-3	545					903.			1188		1825	7.
59	460	40-3	545					97.			1188			
		60-3						1139.					1825	
								1139.	.00		87098	4	0265	96
OBS	F3	F4	F5	F6	F7	F8	F9	F10	F11	F12	F13	В1	В2	вз
41	0	0	0	1	0	1	0	0	0	0	1	0	1	0
42	0	0	0	1	0	1	0	0	ō	ō	ī	ō	ī	ő
43	0	0	0	1	0	1	0	0	Ō	ō	ī	ō	ī	ō
44	0	0	0	1	0	1	ō	ō	ō	ő	ī	ő	ī	ő
45	0	0	0	1	0	ī	ō	ő	ō	ő	1	0	1	0
46						-			-	-	ō	0	0	0
47							:		•	•	ŏ	0		
48					·	:		•	•	•	0	-	0	0
49	ō	ō	i	ò	ò	i	ò	ò	i			0	0	0
50	ő	ő	ī	ő	ő	1	0			0	0	0	1	0
51	ő	ō	ī	Ö	o	1		0	1	0	0	0	1	0
52	0	o	ī	0	_		0	0	1	0	0	0	1	0
53	0	0	1		0	1	0	0	1	0	0	0	1	. 0
	-	-		0	0	1	0	0	1	0	0	0	1	0
54	•	•	•	•	•	•		•			0	0	1	0
55	•	•	•	•	•	•					0	0	1	0
56	•	•	•		•						0	0	1	0
57	•	•									0	0	1	ō
58	0	0	0	0	0	0	0	0	0	0	ī	ō	ō	1
59														
60	0	0	0	ō	ō	ō	ő	ŏ	ŏ	Ö	i	o	0	1

OBS	PRO	JECT BER	?				PROI	OUCTIO SY/I		ΓE	F1		F2	!
61 62		60 - 3						2314. 4789.			87098 87098		0265	
63	480	60-3	506					1634.			87098		0265	
64	480	60-3	506					3675.			87098		0265	
65	487	31-3	604					306.			1823	*	2093	
66	487	31-3	604					338.			1823		2093	
67		31-3						152.			1823		2093	
68		31-3						485.			1823		2093	
69		30-3						168.		_	1823 275165	-		
70		30-3						78.			275165 275165		2050	
71		30-3						2000.			75165		2050	
72		30-3						2635.					2050	
73		30-3						2234.			75165		2050	
74		20-3						55.		2	75165	/	2050	
75		20-3									588		2355	
76		20-3						55.			588		2355	
77		20-3						163.			588		2355	
78		20-3						130.			588		2355	
79		40-3						184.			588	_	2355	
80		40-3						3117.			44089		1946	
30	330	40-3	323					4500.	00		44089	1	1946	47
OBS	F3	F4	F5	F6	F7	F8	F9	F10	F11	B10				
000	13		13	10	Ι,	10	ry	FIU	FII	F12	F13	В1	B2	вз
61	1	0	0	0	0	1	0	0	0	0	1		0	0
62	1											0	0	
63				0	0	1	0	0	0	O	1	0	o	0
	1	0	0	ō	ō	1	ō	Ō	0	0	1			0
64	1	0	0	0	0	1	0	0	0 0 0	0 0	1 1 1	0	0 0 0	0
65	1	0	0 0 1	0	0	1 0	0 0 1	0	0 0 0	0 0 0	1 1 1 0	0 0 0	0	0 0 1
65 66	1 0 0	0 0 0	0 0 1 1	0 0 0	0 0 0	1 1 0 0	0 0 1 1	0 0 0	0 0 0 0	0 0 0 1	1 1 0 0	0 0 0 0	0 0 0 0	0 0 1 1
65 66 67	1 0 0	0 0 0 0	0 0 1 1	0 0 0	0 0 0 0	1 0 0	0 0 1 1 1 1	0 0 0	0 0 0 0	0 0 0 1 1	1 1 0 0	0 0 0	0 0 0 0	0 0 1
65 66 67 68	1 0 0 0 0	0 0 0 0 0	0 0 1 1 1	0 0 0 0 0	0 0 0 0 0	1 0 0 0	0 0 1 1 1 1 1	0 0 0 0 0	0 0 0 0 0	0 0 0 1 1 1	1 1 0 0 0	0 0 0 0	0 0 0 0 0 0	0 0 1 1 1
65 66 67 68 69	1 0 0 0 0	0 0 0 0 0 0	0 0 1 1 1 1	0 0 0 0 0 0 1	0 0 0 0 0 0	1 0 0 0 0	0 0 1 1 1 1 1 0	0 0 0 0 0 0 0 0	0 0 0 0 0	0 0 0 1 1 1 1 1 1 1	1 1 0 0	0 0 0 0 0	0 0 0 0	0 0 1 1
65 66 67 68 69 70	1 0 0 0 0 0	0 0 0 0 0 0 0	0 0 1 1 1 0 0	0 0 0 0 0 0	0 0 0 0 0 0	1 0 0 0 0 0	0 0 1 1 1 1 0 0	0 0 0 0 0 0 0 0 0	0 0 0 0 0	0 0 0 1 1 1	1 1 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0	0 0 1 1 1
65 66 67 68 69 70	1 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 1 1 1 0 0	0 0 0 0 0 0	0 0 0 0 0 0 0 0	1 0 0 0 0 1 1	0 0 1 1 1 1 0 0 0 0	0 0 0 0 0 0 0 0 0 0	0 0 0 0 0	0 0 0 1 1 1 1 1 1 1 1 1 1 1 1	1 1 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0	0 0 1 1 1 1
65 66 67 68 69 70 71 72	1 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0	0 0 1 1 1 0 0	0 0 0 0 0 0 0 1 1 1	0 0 0 0 0 0 0 0 0	1 1 0 0 0 0 1 1 1	0 0 1 1 1 1 0 0	0 0 0 0 0 0 0 0 0	0 0 0 0 0	0 0 0 1 1 1 1 1 1 1 1 1	1 1 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0	0 0 1 1 1 1 0
65 66 67 68 69 70 71 72 73	1 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0	0 0 1 1 1 0 0 0	0 0 0 0 0 0 0 1 1 1	0 0 0 0 0 0 0 0 0	1 0 0 0 0 1 1 1	0 0 1 1 1 1 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 1 1 1 1 1 1 1 1 1 1 1 1	1 1 0 0 0 0	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 1 1	0 0 1 1 1 1 0 0
65 66 67 68 69 70 71 72 73	1 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0	0 0 1 1 1 0 0 0 0	0 0 0 0 0 0 1 1 1 1 1 0	0 0 0 0 0 0 0 0 0 0	1 1 0 0 0 0 1 1 1 1 1 0	0 0 1 1 1 1 0 0 0 0 0 0 1	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 1 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 1 1 1 1	0 0 1 1 1 1 0 0
65 66 67 68 69 70 71 72 73 74	1 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0	0 0 1 1 1 0 0 0 0	0 0 0 0 0 0 1 1 1 1 1 0 0	0 0 0 0 0 0 0 0 0 0 0	1 1 0 0 0 1 1 1 1 0 0	0 0 1 1 1 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 1 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 1 1 1	0 0 1 1 1 1 0 0 0
65 66 67 68 69 70 71 72 73 74 75	1 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0	0 0 1 1 1 0 0 0 0 0	0 0 0 0 0 0 1 1 1 1 0 0 0 0	000000000000000000000000000000000000000	1 1 0 0 0 1 1 1 1 0 0 0 0	0 0 1 1 1 0 0 0 0 0 1 1 1 1	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 1 1 1 1 1 1 1 1 1 1 1 1 0	1 1 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 1 1 1 1	0 0 1 1 1 0 0 0 0
65 66 67 68 69 70 71 72 73 74 75 76	1 0 0 0 0 0 0 0 0 0	000000000000000000000000000000000000000	0 0 1 1 1 0 0 0 0 0	0 0 0 0 0 0 1 1 1 1 0 0 0 0 0	000000000000000000000000000000000000000	1 0 0 0 0 0 1 1 1 1 0 0	0 0 1 1 1 0 0 0 0 0 1 1 1 1 1	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 1 1 1 1 1 1 1 1 1 1 1 0 0 0	1 1 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 1 1 1 1	0 0 1 1 1 0 0 0 0
65 66 67 68 69 70 71 72 73 74 75 76 77	000000000000000000000000000000000000000	000000000000000000000000000000000000000	0 0 1 1 1 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0	000000000000000000000000000000000000000	1 1 0 0 0 0 1 1 1 1 0 0 0 0 0 0	0 0 1 1 1 0 0 0 0 1 1 1 1 1 1 1	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 1 1 1 1 1 1 1 1 1 1 1 0 0 0 0	1 1 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 1 1 1 1 1	0 0 1 1 1 0 0 0 0 0
65 66 67 68 69 70 71 72 73 74 75 76	1 0 0 0 0 0 0 0 0 0	000000000000000000000000000000000000000	0 0 1 1 1 0 0 0 0 0	0 0 0 0 0 0 1 1 1 1 0 0 0 0 0	000000000000000000000000000000000000000	1 0 0 0 0 0 1 1 1 1 0 0	0 0 1 1 1 0 0 0 0 0 1 1 1 1 1	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 1 1 1 1 1 1 1 1 1 1 1 0 0 0 0 0	1 1 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 1 1 1 1 1 1	0 0 1 1 1 0 0 0 0 0

OBS	PRO	JEC:	r			1	PRODU	JCTION SY/D	N RATE		F1		F2	
81		40-3						930.0		44	1089.0	11	19464	17
82		40-3					5	5950.0	00	44	1089.0	11	19464	17
83		40-3					3	3300.0	00	44	1089.0	11	19464	17
		80-3						1794.0		4 (0854.0	21	L6381	.7
		80-3					3	987.0	00	40	0854.0	21	16381	.7
		80-3					4	746.0	00	40	0854.0	21	L6381	7
87		80-3					3	778.0	00	40	854.0	21	L6381	.7
		80-3					2	503.0	00	40	854.0	21	16381	7
89		30-3						917.0	00	236	916.0	76	7869	19
		40-3						70.0	00	9	765.0	39	5493	9
91		40-3						91.0	00	9	765.0		5493	
92		40-3						261.0	00		765.0		5493	
93		40-3						175.0	00	9	765.0	39	5493	9
94		40-3						49.0	00	9	765.0		5493	
		80-3					3	584.0	00		599.0		7751	
96		80-3					3	665.0	00	18	599.0		7751	
		80-3					2	213.0	00		599.0		7751	
98	570	80-3	505				3	169.0	0		599.0		7751	
99	570	80-3	505				2	997.0	0		599.0		7751	
100	580	50-3	514					306.0			594.0		4427	
OBS	F3	F4	F5	F6	F7	F8	F9	F10	F11	F12	F13	В1	В2	ВЗ
OBS 81	F3	F4 0	F5 0	F6 0	F7 0	F8 0	F9 0	F10 0						
81 82	1	0							F11 0 0	F12 0 0	0	0	1	0
81 82 83	1 1 1	0	0	0	0	0	0	0	0	0		0	1	0
81 82 83 84	1	0	0	0	0	0	0	0	0	0	0	0	1 1 1	0 0 0
81 82 83	1 1 1	0	0 0	0 0 0	0 0	0	0 0	0 0 0	0 0 0	0 0	0 0 0	0 0 0	1 1 1 0	0 0 0
81 82 83 84 85 86	1 1 1 1	0 0 0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0	1 1 0 0	0 0 0 0
81 82 83 84 85 86 87	1 1 1 1 1	0 0 0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 1 1	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 1	0 0 0 0	0 0 0 1 1	1 1 0 0	0 0 0 0
81 82 83 84 85 86 87 88	1 1 1 1 1 1 1	0 0 0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0	0 0 0 1 1 1 1	0 0 0 0 0	0 0 0 0 0	0 0 0 0	0 0 0 1 1	0 0 0 0	0 0 0 1 1	1 1 0 0	0 0 0 0
81 82 83 84 85 86 87 88	1 1 1 1 1 1 1 1 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0	0 0 0 0 0 0	0 0 0 1 1 1	0 0 0 0 0	0 0 0 0 0	0 0 0 0	0 0 0 1 1 1	0 0 0 0 0	0 0 0 1 1 1 1	1 1 0 0 0 0	0 0 0 0 0 0 0
81 82 83 84 85 86 87 88 89	1 1 1 1 1 1 1 1 0	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 1 1 1 1	0 0 0 0 0 0 0	0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 1 1 1 1	0 0 0 0 0	0 0 0 1 1 1	1 1 0 0 0	0 0 0 0 0 0 0 0
81 82 83 84 85 86 87 88 89 90	1 1 1 1 1 1 1 0 1	0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0	0 0 0 1 1 1 1 1	0 0 0 0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0 0 0 0	0 0 0 1 1 1 1	0 0 0 0 0 0 0 0 0	0 0 0 1 1 1 1 1	1 1 0 0 0 0	0 0 0 0 0 0 0
81 82 83 84 85 86 87 88 89 90 91	1 1 1 1 1 1 1 1 1 1 1 1 1 1	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0	0 0 0 1 1 1 1 1	0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0	0 0 0 1 1 1 1 1 1 0	0 0 0 0 0 0 0 0	0 0 0 1 1 1 1 1 0 0	1 1 0 0 0 0 0 0	0 0 0 0 0 0 0 0
81 82 83 84 85 86 87 88 89 90 91 92 93	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0	0 0 0 1 1 1 1 1 1 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0	0 0 0 1 1 1 1 1	0 0 0 0 0 0 0 0 0	0 0 0 1 1 1 1 1 0 0	1 1 0 0 0 0 0 0	0 0 0 0 0 0 0 0
81 82 83 84 85 86 87 88 89 90 91 92 93	1 1 1 1 1 1 1 1 0 1 1 1 1	000000000000000000000000000000000000000	0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 1 1 1 1 1 1 0 0	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 1 1 1 1 1 1 0 0	0 0 0 0 0 0 0 0 0	0 0 0 1 1 1 1 1 0 0 0	1 1 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0
81 82 83 84 85 86 87 88 89 90 91 92 93 94	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 1 1 1 1 1 0 0	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 1 1 1 1 1 0 0	0 0 0 0 0 0 0 0 0 0	0 0 0 1 1 1 1 0 0 0	1 1 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0
81 82 83 84 85 86 87 88 99 91 92 93 94 95	1 1 1 1 1 1 1 0 1 1 1 1 1	0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 1 1 1 1 1 0 0	0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 1 1 1 1 1 0 0	0 0 0 0 0 0 0 0 0	0 0 0 1 1 1 1 0 0 0 0	1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0
81 82 83 84 85 86 87 88 89 90 91 92 93 94 95 96	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	000000000000000000000000000000000000000	0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 1 1 1 1 1 1 0 0 0	0 0 0 0 0 0 0 0 0 1 1 1	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 1 1 1 1 1 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 1 1 1 1	0 0 0 1 1 1 1 0 0 0	1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 1 1 1 1
81 82 83 84 85 86 87 88 89 90 91 92 93 94 95 97	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 1 1 1 1 1 1 0 0 0 0	0 0 0 0 0 0 0 0 0 0 1 1 1	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 1 1 1 1 1 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 1 1 1 1	0 0 0 1 1 1 1 0 0 0 0 0 0	1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 1 1 1 1
81 82 83 84 85 86 87 88 89 90 91 92 93 94 95 96	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 1 1 1 1 1 0 0 0 0 1 1 1 1	0 0 0 0 0 0 0 0 0 0 1 1 1 1	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		0 0 0 1 1 1 1 1 1 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 1 1 1 1	0 0 0 1 1 1 1 0 0 0 0	1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 1 1 1 1

OBS		JECT IBER	r				PRODI	JCTION	N RATE		F1		F2	
101	580	050-3	2514					2396.0		_				
		50-3					•	798.0			5594.0	_	1442	
		50-3									5594.0		1442	
		50-3						2665.0			5594.0	_	4427	
		20-3						1344.0		36	5594.0	24	4427	75
		20-3						900.0			•			•
		20-3					_	837.0						
108		20-3					-	426.0			•			
		86-3						455.0						
110		.00-3						76.4			79.0		3004	
								918.0			171.0	3	6402	27
111		.00-3						.317.0			171.0	3	6402	:7
112		.00-3						488.0			171.0		6402	
113		.00-3						420.0			171.0	3	6402	7
114		.60-3						000.0			000.0	40	1607	7
		60-3						011.0		113	000.0	40	1607	7
		60-3					1	331.0	0	113	000.0	40	1607	7
117		60-3					1	331.0	0	113	000.0	40	1607	7
118		60-3					1	331.0	0	113	000.0		1607	
		60-3					1	331.0	0	113	000.0		1607	
120	760	00-3	608					906.0	0		244.8		2367	
														_
OBS	F3	F4	F5	F6	F7	F8	F9	F10	F11	F12	F13	В1	В2	ВЗ
101	1	0	0	0	0	1	0	0	0	1	0	0	0	1
102	1	0	0	0	0	1	0	٠ ٥	ō	ī	ő	ő	ő	ī
103	1	0	0	0	0	1	0	0	0	ī	ō	ō	Ö	ī
104	1	0	0	0	0	1	Ō	0	ō	ī	Ö	õ	ő	î
105											Ô	ő	ő	ō
106										÷	Ö	ŏ	0	0
107										÷	Ö	o	Ö	ő
108								·		:	ō	Ö	0	o
109	1	0	0	0	0	Ó	i	Ö	ò	i	Ö	0	0	1
110	1	0	0	0	0	ō	ī	Ö	ő	ō	1	0	0	1
111	1	0	0	ō	ō	ō	ī	Ö	Ö	0	1	0	0	1
112	1	0	0	ō	ō	ŏ	ī	Ö	0	0	1	0	0	1
113	1	0	ō	ō	ō	ō	ī	ő	Ö	0	i	0		
114	1	0	ō	ō	ō	ő	ī	Ö	0	0	1	0	0	1
115	ī	ō	ŏ	ŏ	ő	ō	i	ő	0	0	1	0	1	0
116	ī	ō	ō	ő	Ö	o	ī	ő	0	0	1	0	1	0
117	ī	ő	ő	Ö	0	o	1	0	0	0			1	0
118	ī	ō	ő	ő	0	0	1	0	0	0	1	0	1	0
119	ī	o	ő	Ö	Ö	0	1	0	0	0	1 1	0	1	0
120	ī	Ö	ő	0	0	1	0	0	1	0	0	0	1	0
	-	-	-	-	-	_	0	0	_	U	U	U	1	0

OBS	PRO	JECT	r				PRO	OUCTIO		ΓE	F1			F2
								51/1	'AL		FI		1	: 4
121		00-3						1000.			4244.	. 8	523	3676
122		00-3						1000.			4244.	. 8	523	3676
123		20-3						14.	40		4189.	. 0	527	7986
124		10-3						177.					348	3638
125		10-3						135.					348	8638
126		10-3						97.		,			348	8638
127		10-3						49.					348	8638
128 129		40-3						30.			70448.		3558	
130		40-3						30.			70448.		3558	
131		40-3						30.			70448.		3558	
132		40-3						30.			70448.		3558	
133		70-3						30.			70448.		3558	
134		70-3						178.			10496.			401
135		70-3						734.			10496.			401
136		70-3						867.			10496.			401
137		90-3						219. 700.			10496.			401
138		90-3						1237.			8755.			699
139		90-3						444.			8755. 8755.			699
140		90-3						373.			8755.			699
			000					3/3.	45		8/55.	U	/96	699
OBS	F3	F4	F5	F6	F7	F8	F9	F10	F11	F12	F13	В1	B2	вз
														23
121	1	0	0	0	0	1	0	0	1	0	0	0	1	0
122	1	0	0	0	0	1	0	0	1	0	0	0	1	0
123	1	0	0	0	0	0	1	0	0	0	1	0	1	0
124 125	0	0	1	0	0	0	1	0	0	0	1	0	0	1
125	0	0	1	0	0	0	1	0	0	0	1	0	0	1
126	0	0		0	0	0	1	0	0	0	1	0	0	1
128	1	0	1	0	0	0	1	0	0	0	1	0	0	1
129	1	0	0	0	0	0	1	0 -	0	0	1	0	1	0
130	1	0	0	0	0	0	1	0	0	0	1	0	1	0
131	ī	0	0	0	0	0	1	0	0	0	1	0	1	0
132	i	Ö	0	0	0	0	1	0	0	0	1	0	1	0
133	ī	Ö	0	0	0	0	1	0	0	0	1	0	1	0
134	ī	Ö	0	0	0			0	0	0	1	0	1	0
		0	0			0	1	0	0	0	1	0	1	0
135		Ω	Ω	0	Λ.									
135 136	1	0	0	0	0	0	1	0	0	0	1	0	1	0
136		0	0	0	0	0	1	O	Ō	0	1	ō	1	0
136 137	1 1 1	0	0	0	0	0	1	0	0	0	1	0	1	0
136	1	0	0 0 0	0	0	0	1	0	0	0	1 1 1	0	1 1 1	0 0 0
136 137 138	1 1 1 1	0 0 0	0	0	0	0	1	0	0	0	1	0	1	0

OBS		JECT IBER	r				PROI	OUCTIO SY/I		Έ	F1		F	2
142 143 144 145 146 147 148 149	870 870 870 870 930 930 932 932	190-3 055-3 055-3 055-3 055-3 060-3 060-3 130-3	3601 3601 3601 3601 3542 3542 3542					1581. 920. 2200. 1200. 1300. 1760. 3533. 1062. 3768. 802.	00 00 00 00 00 00 00 00 50	4	8755. 17650. 17650. 17650. 17650. 5293. 5293. 5973. 5973.	0 0 0 0 0 0 0 0 0	796 1807 1807 1807 1807 1807 4039 4039 413 413	699 970 970 970 970 970
OBS	F3	F4	F5	F6	F7	F8	F9	F10	F11	F12	F13	В1	B2	вз
141 142 143 144 145 146 147 148 149 150	1 1 1 1 1 1 1 1	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	1 1 1 1 1 1 0 0	0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 1 1 1	1 1 1 1 1 0 0 0	0 0 0 0 0 0 0 0 0	1 1 1 1 1 0 0 0 0	0 0 0 0 0 0 1 1 1 1

OBS		OJE MBE						PR	ODUC			Έ	E1		E2
1 2 3 4 5 6 7 8 9 10 11 12 13 14	NU. 022 022 022 029 099 099 099 099 099 099		-35 -35 -35 -35 -35 -35 -35 -35 -35 -35	32 32 32 20 20 20 20 12 12 12 12				PK	11 13 6 9 9 6 10 9 8 11 12	33.3 17.6 43.5 90.6 65.8 10.2 97.7 51.8 29.9 06.2 76.3 31.5 09.1	Y 0 0 1 2 2 9 5 3 6 4 8 5 5 8 8 9		F1 400.0 400.0 400.0 22775.5 22775.5 22775.5 227775.5 46595.0 46595.0 46595.0 99793.0		F2 177625.00 177625.00 177625.00 177625.00 1498587.00 1498587.00 1498587.00 1498587.00 2853579.00 2853579.00 2853579.00 2853579.00 3185151.00
17 18 19	100 100	020- 020- 160- 160-	-35: -35: -35:	13 13 25					29 70 20	91.2 90.0 90.5 37.0	0 0 4		99793.0 99793.0 99793.0 4109.4 4109.4	0	3185151.00 3185151.00 3185151.00 4319100.35 4319100.35
OBS	F3	F4	F5	F6	F7	F8	F9	F10	F11	F12	F13	Al			
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	1 1 1 1 1 1 1 1 1 1 1 1 0 0 0 0			0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	000000000000000000000000000000000000000	0 0 0 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 0 0	1 1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 1 1 1 1 1 1	1 1 1 1 1 1 1 0 0 0 0 0 0 0				0 0 0 0 0 0 0 0 0 0 1 1 1 1 1 0 0 0 0 0

		OJE						PR	ODUC	TION	RAT	E		
obs	NU.	MBE	R						Т	N/DA	Y		F1	F2
21			-35							17.0			4109.40	4319100.35
22			-35						2	47.2	0		4109.40	4319100.35
23			-35						1	71.8	2		4109.40	4319100.35
			-35							70.5			3513.30	345775.00
			-35						2	31.7	5		3513.30	345775.00
			-35						5	53.7	4		3513.30	345775.00
			-35						4	97.0	6		3513.30	345775.00
			-35						7	32.4	4		3513.30	345775.00
			-34						5	81.6	3		38651.00	1570359.00
			-34					•	10	72.5	7		38651.00	1570359.00
			-34						12	01.1	3		38651.00	1570359.00
			-34						10	68.9	2		38651.00	1570359.00
			-34						12	46.9	1		38651.00	1570359.00
34			-35						20	45.9	0		20022.00	1465504.00
35			-35						11:	36.3	0		20022.00	1465504.00
36			-35						14	02.4	0		20022.00	1465504.00
			-350						12	95.1	0		20022.00	1465504.00
			-350						15	35.9	0		20022.00	1465504.00
			-352						13	45.0	0		35734.00	1539380.00
40	340	010	-352	26					16	02.00	0		35734.00	1539380.00
000	п.													
OBS	F 3	F4	F'5	1.6	F 7	F8	F9	F10	F11	F12	F13	A1		
21	0	0	0	1	0	0	1	0	0	0	1			1
22	0	0	0	1	0	0	1	0	ō	ō	ī			1
23	0	0	0	1	0	0	1	0	Ō	ō	ī			î
24	1	0	0	0	0	0	0	0	ō	i	ō			î
25	1	0	0	0	0	0	0	0	0	1	ō			ī
26	1	0	0	0	0	0	0	0	0	1	ō			i
27	1	0	0	0	0	0	0	0	0	1	0			î
28	1	0	0	0	0	0	0	0	0	1	o			ī
29	1	0	0	0	0	0	0	1	0	0	1			ō
30	1	0	0	0	0	0	0	1	0	0	1			Ö
31	1	0	0	0	0	0	0	1	0	0	1			Ö
32	1	0	0	0	0	0	0	1	0	0	1			ō
33	1	0	0	0	0	0	0	1	0	0	1			ŏ
34	1	0	0	0	0	1	0	0	1	ō	ō			ő
35	1	0	0	0	0	1	0	0	1	0	0			ŏ
36	1	0	0	0	0	1	0	0	1	0	0			Ö
37	1	0	0	0	0	1	0	0	1	0	0			Ô
38	1	0	0	0	0	1	0	0	1	0	ō			0
39	1	0	0	0	0	1	0	0	0	1	0			ő
40	1	0	0	0	0	1	0	0	0	1	0			Ö

OBS		OJE MBE						PROD		ON R	ATE	F	'1 F2	F3
41	24	010	- 2 -	2.0					•			_		
42			-35 -35							3.00			0 1539380	1
43			-35 -35							7.00			0 1539380	
44										2.00		35734.0		1
	35		-35							0.45		1705.2		0
										3.40		•	2322152	0
	35									9.00			2322152	0
47			-35							8.62			0 1646955	1
48			-35							5.04		40003.0		1
49			-35							0.30		40003.0	0 1646955	1
	35									4.63		40003.0		1
	35									3.89		40003.0	0 1646955	1
	35									6.00			2997476	0
	353								62	0.00			2997476	0
54			-35						29	0.00			2997476	0
	353								20	9.00			2997476	0
	353								11	4.00			2997476	ō
	365								29	2.25		1095.5	1 143684	ō
	365								35	5.63		1095.5		ō
59	365	570-	-36	05					15	5.07		1095.5		ō
60	365	70-	-36)5						2.56		1095.5		ō
														٠
OBS	F4	DE.	D.C											
		ro	10	F /	F8	F9	F10	F11	F12	F13	A1			
				F/	F8	F9	F10	F11	F12	F13	A1			
41	0	0	0	0	1	F9 0	F10 0	F11	F12	F13 0	Al		0	
42	0	0	0	0	1	0			1		Al		0	
42 43	0	0	0	0	1 1 1	0	0 0 0	0	1 1 1	0	Al			
42 43 44	0 0 0 1	0 0 0	0	0	1	0	0	0	1	0	Al		0	
42 43 44 45	0 0 0 1 1	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0	0 0 0	1 1 1	0 0 0	Al		0 0 0	
42 43 44 45 46	0 0 0 1 1	0 0 0 0	0 0 0 0 0	0 0 0 0 0	1 1 1 1	0 0 0	0 0 0	0 0 0	1 1 1	0 0 0	Al		0 0 0	
42 43 44 45 46 47	0 0 0 1 1	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	Al		0 0 0 0	
42 43 44 45 46 47 48	0 0 0 1 1	0 0 0 0	0 0 0 0 0	0 0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0 0	0 0 0 0	1 1 1 1 1	0 0 0 0	Al		0 0 0 0	
42 43 44 45 46 47	0 0 0 1 1 1	0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0	1 1 1 1 1	0 0 0 0 0 0	0 0 0 0 0	0 0 0 0 0	1 1 1 1 1	0 0 0 0 0	Al		0 0 0 0 0	
42 43 44 45 46 47 48	0 0 0 1 1 1 0	0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0 0	1 1 1 1 1 1	0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0	1 1 1 1 1 1 1	0 0 0 0 0 0	Al		0 0 0 0 0 0	
42 43 44 45 46 47 48 49	0 0 0 1 1 1 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	1 1 1 1 1 1 1	0 0 0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0	1 1 1 1 1 1 1 1	0 0 0 0 0 0	Al		0 0 0 0 0 0	
42 43 44 45 46 47 48 49 50	0 0 0 1 1 1 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	1 1 1 1 1 1 1 1	0 0 0 0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0	1 1 1 1 1 1 1 1 1	0 0 0 0 0 0	Al		0 0 0 0 0 0 0	
42 43 44 45 46 47 48 49 50	0 0 0 1 1 0 0 0	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0	1 1 1 1 1 1 1 1	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0 0	1 1 1 1 1 1 1 1 1 1	0 0 0 0 0 0 0 0	Al		0 0 0 0 0 0 0	
42 43 44 45 46 47 48 49 50 51	0 0 0 1 1 0 0 0 0	0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 1	0 0 0 0 0 0 0 0 0 0	1 1 1 1 1 1 1 1 1	0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	1 1 1 1 1 1 1 1 1 1 0	0 0 0 0 0 0 0 0 0	Al		0 0 0 0 0 0 0	
42 43 44 45 46 47 48 49 50 51 52 53	0 0 0 1 1 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 1 1	0 0 0 0 0 0 0 0 0 0	1 1 1 1 1 1 1 1 1 1 1 1	000000000000000000000000000000000000000	0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0	1 1 1 1 1 1 1 1 1 0 0	0 0 0 0 0 0 0 0 0 0	Al		0 0 0 0 0 0 0 0 0	
42 43 44 45 46 47 48 49 50 51 52 53	0 0 0 1 1 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 1 1 1	0000000000000	1 1 1 1 1 1 1 1 1 1 1 1	0000000000000	0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	1 1 1 1 1 1 1 1 1 0 0	0 0 0 0 0 0 0 0 0 0	Al		0 0 0 0 0 0 0 0 0	
42 43 44 45 46 47 48 49 50 51 52 53 54 55	0 0 0 1 1 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 1 1 1	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	00000000000000	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 1 1 1 1 1 1 1 1 0 0	0 0 0 0 0 0 0 0 0 0 0	Al		0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
42 43 44 45 46 47 48 49 50 51 52 53 54 55 56	0 0 0 1 1 1 0 0 0 0 0 0 0 0	000000000000000000000000000000000000000	0 0 0 0 0 0 0 0 0 0 0 0 1 1 1 1	000000000000000000000000000000000000000	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	000000000000000000000000000000000000000	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0	1 1 1 1 1 1 1 1 1 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0	Al		0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
42 43 44 45 46 47 48 49 50 51 52 53 55 57 58	0 0 0 1 1 1 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 1 1 1 1 1 0 0 0	000000000000000000000000000000000000000	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0	1 1 1 1 1 1 1 1 1 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0	Al		0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57	0 0 0 1 1 1 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 1 1 1 1	000000000000000000000000000000000000000	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	000000000000000000000000000000000000000	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0	1 1 1 1 1 1 1 1 1 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0	Al		0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	

OBS		OJE MBE						PROD	UCTI TN/	ON R	ATE	F1	F2	F3
61	46	040	-35	45					1	0.08		133.50		
62			-35							0.51		133.50		0
63	46	040	-35	45						0.33		133.50		0
64			-35							6.12		284.93	182576	0
	48									4.30				1
	48											284.93		1
67			-35							8.65		284.93		1
	48									5.85			4026596	1
	48									2.00		290.88	209372	0
	48									5.00		290.88	209372	0
										7.00		290.88	209372	0
	48									7.00		290.88	209372	0
	50									0.45		13927.00	1713257	1
	50								45	1.10			1713257	1
74			351						184	0.78			1713257	1
	50								160	4.19			1713257	1
	50								72	5.24			1713257	1
77	53	030	-35	10					455	5.00		281653.00	7205002	ō
	53									1.00		281653.00		ő
79	530	030	-35	10					1144			281653.00		ő
80	530	030-	-35	10						0.00		281653.00		0
													, 203002	
OBS	F4	F5	F6	F7	F8	F9	F10	F11	F12	F13	A1			
61	0	0	0	0	0	0	0	0	0	1			0	
62	0	0	0	0	0	0	0	0	0	1			ō	
63	0	0	0	0	0	0	0	0	0	1			ő	
64	0	0	0	0	1	0	0	0	0	1			ő	
65	0	0	0	0	1	0	0	0	0	1			0	
66	0	0	0	0	1	0	0	0	0	ī			0	
67	0	0	0	0	1	0	0	0	ō	ī			Ö	
68	0	1	0	0	0	1	0	ō	ī	ō			0	
69	0	1	0	0	ō	ī	ō	ŏ	î	ŏ			0	
70	0	1	Ó	ō	ō	ī	ō	ŏ	ī	ŏ			0	
71	ō	ī	ō	ō	ō	ī	ŏ	ō	i	Ö				
72	ō	ō	ō	ō	ĭ	ō	Ö	1	ō	Ö			0	
73	ō	ő	ŏ	ő	ī	ő	Ö	1	0				0	
74	ő	ő	ő	ő	1	0	0	1	-	0			0	
75	ő	. 0	ő	ő	1	0			0	0			0	
76	0	0	0	0	1		0	1	0	0			0	
77	0	0	1	0	1	0	0	1	0	0			0	
78	0	0	1			0	0	0	1	0			0	
				0	1	0	0	0	1	0			0	
79	0	0	1	0	1	0	0	0	1	0			0	
80	0	0	1	0	1	0	0	0	1	0			0	

OBS		OJE MBE						PROD		ON R DAY	ATE		F1	F2	F3
		030							3229					7205002	0
82		020								.58		937.		235512	1
		020							462			937.	44	235512	1
		020							133			937.		235512	1
		040							996					1194647	1
		080							700			14906.			1
		080							1060					2163817	1
		080 080							1080					2163817	1
		080.							1162					2163817	1
		030.							1183					2163817	1
		030.							812			46546.	00		0
		030.							200					7678699	0
		030.							2863					7678699	0
		030.							2038					7678699	0
)40-							1639					7678699	0
)40.)40.							430					3954939	1
		040-							806					3954939	1
		040-							955					3954939	1
100									943					3954939	1
100	570	740	-33	00					610	.00		25379.	00	3954939	1
OBS	F4	F5	F6	F7	FR	F9	FIO	Fll	F12	E12	2.1				
OBS	F4	F5	F6	F7	F8	F9	F10	F11	F12	F13	A1				
OBS 81	F4 0	F5 0	F6 1	F7 0	F8 1						A1			0	
						F9 0 1	F10 0 0	F11 0 0	1	0	A1			0	
81	0	0	1	0	1	0	0	0	1	0	A1			0	
81 82	0	0	1	0	1	0	0	0	1 0 0	0 1 1	A1			0	
81 82 83	0	0	1 0 0	0	1 0 0	0 1 1	0 0 0	0 0 0	1	0 1 1	A1			0 0 0	
81 82 83 84	0 0 0	0 0 0	1 0 0	0 0 0	1 0 0	0 1 1	0 0 0	0 0 0	1 0 0 0	0 1 1 1 0	Al			0 0 0	
81 82 83 84 85	0 0 0 0	0 0 0	1 0 0 0	0 0 0	1 0 0 0	0 1 1 1 0	0 0 0 0	0 0 0 0	1 0 0 0 0	0 1 1 1 0 0	Al			0 0 0 0	
81 82 83 84 85 86	0 0 0 0	0 0 0 0 0	1 0 0 0 0	0 0 0 0 0	1 0 0 0 0	0 1 1 0 0	0 0 0 0	0 0 0 0	1 0 0 0	0 1 1 1 0	Al			0 0 0 0 0	
81 82 83 84 85 86	0 0 0 0 0	0 0 0 0 0	1 0 0 0 0 0	0 0 0 0 0	1 0 0 0 0 1 1	0 1 1 0 0	0 0 0 0 0	0 0 0 0	1 0 0 0 0 1	0 1 1 1 0 0	Al			0 0 0 0 0	
81 82 83 84 85 86 87 88	0 0 0 0 0 0	0 0 0 0 0	1 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0	1 0 0 0 0 1 1	0 1 1 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	1 0 0 0 0 1 1	0 1 1 0 0 0	Al			0 0 0 0 0 0	
81 82 83 84 85 86 87 88 89	0 0 0 0 0 0 0	0 0 0 0 0 0 0	1 0 0 0 0 0 0	0 0 0 0 0 0 0	1 0 0 0 0 1 1 1	0 1 1 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0	1 0 0 0 0 1 1 1	0 1 1 1 0 0 0 0	Al			0 0 0 0 0 0 0	
81 82 83 84 85 86 87 88 89 90 91	0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0	1 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	1 0 0 0 0 1 1 1 1 1	0 1 1 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0	1 0 0 0 0 1 1 1 1	0 1 1 1 0 0 0	Al			0 0 0 0 0 0 0	
81 82 83 84 85 86 87 88 90 91 92 93	0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0	1 0 0 0 0 0 0 0 0 1 1 1	0 0 0 0 0 0 0 0 0	1 0 0 0 0 1 1 1 1	0 1 1 0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0	1 0 0 0 0 1 1 1 1	0 1 1 1 0 0 0 0 0	Al			0 0 0 0 0 0 0 0	
81 82 83 84 85 86 87 88 89 90 91 92 93	0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0	1 0 0 0 0 0 0 0 0 1 1 1 1	0 0 0 0 0 0 0 0 0 0	1 0 0 0 0 1 1 1 1 1 1 1 1 1 1 1	0 1 1 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0	1 0 0 0 0 1 1 1 1 1	0 1 1 0 0 0 0 0	Al			0 0 0 0 0 0 0 0 0	
81 82 83 84 85 86 87 88 89 90 91 92 93 94 95	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	00000000000000	1 0 0 0 0 0 0 0 0 0 0 1 1 1 1	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 0 0 0 0 1 1 1 1 1 1 1 1 1 1 1 1 1	011100000000000000000000000000000000000	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0	1 0 0 0 0 1 1 1 1 1	0 1 1 0 0 0 0 0 0	Al			0 0 0 0 0 0 0 0	
81 82 83 84 85 86 87 88 99 91 92 93 94 95 96	000000000000000000000000000000000000000	000000000000000000000000000000000000000	1 0 0 0 0 0 0 0 0 0 0 0 1 1 1 1	000000000000000000000000000000000000000	1 0 0 0 0 0 1 1 1 1 1 1 1 1	0 1 1 1 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0	1 0 0 0 0 1 1 1 1 1 1	0 1 1 0 0 0 0 0 0 0	Al			0 0 0 0 0 0 0 0 0	
81 82 83 84 85 86 87 88 99 91 92 93 94 95 96	000000000000000000000000000000000000000	000000000000000000000000000000000000000	1 0 0 0 0 0 0 0 0 0 0 0 1 1 1 1 0 0	000000000000000000000000000000000000000	1 0 0 0 0 0 1 1 1 1 1 1 1 1 1 0 0	0 1 1 1 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 0 0 0 0 1 1 1 1 1 1 1	0 1 1 0 0 0 0 0 0 0	Al			0 0 0 0 0 0 0 0 0 1 1 1	
81 82 83 84 85 86 87 88 90 91 92 93 94 95 97 98			1 0 0 0 0 0 0 0 0 0 0 0 0 1 1 1 1 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 0 0 0 0 0 1 1 1 1 1 1 1 1 1 0 0 0	0 1 1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 1 1 1 1 1 1 1	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 0 0 0 0 1 1 1 1 1 1 1 1 0 0	0 1 1 0 0 0 0 0 0 0 0 0	Al			0 0 0 0 0 0 0 0 0 0 1 1 1	
81 82 83 84 85 86 87 88 99 91 92 93 94 95 96	000000000000000000000000000000000000000	000000000000000000000000000000000000000	1 0 0 0 0 0 0 0 0 0 0 0 1 1 1 1 0 0	000000000000000000000000000000000000000	1 0 0 0 0 0 1 1 1 1 1 1 1 1 1 0 0	0 1 1 1 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 0 0 0 0 1 1 1 1 1 1 1 1	0 1 1 0 0 0 0 0 0 0 0 0	Al			0 0 0 0 0 0 0 0 1 1 1	

OBS		OJE MBE						PROD		ON R	ATE	F1	F2	F3 .
101 102 103 104 105 106 107 110 111 112 113 114 115 116 117 118 119 120	57 57 57 58 58 58 58 58 60 60 60 60 60 60 60 60	080 080 080 050 050 050 050 050 050 060 060 060	-35 -35 -35 -35 -35 -35 -35 -35 -35 -35	05 005 005 005 005 14 114 114 114 114 114 114 114 114 114					463 493 839 881 181 1217 1447 1026 935 1002 1521 1127 1019	.25 .00 .05 .03 .43 .98 .32 .55 .08 .51 .00 .15 .95 .70		6979.10 6979.10 6979.10 6979.10 9304.80 9304.80 9304.80 9304.80 9304.80	1277510 1277510 2444275 2444275 2444275 2444275 2444275 2444275 2444275 2444275	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
OBS	F4	F5	F6	F7	F8	F9	F10	F11	F12	F13	A1			-
101 102 103 104 105 107 108 109 110 111 112 113 114 115 116 117 118	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0				1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	000000000000000000000000000000000000000	000000000000000000000000000000000000000	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 1 1 1 1 1 1 1 1 1 1 1 1 1 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0				

OBS		OJE MBE						PROD	UCTI TN/		ATE	F1	F2	F3
121	61	086	-35	22					354	. 55			330043	1
122	61	086	-35	22					432			787.15	330043	1
123	70	100	-35	47					278			4929.10	364027	1
124	70	100	-35	47					346			4929.10	364027	i
125	70	100	-35	47					359			4929.10	364027	1
126									306			4929.10		
127									359					1
128		001							1177			4929.10		1
129												39846.40		1
130									1132			39846.40		1
131									1026			39846.40		1
132									1026			39846.40		1
									1228			39846.40		1
133									1177			39864.40		1
		001-							1132			39864.40	1889673	1
135									1026	. 66		39864.40	1889673	1
136									1026	.18		39864.40	1889673	1
137									1228	.39		39864.40	1889673	1
138									689	. 37		5208.00	485923	1
139									423	. 44		5208.00	485923	ī
140	720	050-	-354	12					568			5208.00	485923	ī
													.00320	-
OBS	F4	F5	F6	F7	F8	F9	F10	F11	F12	F13	A1			
121	0	0	0	0	0	1	0	0	1	0			0	
122	0	0	0	0	0	1	0	0	1	0			0	
123	0	0	0	0	0	1	0	0	0	1			0	
124	0	0	0	0	0	1	0	0	0	1			ō	
125	0	0	0	0	0	1	0	0	0	1			ō	
126	0	0	0	0	0	1	0	0	0	1			ő	
127	0	0	0	0	0	1	0	0	0	1			ő	
128	0	0	0	0	0	0	1	ō	ō	ī			0	
129	0	0	0	0	0	0	1	ō	ō	ī			0	
130	0	0	0	0	ō	ō	ī	ō	Ö	ī			0	
131	0	0	0	0	ō	ō	ī	ő	Ö	ī			0	
132	0	0	0	ō	ō	ō	ī	ŏ	ő	ī			0	
133	ō	ō	ō	ō	ō	ō	ī	ő	Ö	1				
134	ō	ő	ō	Ö	ő	0	1	Ö	0	1			0	
135	ő	ő	ő	0	ő	Ö	1	0	0				. 0	
136	o	0	Ö	0	0	0	1	0		1			0	
137	0	ő	0	0	0	0	1		0	1			0	
138	0	ő	0	0	0	1		0	0	1			0	
139	0	0	0	0			0	0	0	1			0	
140	0	0	0	0	0	1	0	0	0	1			0	
140	U	U	U	U	0	1	0	0	0	1			0	

OBS		OJE MBE						PROD	UCTI TN/		ATE	F1	F.2	77.
			-						1117	DAI		rı	F2	F3
141	72	050	-35	42					736	.88		5208.00	485923	1
142		050							478	.12		5208.00	485923	ī
143	72	050	-35	42					689			5208.00	485923	ī
144	72	050	-35	42					423	. 44		5208.00	485923	ī
145	72	050	-35	42					586	.20		5208.00	485923	ī
146									736	.88		5208.00	485923	ī
147	72	050	- 35	42					478	.12		5208.00	485923	ī
148	72	160	-35	51					1594	.00		16652.00		ī
149									535	.00		16652.00		ī
150									1275	.00		16652.00		ī
151									968	.00		16652.00		ī
152	72	160	-35	51					811	.00		16652.00		ī
153	76	000	-360	80					1053	. 04		11775.30	523676	ī
		000							1461	.72		11775.30	523676	ī
155									1118	. 19		11775.30	523676	ī
156									1171	.80		11775.30	523676	ī
157	78	010	-352	27					201			367.00	348638	ō
158	78	010-	-352	27					20	. 82		367.00	348638	ō
159	78	010-	-352	27						.61		367.00	348638	ō
160	78	010-	-352	27						.17		367.00	348638	ō
												00,.00	340030	•
OBS	F4	F5	F6	F7	F8	F9	F10	F11	F12	F13	A1			
141	^						_	_						
141	0	0	0	0	0	1	0	0	0	1			0	
143	0	0	0	0	0	1	0	0	0	1			0	
144	0	0	0	0	0	1	0	0	0	1			0	
145	0	0	0	0	0	1	0	0	0	1			0	
146	0	0	0	0	0	1	0	0	0	1			0	
147	0	0	0	0	0	1	0	0	0	1			0	
148	0	ŏ	ō	0	0	1	0		0	1			0	
149	0	0	Ö	0	0	1	0	0	0	1			0	
150	0	0	0	0	0			0	0	1			0	
151	0	0	0	0	0	1	0	0	0	1			0	
152	0	0	0	0		1	0	0	0	1			0	
153	0	0	0	0	0	0	0	0	0	1			0	
154	0	0	0	0	1	0		1	0	0			0	
155	0	0	0	0	1	0	0	1	0	0			0	
156	0	0	0	0	1	0	0	1	0	0			0	
157	0	1	0	0	0	1		1	0	0			0	
158	0	i	0	0	0	1	0	0	0	1			0	
159	0	1	0	0		1	0	0	0	1			0	
160	0	1	0	0	0	1	0	0	0	1			0	
									0	1			0	

		OJE						PROD	UCTI	ON F	ATE			
OBS	NU	MBE	R						TN/	DAY		F1	F2	F3
161		170							209	.94		4912.10	563401	1
162		170							215	.89		4912.10		ī
163	79	170	-35	10					115	.80		4912.10		ī
164		170							37	.46		4912.10		ī
165	79	170	-35	10						.84		4912.10		ī
166	79	190	-35	05					341			3106.80		ī
167	79	190	-35	05					221			3106.80		ī
168	79	190	-35	05					437			3106.80		1
169	79	190	-35	05					134			3106.80		1
170										.06		3106.80		1
171	79	210	-35	01					333			6424.00		1
172		210							332			6424.00		1
173	79	210	-350	01					709			6424.00		1
174	79	210	-350	01					393			6424.00		
175										.95		6424.00		1
176									225				392641	1
177									247				1807970	1
178									375				1807970	1
179													1807970	1
180									232				1807970	1
100	071	055	-360	<i>J</i> 1					352	.50		3600.98	1807970	1
OBS	F4	F5	F6	F7	F8	F9	F10	F11	F12	F13	A1			
161	0	0	0	0	0	1	0	0	0	1			0	,
162	0	0	0	0	0	1	ō	ō	ō	ī			0	
163	0	0	0	0	0	1	ō	ō	ō	ī			0	
164	0	0	0	0	0	1	ō	ō	ō	ī			0	
165	0	0	0	0	0	1	ō	ō	ō	ī			0	
166	0	0	o	ō	ō	ī	ō	ŏ	ő	ī			0	
167	0	o	ō	ō	ō	ī	ŏ	ő	ŏ	î			0	
168	ō	ō	ō	ō	ō	ī	ŏ	ő	ő	1			0	
169	ō	ō	ō	ō	ō	ī	ŏ	ő	ő	ī			0	
170	ō	ō	ō	ō	ő	ī	ō	ŏ	ő	1				
171	ō	ō	ō	ō	ĭ	ō	Ö	ŏ	1	ō			0	
172	ō	ō	ō	ő	ĩ	ő	ŏ	ŏ	1	0			1	
173	ő	ő	ő	ő	ī	ō	Ö	0					1	
174	ő	ő	ő	o	1	0	0		1	0			1	
175	ő	ő	ő	Ö	i	0	0	0	1	0			1	
176	0	0	0	0	0	1	0			0			1	
177	ő	o	0	0	0	1		0	0	1			0	
178	0	0	0	0	0		0	0	0	1			9	
179	0	0	0	0		1	0	0	0	1			1	
	0	0	0	0	0	1	0	0	0	1			0	
180	U	0	0	0	0	1	0	0	0	1			0	

								PROD	UCTI	ON R	ATE			
OBS	NU	MBE	R						TN/	DAY		F1	F2	F3
									1123	.00	٠	24385.00	4039137	1
182	93	060	-35	42					1431	.00		24385.00	4039137	1
183	93	060	-35	42					1325	.00				ī
L84	93	060	-35	42					1638	.00				ī
185	93	060	-35	42					1163	.00				ī
186	93	230-	-35	04										ī
L87	93	230	-350	04										ī
188	93:	230-	-35	04										ī
												5500.00	413413	_
BS	F4	F5	F6	F7	F8	F9	F10	F11	F12	F13	A 1			
81	0	0	0	0	0	1	0	0	1	0				,
182	0	0	0	0	0	1	0	o	1					
83	0	0	0	0	0	1	ō		î					
84	0	0	0	0	0	1	ō		1					
.85	0	0	0	0	0	1	ō		î					
.86	0	0	0	0	1	0	ō	_					-	
.87	0	0	0	0	1	ō	ō	-						
.88	0	0	0	0	1	ō	ō	ŏ	î	Ö			0	
	182 183 184 185 186 187	OBS NU 181 93 182 93 183 93 184 93 185 93 186 93 187 93 188 93 OBS F4 L81 0 182 0 184 0 185 0 184 0 185 0 186 0	DBS NUMBE: 181 93060 182 93060 183 93060 184 93060 185 93060 187 93230 187 93230 188 93230 188 93230 188 93230 188 93230 188 93230 188 93230 188 93230 188 93230	181 93060-35 182 93060-35 183 93060-35 184 93060-35 185 93060-35 186 93230-35 187 93230-35 188 93230-35 188 93230-35 188 93230-35 188 0 0 0 182 0 0 0 183 0 0 0 184 0 0 0 185 0 0 0 186 0 0 0 187 0 0 0	DBS NUMBER 181 93060-3542 182 93060-3542 184 93060-3542 185 93060-3542 186 93230-3504 187 93230-3504 188 93230-3504 DBS F4 F5 F6 F7 181 0 0 0 0 0 182 0 0 0 0 183 0 0 0 0 185 0 0 0 0 186 0 0 0 0 186 0 0 0 0 186 0 0 0 0	DBS NUMBER 181 93060-3542 182 93060-3542 184 93060-3542 185 93060-3542 185 93060-3542 186 93230-3504 187 93230-3504 188 93230-3504 188 93230-3504 188 93230-3504 188 93230-3504 188 90 0 0 0 0 0 189 0 0 0 0 0 0 180 0 0 0 0 0 180 0 0 0 0 0 181 0 0 0 0 0 0 181 0 0 0 0 0 0 182 0 0 0 0 0 0 183 0 0 0 0 0 0 184 0 0 0 0 0 0 185 0 0 0 0 0 0 186 0 0 0 0 0 1	DBS NUMBER 181 93060-3542 182 93060-3542 184 93060-3542 185 93060-3542 185 93060-3542 186 93230-3504 187 93230-3504 188 93230-3504 188 93230-3504 188 93230-3504 188 93230-3504 188 93230-3504 188 93230-3504 188 93230-3504	DBS NUMBER 181 93060-3542 182 93060-3542 184 93060-3542 185 93060-3542 185 93060-3542 186 93230-3504 187 93230-3504 188 93230-3504 188 93230-3504 188 0 0 0 0 0 1 0 181 0 0 0 0 0 1 0 182 0 0 0 0 0 1 0 183 0 0 0 0 0 1 0 184 0 0 0 0 0 1 0 185 0 0 0 0 0 1 0 185 0 0 0 0 0 1 0 186 0 0 0 0 0 1 0 187 0 0 0 0 1 0 188 0 0 0 0 0 1 0 188 0 0 0 0 0 1 0 188 0 0 0 0 0 1 0 188 0 0 0 0 0 1 0 188 0 0 0 0 0 1 0 188 0 0 0 0 0 1 0 188 0 0 0 0 0 1 0 188 0 0 0 0 0 1 0 188 0 0 0 0 0 1 0 188 0 0 0 0 0 1 0 188 0 0 0 0 0 1 0 188 0 0 0 0 0 1 0 188 0 0 0 0 0 1 0 188 0 0 0 0 0 1 0 188 0 0 0 0 0 0 1 0 188 0 0 0 0 0 0 1 0 188 0 0 0 0 0 0 1 0 188 0 0 0 0 0 0 1 0 188 0 0 0 0 0 0 1 0 188 0 0 0 0 0 0 1 0 188 0 0 0 0 0 0 0 1 0 188 0 0 0 0 0 0 1 0 188 0 0 0 0 0 0 1 0 188 0 0 0 0 0 0 0 1 0 188 0 0 0 0 0 0 1 0 188 0 0 0 0 0 0 0 0 0 188 0 0 0 0 0 0 0 0 0 188 0 0 0 0 0 0 0 0 0 0 188 0 0 0 0 0 0 0 0 0 188 0 0 0 0 0 0 0 0 0 188 0 0 0 0 0 0 0 0 0 188 0 0 0 0 0 0 0 0 0 188 0 0 0 0 0 0 0 0 0 188 0 0 0 0 0 0 0 0 0 188 0 0 0 0 0 0 0 0 0 188 0 0 0 0 0 0 0 0 0 188 0 0 0 0 0 0 0 0 0 188 0 0 0 0 0 0 0 0 0 188 0 0 0 0 0 0 0 0 0 188 0 0 0 0 0 0 0 0 0 188 0 0 0 0 0 0 0 0 0 188 0 0 0 0 0 0 0 0 0 188 0 0 0 0 0 0 0 0 0 188 0 0 0 0 0 0 0 0 0 188 0 0 0 0 0 0 0 0 188 0 0 0 0 0 0 0 0 0 188 0 0 0 0 0 0 0 0 0 188 0 0 0 0 0 0 0 0 188 0 0 0 0 0 0 0 0 0 188 0 0 0 0 0 0 0 0 188 0 0 0 0 0 0 0 0 188 0 0 0 0 0 0 0 0 188 0 0 0 0 0 0 0 0 188 0 0 0 0 0 0 0 0 188 0 0 0 0 0 0 0 0 188 0 0 0 0 0 0 0 0 188 0 0 0 0 0 0 0 0 188 0 0 0 0 0 0 0 0 0 188 0 0 0 0 0 0 0 0 0 188 0 0 0 0 0 0 0 0 0 188 0 0 0 0 0 0 0 0 0 188 0 0 0 0 0 0 0 0 0 188 0 0 0 0 0 0 0 0 0 0 188 0 0 0 0 0 0 0 0 0 0 188 0 0 0 0 0 0 0 0 0 0 0 188 0 0 0 0 0 0 0 0 0 0 0 0 188 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	DBS NUMBER 181 93060-3542 182 93060-3542 184 93060-3542 185 93060-3542 185 93060-3542 186 93230-3504 187 93230-3504 188 93230-3504	DBS NUMBER TN/ 181 93060-3542 1123 182 93060-3542 1431 183 93060-3542 1325 184 93060-3542 1638 185 93060-3542 1638 186 93230-3504 229 187 93230-3504 393 188 93230-3504 605 DBS F4 F5 F6 F7 F8 F9 F10 F11 F12 181 0 0 0 0 0 0 1 0 0 1 182 0 0 0 0 0 1 0 0 1 183 0 0 0 0 0 1 0 0 1 184 0 0 0 0 0 0 1 0 0 1 185 0 0 0 0 0 0 1 0 0 1 185 0 0 0 0 0 0 1 0 0 1 186 0 0 0 0 0 1 0 0 1 187 0 0 0 0 1 0 0 1 188 0 0 0 0 0 1 0 0 1 188 0 0 0 0 0 1 0 0 1 188 0 0 0 0 0 1 0 0 1 188 0 0 0 0 0 1 0 0 1 188 0 0 0 0 0 1 0 0 1 188 0 0 0 0 0 1 0 0 1 188 0 0 0 0 0 1 0 0 1 188 0 0 0 0 0 1 0 0 1 188 0 0 0 0 0 1 0 0 1 188 0 0 0 0 0 1 0 0 1 188 0 0 0 0 0 1 0 0 1 188 0 0 0 0 0 1 0 0 1 188 0 0 0 0 0 1 0 0 1 188 0 0 0 0 0 1 0 0 1 188 0 0 0 0 0 1 0 0 1 188 0 0 0 0 0 1 0 0 1 188 0 0 0 0 0 0 1 0 0 1	DBS NUMBER TRYDAY 181 93060-3542 1123.00 182 93060-3542 1431.00 183 93060-3542 1325.00 184 93060-3542 1638.00 185 93060-3542 1638.00 186 93230-3504 229.00 187 93230-3504 393.00 188 93230-3504 393.00 188 93230-3504 505.00 181 0 0 0 0 0 1 0 0 1 0 1 0 182 0 0 0 0 0 1 0 0 1 0 183 0 0 0 0 0 1 0 0 1 0 184 0 0 0 0 0 1 0 0 1 0 185 0 0 0 0 0 0 1 0 0 1 0 186 0 0 0 0 0 1 0 0 1 0 187 0 0 0 0 1 0 0 1 0 188 0 0 0 0 0 1 0 0 1 0 188 0 0 0 0 0 1 0 0 1 0 188 0 0 0 0 0 1 0 0 1 0 189 0 0 0 0 0 1 0 0 1 0 180 0 0 0 0 1 0 0 1 0 180 0 0 0 0 0 1 0 0 1 0 180 0 0 0 0 0 1 0 0 1 0 180 0 0 0 0 0 1 0 0 1 0 180 0 0 0 0 0 1 0 0 1 0 180 0 0 0 0 0 1 0 0 1 0 180 0 0 0 0 0 1 0 0 1 0 180 0 0 0 0 0 1 0 0 1 0 180 0 0 0 0 0 1 0 0 1 0 180 0 0 0 0 0 1 0 0 1 0 180 0 0 0 0 0 1 0 0 1 0 180 0 0 0 0 0 1 0 0 0 1 0 180 0 0 0 0 0 1 0 0 0 1 0 180 0 0 0 0 0 1 0 0 0 1 0 180 0 0 0 0 0 1 0 0 0 1 0 180 0 0 0 0 0 1 0 0 0 1 0 180 0 0 0 0 0 1 0 0 0 1 0 180 0 0 0 0 0 0 1 0 0 0 1 0 180 0 0 0 0 0 1 0 0 0 1 0 180 0 0 0 0 0 0 1 0 0 0 1 0 180 0 0 0 0 0 0 0 0 0 0 0 0 0 180 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 180 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 180 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 180 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 180 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 180 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 180 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 180 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 180 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 180 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	DBS NUMBER TN/DAY 181 93060-3542 1123.00 182 93060-3542 1431.00 183 93060-3542 1325.00 184 93060-3542 1638.00 185 93060-3542 1638.00 186 93230-3504 229.00 187 93230-3504 393.00 188 93230-3504 393.00 188 93230-3504 605.00 DBS F4 F5 F6 F7 F8 F9 F10 F11 F12 F13 A1 181 0 0 0 0 0 0 1 0 0 1 0 182 0 0 0 0 0 1 0 0 1 0 183 0 0 0 0 0 1 0 0 1 0 184 0 0 0 0 0 1 0 0 1 0 185 0 0 0 0 0 0 1 0 0 1 0 186 0 0 0 0 0 1 0 0 1 0 187 0 0 0 0 1 0 0 1 0 188 6 0 0 0 0 0 1 0 0 1 0 188 6 0 0 0 0 0 1 0 0 1 0 188 6 0 0 0 0 0 1 0 0 1 0 188 6 0 0 0 0 0 1 0 0 1 0 187 0 0 0 0 0 1 0 0 1 0 188 6 0 0 0 0 0 1 0 0 1 0 187 0 0 0 0 0 1 0 0 1 0 187 0 0 0 0 0 1 0 0 1 0 187 0 0 0 0 0 1 0 0 1 0 187 0 0 0 0 0 1 0 0 1 0 187 0 0 0 0 0 1 0 0 1 0 187 0 0 0 0 0 1 0 0 0 1 0 187 0 0 0 0 0 1 0 0 0 1 0 187 0 0 0 0 0 1 0 0 0 1 0 187 0 0 0 0 0 1 0 0 0 1 0 187 0 0 0 0 0 1 0 0 0 1 0 187 0 0 0 0 0 1 0 0 0 1 0 187 0 0 0 0 0 1 0 0 0 1 0 187 0 0 0 0 0 1 0 0 0 1 0 187 0 0 0 0 0 1 0 0 0 1 0 187 0 0 0 0 0 0 1 0 0 0 1 0 187 0 0 0 0 0 0 1 0 0 0 1 0 187 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 187 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	DBS NUMBER TN/DAY F1 181 93060-3542 1123.00 24385.00 182 93060-3542 1431.00 24385.00 183 93060-3542 1325.00 24385.00 184 93060-3542 1325.00 24385.00 185 93060-3542 1163.00 24385.00 186 93230-3504 229.00 5588.00 187 93230-3504 393.00 5588.00 DBS F4 F5 F6 F7 F8 F9 F10 F11 F12 F13 A1 181 0 0 0 0 0 0 1 0 0 1 0 182 0 0 0 0 0 1 0 0 1 0 183 0 0 0 0 0 1 0 0 1 0 184 0 0 0 0 0 0 1 0 0 1 0 185 0 0 0 0 0 0 1 0 0 1 0 186 0 0 0 0 0 0 1 0 0 1 0 187 0 0 0 0 0 1 0 0 1 0 188 0 0 0 0 0 0 1 0 0 1 0 188 0 0 0 0 0 0 1 0 0 1 0 188 0 0 0 0 0 0 1 0 0 1 0 189 0 0 0 0 0 1 0 0 1 0 180 0 0 0 0 0 1 0 0 1 0 180 0 0 0 0 0 1 0 0 1 0 180 0 0 0 0 0 1 0 0 1 0 180 0 0 0 0 0 1 0 0 1 0 180 0 0 0 0 0 1 0 0 1 0 180 0 0 0 0 0 1 0 0 1 0 180 0 0 0 0 0 1 0 0 1 0 180 0 0 0 0 0 1 0 0 1 0 180 0 0 0 0 0 1 0 0 1 0 180 0 0 0 0 0 1 0 0 0 1 0 180 0 0 0 0 0 1 0 0 0 1 0 180 0 0 0 0 0 1 0 0 0 1 0 180 0 0 0 0 0 1 0 0 0 1 0 180 0 0 0 0 0 1 0 0 0 1 0 180 0 0 0 0 0 1 0 0 0 1 0 180 0 0 0 0 0 1 0 0 0 1 0 180 0 0 0 0 0 1 0 0 0 1 0 180 0 0 0 0 0 1 0 0 0 1 0 180 0 0 0 0 0 1 0 0 0 1 0 180 0 0 0 0 0 0 1 0 0 0 1 0 180 0 0 0 0 0 1 0 0 0 1 0 180 0 0 0 0 0 1 0 0 0 1 0 180 0 0 0 0 0 1 0 0 0 1 0 180 0 0 0 0 0 1 0 0 0 1 0 180 0 0 0 0 0 1 0 0 0 1 0 180 0 0 0 0 0 0 0 1 0 0 0 1 0 180 0 0 0 0 0 1 0 0 0 1 0 180 0 0 0 0 0 0 1 0 0 0 1 0 180 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	DBS NUMBER TN/DAY F1 F2 181 93060-3542 1123.00 24385.00 4039137 182 93060-3542 1431.00 24385.00 4039137 183 93060-3542 1325.00 24385.00 4039137 184 93060-3542 1325.00 24385.00 4039137 185 93060-3542 1638.00 24385.00 4039137 186 93230-3504 229.00 5588.00 413419 187 93230-3504 393.00 5588.00 413419 188 93230-3504 605.00 5588.00 413419 DBS F4 F5 F6 F7 F8 F9 F10 F11 F12 F13 A1 181 0 0 0 0 0 0 1 0 0 1 0 0 1 0 0 1 0 0 1 0 0 1 0

OBS		JEC IBER	r				PROI	DUCTION LF/	ON RAT	ΓE	F1		F2
1	020	10-3	3532					152	0		1281	177	CDE 00
2		10-3						140			1281		625.00
3		10-3						84			1281		625.00
4		10-3						120			1281		625.00
5		10-3						166					625.00
6		60-3						120			1281		625.00
7		60-3									3000		100.35
8		60-3						128			3000		100.35
9		60-3						60.			3000		100.35
10		60-3						64.			3000		100.35
11		40-3						64.			3000		100.35
12		40-3						48.			472		775.00
13		40-3						36.			472		775.00
14		40-3						34.			472		775.00
15		05-3						80.			472		775.00
16		05-3						5.			80		358.00
								3.			80	3398	358.00
17		05-3						6.			80	3398	358.00
		05-3						56.			80	3398	358.00
		05-3						8.			80	3398	358.00
20	120	20-3	534					16.	0		118	13693	59.00
OBS	F3	F4	F5	F6	F7	F8							
ODD	13	14	rs	10	F /	rs	F9	F10	F11	F12	F13	ST1	ST2
1	1	0	0	0	0	0	1	0	0	0	1	4.0	24
2	1	0	0	0	0	0	1	0	0	0	1	4.0	24
3	1	0	0	0	0	0	1	0	0	0	1	4.0	24
4	1	0	0	0	0	0	1	0	0	0	1	3.5	18
5	1	0	0	0	0	0	1	0	0	0	1	6.0	18
6	0	0	0	1	0	0	1	0	0	0	1	4.0	24
7	0	0	0	1	0	0	1	0	0	0	1	4.0	18
8	0	0	0	1	0	0	1	0	0	O	1	4.0	24
9	0	0	0	1	0	0	1	0	0	0	1	4.0	24
10	0	0	0	1	0	0	1	0	0	ō	1	4.0	18
11	1	0	0	0	0	0	0	0	0	1	ō	3.0	24
12	1	0	0	0	0	0	0	0	ō	1	ō	3.0	24
13	1	0	0	0	0	0	0	0	Ō	ī	ō	3.0	24
14	1	0	0	0	0	0	ō	ō	Ö	ī	Ö	3.0	24
15	0	0	0	0	1	0	ī	ō	ō	ō	ĭ	4.0	24
16	0	0	0	0	1	0	1	ō	ō	ő	ī	5.0	24
17	0	0	0	0	1	ō	ī	ō	ő	Ö	î	5.0	24
18	0	0	0	ō	ī	ō	ī	ŏ	ő	0	1	2.0	18
19	0	0	0	ō	ī	ō	ī	ő	ŏ	0	1	2.0	18
20	1	0	0	0	0	ō	ī	ō	o	Ö	ī	4.0	18

OBS		JECT IBER	r				PROI	DUCTIO LF/I	ON RAT	ΓE	F1	F	2
21 22		20-3 20-3						8. 16.	. 0		118 118	1369	
23		20-3							. 0		118	13693 13693	
24		20-3						71.			118		
25		50-3						64.				13693	
26		50-3						52.			•	29974	
27		50-3						60.			•	29974	
28		50-3						96.			•	29974	
29		50-3						174.			•	29974	
30		90-3									.:	29974	
31		90-3						8.			12	18163	
32		70-3						4.			12	18163	
33		70-3						8.			76	1436	
34		70-3						20.			76	1436	
35		70-3						8.			76	1436	
36		40-3						40.			76	1436	
37		40-3						108.			176	1825	
38		60-3						44.			176	1825	
39		60-3						76.			314	40265	
40		60-3						64.			314	40265	
40	400	00-3	506					88.	0		314	40265	96
OBS	F3	F4	F5	F6	F7	F8	F9	F10	F11	F12	F13	ST1	ST2
21	1	0	0	0	0	0	1	0	0	0	1	10.0	72
22	1	0	0	0	0	ō	ī	ō	ő	ō	ī	10.0	72
23	1	0	0	0	0	ō	ī	ō	ő	Ö	ī	10.0	72
24	1	0	0	ō	ō	ō	ī	ŏ	ő	Ö	1	2.5	12
25	0	0	0	1	ō	i	ō	Ö	o	ő	1	7.0	15
26	0	0	0	1	o	ī	ō	ŏ	ŏ	ő	i	7.0	15
27	0	0	0	1	ō	ī	ō	ŏ	Ö	ő	i	7.0	18
28	0	0	0	1	ō	ī	ő	ŏ	ő	Ö	i	7.0	24
29	0	0	0	ī	ō	ī	ő	ŏ	ő	Ö	1	7.0	36
30	1	0	0	0	ō	ī	ő	Ö	í	ő	ō	3.0	24
31	1	0	0	ō	ō	ī	ō	ő	ī	ő	ő	3.0	24
32	0	0	1	ō	ō	ī	ő	ŏ	ī	ő	Ö	4.0	
33	0	0	1	ō	ō	ī	ō	ŏ	î	Ö	0		18
34	0	ō	ī	ō	ō	î	Ö	ő	i	0	0	4.0	18
35	ō	Ö	î	ō	ő	i	0	0	1	0	0	3.0	30
36	ō	ō	ō	Ö	o	ō	0	0	0			3.0	18
37	ō	ō	ŏ	Ö	Ö	Ö	0	0		0	1	8.0	24
38	ĭ	ō	ō	Ö	ő	1	0	0	0		1	8.0	24
39	ī	Ö	ŏ	Ö	Ö	1	0	0	0	0	1	4.0	18
40	î	ō	ō	Ô	ő	ī	0	o	0	0	1	4.0	18 18

OBS		JECT IBER	r				PROI	DUCTION LF/	ON RAY	ΓE	F1		F2
41 42 43 44 45 46 47 48 49 55 55 55 55 55 55 56 56 56 56 56 56 56	506 506 506 506 530 530 530 570 570 570 570 570	060-3 50-35 60-35 60-35 60-35 330-3 330-3 330-3 330-3 330-3 30-3	510 510 510 510 510 5510 5510 5510 5515 548 548 548 558					10 7: 33 64 7: 64 9: 88 102 7: 7: 144 100 16 32 56 8 8	2 2 4 4 3 3 4 4 4 4 4 4 4 4 4 4 4 4 4 4		314 557 5059 5059 5059 5059 95 3034 765 765	17: 17: 17: 17: 72: 72: 72: 72: 72: 76: 76: 76: 76: 76: 76: 76: 76: 76: 76	26596 13257 13257 13257 13257 13257 13257 15257 05002 05002 05002 05002 04647 78699 78699 78699 78699 78699 78699 78699 78699 78699 78699
OBS	F3	F4	F5	F6	F7	F8	F9	F10	F11	F12	F13	ST1	ST2
41 42 43 44 45 47 48 49 55 55 55 55 55 55 55 56 56 56 56 56 56	1 1 1 1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 1	000000000000000000000000000000000000000	000000000000000000000000000000000000000	0 0 0 0 0 1 1 1 1 1 0 0 0 0	000000000000000000000000000000000000000	111111111111111111111111111111111111111	000000000000000000000000000000000000000		0 1 1 1 1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 1 1 1 1 0 0 0 0	1 0 0 0 0 0 0 0 0 0 0 0 0 0	4.0 3.5 3.5 3.5 3.5 5.0 4.0 7.0 7.0 4.0 7.0 7.0	18 18 18 18 18 15 15 15 14 42 42 42 46 60 60

OBS		JECT IBER	r				PROI	UCTIO LF/I	ON RAT	ΓE	F1		F2
61 62 63 64 65 66 67 68 70 71 72 73 74 75 77 78 80	570 570 570 570 580 610 610 610 721 721 721 721 791	L 0 0 0 0 0 L 0 0 0 0						168 36 40 12 12 24 64 81 16 120 72 128 80 24 136		1 1 1	765 765 125 125 125 125 125 307 307 307 307 307 4377 4377 4377 4377	399 370 370 370 370 370 244 244 33 33 33 400 401 401 401 56	54939 34203 34203 34203 34203 34203 34203 34203 360043 360043 360043 360043 360077 16077 16077
OBS	F3	F4	F5	F6	F7	F8	F9	F10	F11	F12	F13	ST1	ST2
61 62 63 64 65 66 67 71 72 73 74 75 77 78 80	1 1 0 0 0 0 0 0 1 1 1 1 1 1 1 1 1 1					0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 1 1 1 1 0 0 1 1 1 1 1 1 1 1			0 0 0 0 0 0 0 0 1 1 1 1 1 0 0 0 0	1 1 1 1 1 1 0 0 0 0 0 0 0	7.0 4.0 9.0 9.0 9.0 9.0 4.0 5.0 5.0 4.0 4.0 7.0 7.0 7.0 4.0	60 15 36 36 48 42 42 30 30 24 24 24 15 36 36 36 36 36

OBS		JECT MBER	r				PROI	OUCTIO LF/I	ON RAS	ΓE	Fl		F2
81 82 83 84 85 86 87 88 99 91 93 94 95 97	791 791 791 791 791 870 870 870 930 930 930	170-3 170-3 190-3 190-3 190-3 190-3 055-3 055-3 055-3 060-3 060-3	3510 3505 3505 3505 3505 3505 3601 3601 3601 3542 3542 542 542					80 10 24 48 36 48 150 24 80 72 100 88 58	5 4 4 4 3 3 5 5 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9		266 266 232 232 232 232 7413 7413 7413 800 800 800 800	79 79 79 79 180 180 180 403 403 403	53401 53401 96699 96699 96699 97970 97970 97970 97970 9137 9137 9137
OBS	F3	F4	F5	F6	F7	F8	F9	F10	F11	F12	F13	ST1	ST2
81 82 83 84 85 86 87 88 99 91 92 93 94 95 97	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	000000000000000000000000000000000000000	000000000000000000000000000000000000000	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0	1 1 1 1 1 1 1 1 1 1 1 0 0	4.0 4.0 3.0 4.0 3.0 6.5 6.5 6.5 7.0 7.0 7.0	30 30 18 18 18 18 30 30 30 18 18 18 18

APPENDIX C REGRESSION COMPUTER OUTPUT

Maximum R-square Improvement for Dependent Variable PROD_RT

DF Sum of Squares Mean Square

Step 1 Variable PRICE Entered R-square = 0.15062492 C(p) = 40.06365686

F Prob>	F		•	
Regressio 15.43	n 1 0.0002	92.42906827	92.42906827	
Error Total	87 88	521.20824479 613.63731306	5.99089937	
Variable F Prob>	Parameter Estimate F	Standard Error	Type II Sum of Squares	•
INTERCEP 12.55	1.36975453 0.0006	0.38663997	75.19068029	
PRICE 15.43	0.00000032 0.0002	0.0000008	92.42906827	
Bounds on	condition number:	1,	1	

The above model is the best 1-variable model found.

Step 2 Variable TOT_QTY2 Entered R-square = 0.21251067 C(p) = 32.95147626

F Prob>	DF F	Sum of Squares	Mean Square
Regressic	on 2 0.0001	130.40447836	65.20223918
Error	86	483.23283470	5.61898645
Total	88	613.63731306	5101030045
Variable F Prob>	Parameter Estimate F	Standard Error	Type II Sum of Squares
INTERCEP 6.79	1.03277691 0.0108	0.39624743	38.17140222
PRICE 20.65	0.00000058 0.0001	0.00000013	116.04700470
TOT_QTY2	-0.00008317 0.0110	0.00003199	37.97541009

Bounds on condition number:	2.64274,	10.57096

The above model is the best 2-variable model found.

Step 3 Variable TOT_QTY Entered R-square = 0.43631166 C(p) = 1.99857940

F Prob>	DF F	Sum of Squares	Mean Square
Regressio 21.93	n 3 0.0001	267.73711333	89.24570444
Error Total	85 88	345.90019972 613.63731306	4.06941411
Variable F Prob>	Parameter Estimate F	Standard Error	Type II Sum of Squares
INTERCEP 0.05	0.08076872 0.8300	0.37492402	0.18885644
TOT_QTY 33.75	0.07537392 0.0001	0.01297479	137.33263497
PRICE 6.46	0.00000030 0.0128	0.0000012	26.30216390
TOT_QTY2 43.08	-0.00039076 0.0001	0.00005954	175.29338216
Bounds on	condition number:	15.08104,	92.62268

The above model is the best 3-variable model found.

Step 4 Variable RURAL Entered R-square = 0.45342082 C(p) = 1.47939235

F Prob>F	DF	Sum of Squares	Mean Square
Regression 17.42 0.0	4	278.23593522	69.55898381
Error	84	335.40137783	3.99287355
Total	88	613.63731306	
Variable	Parameter	Standard	Type II
F Prob>F	Estimate	Error	Sum of Squares

INTERCEP 0.86	0.38702458 0.3556	0.41664732	3.44528752
TOT_QTY	0.08437640 0.0001	0.01400005	145.03360090
PRICE	0.00000018 0.2109	0.0000014	6.34741727
RURAL 2.63	-0.95298576 0.1086	0.58770435	10.49882189
TOT_QTY2	-0.00039573 0.0001	0.00005906	179.29930271
Bounds on	condition number:	17.89518,	147.1689

The above model is the best 4-variable model found.

Step 5 Variable TYP_H Entered R-square = 0.46493459 C(p) = 1.78408213

F Prob>	DF F	Sum of Squares	Mean Square	
Regression 5 285.30121452 57.06024290				
Error Total	83 88	328.33609854 613.63731306	3.95585661	
Variable F Prob>	Parameter Estimate F	Standard Error		
INTERCEP 0.05		0.46496727	0.20570544	
TOT_QTY 36.02	0.09386976 0.0001	0.01564112	142.48076542	
	0.3076	0.0000014	4.16820816	
4.19	-1.32744576 0.0439	0.64861683	16.56905278	
TOT_QTY2 43.61 TYP_H		0.00006599	172.52921151	
1.79	0.70348510	0.52639349	7.06527929	
Bounds on	condition number	22.5454,	233.8393	

The above model is the best 5-variable model found.

Step 6 Variable MEDIUM Entered R-square = 0.48172237 C(p) = 1.31221681

F Prob>	DF F	Sum of Squares	Mean Square
	on 6 0.0001	295.60282106	49.26713684
Error Total	82 88	318.03449199 613.63731306	3.87846941
Variable F Prob>		Standard Error	Type II Sum of Squares
INTERCEP 0.32		0.47094763	1.25209181
TOT_QTY 38.80	0.09742953 0.0001	0.01564064	150.49862334
1 15	0.00000015 0.2876	0.0000014	4.44294207
RURAL 4.61	-1.38114286 0.0347	0.64308574	17.88956667
	-0.80134930 0.1070	0.49169927	10.30160654
	-0.00044383 0.0001 1.03567613	0.00006553	177.91859377
3.42	0.0678	0.55965674	13.28204138
Bounds on	condition number:	22.99384,	293.5325

The above model is the best 6-variable model found.

Step 7 Variable TYP_M Entered R-square = 0.48521947 C(p) = 2.79729688

F Prob>F	, DF	Sum of Squares	Mean Square
Regression	7 0.0001	297.74877231	42.53553890
Error	81	315.88854074	3.89985853
Total	88	613.63731306	
Variable	Parameter	Standard	Type II
	Estimate	Error	Sum of Squares

F Prob>F

C(p) = 4.34083423

0.48 0.4883

RURAL

INTERCEP 0.14	-0.36818386 0.7077	0.97855681	0.55208539
TOT_QTY 36.08	0.10237788 0.0001	0.01704341	140.71756535
PRICE 1.61	0.00000019	0.0000015	6.29111261
RURAL	0.2077 -1.39804647	0.64525905	18.30728148
4.69 MEDIUM	0.0332 -0.82961686	0.49452363	10.97564111
2.81 TOT_QTY2	0.0973 -0.00047133	0.00007544	152.20737515
39.03 TYP_M	0.0001 0.59187014	0.79788616	2.14595125
0.55 TYP H	0.4604 1.51850631	0.85942035	12.17505092
3.12	0.0810		12.17303032
Bounds on	condition number:	27.15356,	453.581

The above model is the best 7-variable model found.

Step 8 Variable RC Entered R-square = 0.48831956

F Prob>	DF F	Sum of Squares	Mean Square
Regressio 9.54	n 8 0.0001	299.65110032	37.45638754
Error	80	313.98621273	3.92482766
Total	88	613.63731306	***************************************
Variable F Prob>	Parameter Estimate F	Standard Error	Type II Sum of Squares
INTERCEP 0.34	-0.61099370 0.5592	1.04179745	1.34998042
TOT_QTY 35.96	0.10501718 0.0001	0.01751312	141.12834200
PRICE 1.48	0.00000018 0.2280	0.00000015	5.79117159

0.31437043 0.45155358

-1.51498812 0.66875974 20.14182422

1.90232801

The above model is the best 8-variable model found.

5.13 0.0262

Step 9 Variable II Entered R-square = 0.49317558 C(p) = 5.62582444			
F Prob>	DF F	Sum of Squares	Mean Square
Regressio	n 9 0.0001	302.63093479	33.62565942
Error Total	79 88	311.00637826 613.63731306	3.93678960
Variable F Prob>		Standard Error	Type II Sum of Squares
INTERCEP 0.86	-1.10225839 0.3557	1.18637934	3.39830127
TOT_QTY	0.11122891 0.0001	0.01893730	135.81306828
PRICE 2.01	0.00000023	0.00000016	7.92988721
RC 0.95	0.47682142 0.3328	0.48927240	3.73897258
II 0.76	0.97774329 0.3869	1.12382808	2.97983447
RURAL 4.96	-1.49230691 0.0288	0.67028525	19.51367978
MEDIUM 3.37	-1.00587714 0.0700	0.54755541	13.28543940
TOT_QTY2 36.07	-0.00051139 0.0001	0.00008515	141.99375802
TYP_M 0.90	0.77859711 0.3455	0.82046436	3.54526205

TYP_H 1.96018373 0.95719985 16.50937070 4.19 0.0439

Bounds on condition number: 33.20906, 734.8667

The above model is the best 9-variable model found.

Step10 Variable LIMITED Entered R-square = 0.49582888 C(p) = 7.23514629

F Prob>	DF F	Sum of Squares	Mean Square
Regression 10 7.67 0.0001		304.25910304	30.42591030
Error Total	78 88	309.37821001 613.63731306	3.96638731
Variable F Prob>		Standard Error	Type II Sum of Squares
INTERCEP 1.16		1.24909593	4.59083739
TOT_QTY 34.65	0.11247935 0.0001	0.01910828	137.43499259
PRICE 1.64	0.00000021 0.2034	0.0000016	6.52456837
RC 0.79		0.49433581	3.15219740
0.89		1.13770872	3.52506764
RURAL 3.96		0.69433812	15.72168423
LIMITED 0.41		1.23907561	1.62816825
MEDIUM 3.64		0.63237134	14.43232233
TOT_QTY2 36.21		0.00008592	143.61876993
TYP_M 1.30	1.08023486	0.94861609	5.14340263
TYP_H 4.26	0.2583 2.35424159 0.0424	1.14079014	16.89217850
Bounds on	condition number:	33.55915,	895.6969

The above model is the best 10-variable model found.

Step11 Variable NC Entered R-square = 0.49658671 C(p) = 9.12356181DF Sum of Squares Mean Square F Prob>F Regression 11 304.72413622 27.70219420 6.91 0.0001 Error 77 308.91317683 4.01185944 Total 88 613.63731306 Parameter Standard Type II Estimate Variable Error Sum of Squares F Prob>F INTERCEP -1.35204737 1.25646744 4.64544206 1.16 0.2853 TOT QTY 0.10749993 0.02414988 79.49360726 19.81 0.0001 PRICE 0.00000021 0.00000016 6.35370916 1.58 0.2120 0.58397583 0.65137903 3.22454100 0.80 0.3728 ΙT 1.09666737 1.14640246 3.67131235 0.92 0.3418 NC 0.36250468 1.06474228 0.46503318 0.12 0.7344 RURAL -1.35760176 0.70208480 15.00069418 3.74 0.0568 LIMITED 1.02248392 1.41555377 2.09317693 0.52 0.4723 MEDIUM -1.15247536 0.65531586 12.40816769 3.09 0.0826 TOT_QTY2 -0.00049982 0.00010005 100.11932536 24.96 0.0001 TYP M 1.03431793 0.96352370 4.62305450 1.15 0.2864 TYP H 2.24429855 1.19188967 14.22442925 3.55 0.0635

The above model is the best 11-variable model found.

Bounds on condition number: 52.99647, 1386.106

F Prob>	DF	Sum of Squares	Mean Square
Regressio	on 12 0.0001	305.21737435	25.43478120
Error Total	76 88	308.41993871 613.63731306	4.05815709
Variable F Prob>	Parameter Estimate F	Standard Error	. Type II Sum of Squares
INTERCEP 1.26	-1.47971862 0.2643	1.31568925	5.13310888
TOT_QTY 18.32	0.10587379 0.0001	0.02473264	74.36434713
PRICE 1.35	0.00000020 0.2485	0.00000017	5.48859078
RC 0.85	0.75709081 0.3600	0.82204733	3.44216077
NB 0.12	0.45762921 0.7283	1.31265274	0.49323812
1.03	1.24812000 0.3143	1.23212362	4.16421336
NC 0.23	0.62294483 0.6347	1.30569071	0.92373500
RURAL 3.16	-1.29502557 0.0795	0.72858005	12.82126825
LIMITED 0.64	1.27129778 0.4272	1.59256792	2.58599397
MEDIUM 3.17	-1.18419005 0.0791	0.66533462	12.85557248
TOT_QTY2 22.84	-0.00049218 0.0001	0.00010299	92.68607800
TYP_M 1.18	1.05694254 0.2799	0.97123790	4.80596237
TYP_H 3.17	2.16941759 0.0788	1.21783758	12.87764435
Bounds on	condition number:	54.95091,	1654.153

The above model is the best 12-variable model found.

Step13 Variable HEAVY Entered R-square = 0.49740696 C(p) = 13.00278630

F Prob	DF >F	Sum of Squares	Mean Square		
Regression 5.71	on 13 0.0001	305.22747341	23.47903642		
Error Total	75 88	308.40983965 613.63731306	4.11213120		
Variable F Prob		Standard Error	Type II Sum of Squares		
INTERCEP 0.54		2.12011034	2.23141329		
TOT_QTY	0.10534514	0.02708565	62.20389374		
PRICE 1.33	0.00000019 0.2527	0.0000017	5.46340208		
RC 0.79	0.76935595 0.3759	0.86371470	3.26272878		
NB 0.12	0.46724565 0.7274	1.33552552	0.50333034		
II 0.97	1.26508184 0.3287	1.28664961	3.97542553		
NC 0.22	0.64066488 0.6395	1.36211495	0.90970645		
RURAL 1.75	-1.26460744 0.1901	0.95636652	7.19001341		
LIMITED 0.45	1.32878210 0.5040	1.97876446	1.85432690		
MEDIUM 0.71	-1.12675576 0.4026	1.33855146	2.91377755		
HEAVY 0.00	0.08239762 0.9606	1.66267604	0.01009906		
TOT_QTY2 20.15	-0.00049047 0.0001	0.00010926	82.86370231		
TYP_M 1.17	1.05844360 0.2827	0.97814446	4.81500129		
TYP_H 2.97	2.18553138 0.0890	1.26829812	12.21063799		
Bounds on	condition number:	65.03905,	2338.732		

The above model is the best 13-variable model found.

F Prob	DF >>F	Sum of Squares	Mean Square	
Regression 14 5.23 0.0001		305.23908545	21.80279182	
Error Total	74 88	308.39822760 613.63731306	4.16754362	
Variable F Prob		Standard Error	Type II Sum of Squares	
INTERCEP 0.54		2.14480423	2.24141776	
TOT_QTY 14.51	0.10560883 0.0003	0.02772135	60.48557493	
PRICE 1.21	0.00000020 0.2741	0.00000018	5.05934014	
RC 0.78	0.76934750 0.3791	0.86951467	3.26265700	
NB 0.12	0.47189054 0.7272	1.34737028	0.51119755	
0.89	1.28723085 0.3475	1.36155905	3.72494675	
0.20 RURAL	0.62610578 0.6557 -1.29511776	1.39872566	0.83504618	
1.33 URBAN	0.2525 -0.05289078	1.12296615	5.54326110	
0.00 LIMITED	0.9580 1.30948176	1.00199544	0.01161204	
0.42 MEDIUM	0.5199 -1.13005921	1.34899245	1.74215733	
0.70 HEAVY	0.4049 0.09131215	1.68233925	0.01227750	
0.00 TOT_QTY2	0.9569 -0.00049196	0.00011354	78.24770388	
18.78 TYP_M	0.0001 1.10120523	1.27511778	3.10825100	
0.75 TYP_H 2.25	0.3906 2.22541984 0.1379	1.48367643	9.37617423	
Bounds or	n condition number:	67.222,	2796.588	

The above model is the best 14-variable model found. No further improvement in R-square is possible.

Model: MODEL1

Dependent Variable: PROD_RT

Analysis of Variance

Source Prob>F	DF	Sum Squar		Mean Square	F Value
Model 0.0001	13	305.227	47	23.47904	5.710
Error C Total	75 88	308.409 613.637		4.11213	
Root MSE Dep Mean C.V.	2	.02784 .49574 .25196		quare R-sq	0.4974 0.4103

Parameter Estimates

Variable	DF	Parameter Estimate	Standard Error	T for H0: Parameter=0
INTERCEP TOT_QTY PRICE RC NB II NC RURAL LIMITED MEDIUM HEAVY TOT_QTY2 TYP_M TYP_H	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	-1.561763 0.105345 0.000000195 0.769356 0.467246 1.265082 0.640665 -1.264607 1.328782 -1.126756 0.082398 -0.000490 1.058444 2.185531	2.12011034 0.02708565 0.00000017 0.86371470 1.33552552 1.28664961 1.36211495 0.95636652 1.97876446 1.33855146 0.0010926 0.97814446 1.66267604 0.0010926	-0.737 3.889 1.153 0.891 0.350 0.983 0.470 -1.322 0.672 -0.842 0.050 -4.489 1.082

variable	Dr	Prop > T
INTERCEP	1	0.4636
TOT_QTY	1	0.0002
PRICE	1	0.2527
RC	1	0.3759
NB	1	0.7274
II	1	0.3287

Variable DE

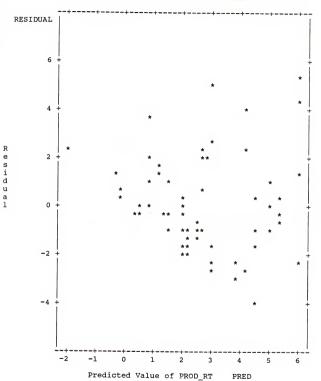
Variable	DF	Prob > T
NC	1	0.6395
RURAL	1	0.1901
LIMITED	1	0.5040
MEDIUM	1	0.4026
HEAVY	1	0.9606
TOT_QTY2	1	0.0001
TYP_M	1	0.2827
TYP_H	1	0.0890

	Dep Var	Predict	
Obs	PROD RT	Value	Residual
			Modiuuui
1	1.0000	1.3860	-0.3860
2	1.0000	1.3860	-0.3860
3	1.0000	1.3860	-0.3860
4	1.0000	1.3860	-0.3860
5	1.0000	1.3860	-0.3860
6	0.4000	1.5522	-1.1522
7	4.5000	5.2831	-0.7831
8	5.6500	5.2831	0.3669
9	5.6500	5.2831	0.3669
10	5.1000	5.2831	-0.1831
11	0.8400	3.0532	-2.2132
12	7.9800	3.0532	4.9268
13	5.8800	3.0532	2.8268
14	1.2600	3.0532	-1.7932
15	0.4200	3.0532	-2.6332
16	3.8000	6.0135	-2.2135
17	7.2500	6.0135	1.2365
18	11.1900	6.0135	5.1765
19	10.3300	6.0135	4.3165
20	10.3300	6.0135	4.3165
21	3.0000	1.2083	1.7917
22	3.0000	1.2083	1.7917
23	2.6500	1.2083	1.4417
24	0.1000		
25	0.1200		
26	1.1000	2.5281	-1.4281
27	1.4000	2.5281	-1.1281
28	1.3000	2.5281	-1.2281
29	1.7000	2.5281	-0.8281
30	1.6000	2.5281	-0.9281
31	0.4900		
32	0.1300		
33	0.2300		
34	0.2700		
35	0.6500		
36	4.8450	2.9148	1.9302
37	1.0400	-0.2763	1.3163
38	8.2300	4.1570	4.0730

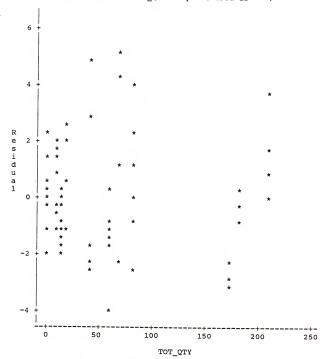
0bs	Dep Var PROD_RT	Predict Value	Residual
39	8.2300	4.1570	4.0730
40	1.6400	4.1570	-2.5170
41	6.5800	4.1570	2.4230
42	0.1300	-0.2350	0.3650
43	0.1700	-0.2350	0.3650
44	0.1300	-0.2350	0.3650
45	0.1300	-0.2350	0.3650
46	0.2900	-0.2350	0.5250
47	1.7000	3.8866	-2.1866
48	1.0000	3.8866	-2.8866
49	1.7000	3.8866	-2.1866
50	1.0000	3.8866	-2.8866
51	0.7500	3.8866	-3.1366
52	2.7000	0.8623	1.8377
53	4.5000	0.8623	3.6377
54	0.9000	0.8623	0.0377
55	1.8000	0.8623	0.9377
56	1.8000	0.8623	0.9377
57	0.0400	0.3518	-0.3118
58	0.0200	0.3518	-0.3318
59	0.0700	0.3518	-0.2818
60	0.0500	0.3518	-0.3018
61	0.0300	0.3518	-0.3218
62	0.1900	0.4340	-0.2440
63	0.2800	0.4340	-0.1540
64	0.5600	0.4340	0.1260
65	0.5700	0.4340	0.1360
66	0.5700	0.4340	0.1360
67	5.0000	4.9535	0.0465
68	4.0000	4.9535	-0.9535
69	6.0000	4.9535	1.0465
70	5.0000	4.9535	0.0465
71	5.0000	4.9535	0.0465
72	2.6400	4.4524	-1.8124
73	2.7000	4.4524	-1.7524
74	0.5000	4.4524	-3.9524
75	4.8200	4.4524	0.3676
76	3.5500	4.4524	-0.9024

	Dep Var	Predict	
0bs	PROD_RT	Value	Residual
77	0.0180	2 2422	
		2.0430	-2.0250
78	2.4000	1.4373	0.9627
79	0.4000	1.4373	-1.0373
80	1.0000	1.4373	-0.4373
81	1.8600	1.9712	-0.1112
82	2.3270	1.9712	0.3558
83	1.5710	1.9712	-0.4002
84	0.1780	1.9712	-1.7932
85	0.8320	1.9712	-1.1392
86	0.4000	2.1706	-1.7706
87	0.4000	2.1706	-1.7706
88	1.3000	2.1706	-0.8706
89	0.3000	2.1706	-1.8706
90	0.7000	2.1706	-1.4706
91	3.2000	2.6135	0.5865
92	4.5000	2.6135	1.8865
93	1.6000	2.6135	-1.0135
94	1.6000	2.6135	-1.0135
95	5.1000	2.6135	2.4865
96	0.2500	-2.0184	2.2684

Sum of Residuals 3.23741E-13 Sum of Squared Residuals 308.4098 Predicted Resid SS (Press) 446.2084

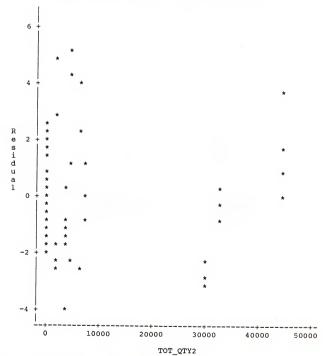


PREDICTION MODEL FOR CLEAR AND GRUBB
Plot of YRESID*TOT_QTY. Symbol used is '*'.

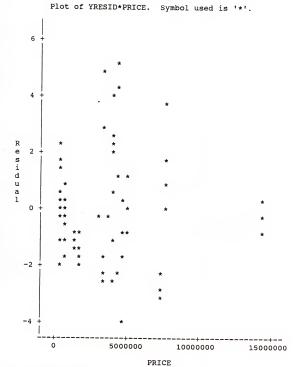


NOTE: 7 obs had missing values. 31 obs hidden.

Plot of YRESID*TOT_QTY2. Symbol used is '*'.



NOTE: 7 obs had missing values. 42 obs hidden.



NOTE: 7 obs had missing values. 31 obs hidden.

Model: MODEL1

Dependent Variable: LOG PR

Analysis of Variance

Source Prob>F	DF	Sum Squar		F Value
Model 0.0001	12	133.838	73 11.15323	14.180
Error C Total	76 88	59.778 193.617		
Root MSE Dep Mean C.V.	0.	.88688 .17149 .15764	R-square Adj R-sq	0.6913 0.6425

NOTE: Model is not full rank. Least-squares solutions for the parameters are not unique. Some statistics will be misleading. A reported DF of 0 or B means that the estimate is biased.

The following parameters have been set to 0, since the

The following parameters have been set to 0, since the variables are a linear combination of other variables as shown.

SG = 0 HEAVY = +1.0000 * INTERCEP -1.0000 * LIGHT -1.0000 * MEDIUM -1.0000

Parameter Estimates

Variable	DF	Parameter Estimate	Standard Error	T for H0: Parameter=0
INTERCEP LOG_TQ RC RC NB II NC SG LIGHT MEDIUM HEAVY TYP_H RURAL URBAN LIMITED	B 1 1 1 0 B 0 1 1 1	-1.181892 0.567505 0.692154 0.705082 0.122397 0.330528 0.0283303 0.0554329 0-0.244324 -0.021495 -1.139281 -0.578627 -0.259863	0.48379543 0.11593198 0.43686895 0.62029991 0.57842904 0.62131457 0.00000000 0.66418594 0.38889080 0.00000000 0.47547398 0.55547019 0.39578642 0.40836230 0.70858268	-2.443 4.895 1.584 1.137 0.212 0.532 0.427 0.140 -0.514 -0.039 -2.879 -1.417 -0.367

Variable	DF	Prob > T
INTERCEP	В	0.0169
LOG TQ	1	0.0001
RC _	1	0.1173
NB	1	0.2592
II	1	0.8330
NC	1	0.5963
SG	0	
LIGHT	В	0.6709
MEDIUM	В	0.8893
HEAVY	0	
TYP_M	1	0.6088
TYP_H	1	0.9691
RURAL	1	0.0052
URBAN	1	0.1606
LIMITED	1	0.7148

Obs	Dep Var LOG_PR	Predict Value	Std Err Predict	Lower95% Mean	Upper95% Mean
1 2	0	0.1575	0.378	-0.5944	0.9094
2	0	0.1575	0.378	-0.5944	0.9094
3	0	0.1575	0.378	-0.5944	0.9094
4	0	0.1575	0.378	-0.5944	0.9094
5	0	0.1575	0.378	-0.5944	0.9094
6	-0.9163	-1.6099	0.458	-2.5230	-0.6968
7	1.5041	2.2518	0.366	1.5231	2.9804
8	1.7317	2.2518	0.366	1.5231	2.9804
9	1.7317	2.2518	0.366	1.5231	2.9804
10	1.6292	2.2518	0.366	1.5231	2.9804
11	-0.1744	0.1633	0.245	-0.3242	0.6509
12	2.0769	0.1633	0.245	-0.3242	0.6509
13	1.7716	0.1633	0.245	-0.3242	0.6509
14	0.2311	0.1633	0.245	-0.3242	0.6509
15 16	-0.8675	0.1633	0.245	-0.3242	0.6509
17	1.3350	0.7326	0.295	0.1441	1.3210
18	1.9810 2.4150	0.7326	0.295	0.1441	1.3210
19	2.3351	0.7326	0.295	0.1441	1.3210
20	2.3351	0.7326	0.295	0.1441	1.3210
21	1.0986	0.7326	0.295	0.1441	1.3210
22	1.0986	0.7675	0.395	-0.0195	1.5545
23	0.9746	0.7675	0.395	-0.0195	1.5545
24	-2.3026	0.7675	0.395	-0.0195	1.5545
25	-2.1203	•	•	•	
26	0.0953	0.4751	0.310		
27	0.3365	0.4751	0.310	-0.1414	1.0917
28	0.2624	0.4751	0.310	-0.1414	1.0917
29	0.5306	0.4751	0.310	-0.1414	1.0917
30	0.4700	0.4751	0.310	-0.1414 -0.1414	1.0917
31	-0.7133	0.1751	0.310	-0.1414	1.0917
32	-2.0402	•	•	•	•
33	-1.4697		•	•	•
34	-1.3093		•	•	•
35	-0.4308	•	:	•	•
36	1.5779	0.7905	0.646	-0.4953	2.0763
37	0.0392	-1.4040	0.476	-2.3514	-0.4565
38	2.1078	0.8736	0.404	0.0682	1.6790

PREDICTION MODEL FOR CLEARING AND GRUBBING

	Dep Var	Predict	Std Err	Lower95%	Upper95%
0bs	LOG_PR	Value	Predict	Mean	Mean
	_				110411
39	2.1078	0.8736	0.404	0.0682	1.6790
40	0.4947	0.8736	0.404	0.0682	1.6790
41	1.8840	0.8736	0.404	0.0682	1.6790
42	-2.0402	-1.9203	0.377	-2.6710	-1.1697
43	-1.7720	-1.9203	0.377	-2.6710	-1.1697
44	-2.0402	-1.9203	0.377	-2.6710	-1.1697
45	-2.0402	-1.9203	0.377	-2.6710	-1.1697
46	-1.2379	-1.9203	0.377	-2.6710	-1.1697
47	0.5306	0.9634	0.227	0.5121	1.4148
48	0	0.9634	0.227	0.5121	1.4148
49	0.5306	0.9634	0.227	0.5121	1.4148
50	0	0.9634	0.227	0.5121	1.4148
51	-0.2877	0.9634	0.227	0.5121	1.4148
52	0.9933	1.0767	0.233	0.6119	1.5415
53	1.5041	1.0767	0.233	0.6119	1.5415
54	-0.1054	1.0767	0.233	0.6119	1.5415
55	0.5878	1.0767	0.233	0.6119	1.5415
56	0.5878	1.0767	0.233	0.6119	1.5415
57	-3.2189	-2.4878	0.331	-3.1480	-1.8275
58	-3.9120	-2.4878	0.331	-3.1480	-1.8275
59	-2.6593	-2.4878	0.331	-3.1480	-1.8275
60	-2.9957	-2.4878	0.331	-3.1480	-1.8275
61	-3.5066	-2.4878	0.331	-3.1480	-1.8275
62	-1.6607	-0.9276	0.397	-1.7175	-0.1376
63	-1.2730	-0.9276	0.397	-1.7175	-0.1376
64	-0.5798	-0.9276	0.397	-1.7175	-0.1376
65	-0.5621	-0.9276	0.397	-1.7175	-0.1376
66	-0.5621	-0.9276	0.397	-1.7175	-0.1376
67	1.6094	1.1192	0.342	0.4376	1.8008
68	1.3863	1.1192	0.342	0.4376	1.8008
69	1.7918	1.1192	0.342	0.4376	1.8008
70	1.6094	1.1192	0.342	0.4376	1.8008
71	1.6094	1.1192	0.342	0.4376	1.8008
72	0.9708	1.4421	0.369	0.7073	2.1769
73	0.9933	1.4421	0.369	0.7073	2.1769
74	-0.6931	1.4421	0.369	0.7073	2.1769
75	1.5728	1.4421	0.369	0.7073	2.1769
76	1.2669	1.4421	0.369	0.7073	2.1769

PREDICTION MODEL FOR CLEARING AND GRUBBING

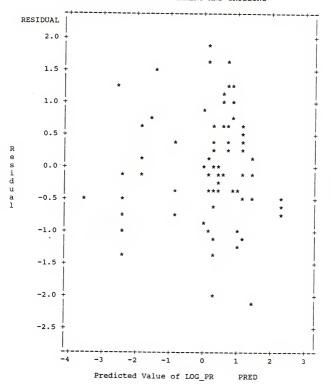
٥١ -	Dep Var	Predict	Std Err	Lower95%	Upper95%
0bs	LOG_PR	Value	Predict	Mean	Mean
77	-4.0174	-3.5461	0.637	-4.8143	-2.2780
78	0.8755	-0.0212	0.201	-0.4207	
79	-0.9163	-0.0212	0.201		0.3783
80	0	-0.0212	0.201	-0.4207	0.3783
81	0.6206	0.2232	0.201	-0.4207	0.3783
82	0.8446	0.2232	0.207	-0.1892	0.6356
83	0.4517	0.2232	0.207	-0.1892	0.6356
84	-1.7260	0.2232	0.207	-0.1892	0.6356
85	-0.1839	0.2232	0.207	-0.1892	0.6356
86	-0.9163	0.2241	0.207	-0.1892	0.6356
87		0.2241	0.207	-0.1884	0.6366
88	0.2624	0.2241	0.207	-0.1884	0.6366
89	-1.2040	0.2241	0.207	-0.1884	0.6366
90	-0.3567	0.2241	0.207	-0.1884	0.6366
91	1.1632	0.5379	0.330	-0.1884	0.6366
92	1.5041	0.5379	0.330	-0.1184 -0.1184	1.1943
93	0.4700	0.5379	0.330	-0.1184	1.1943
94	0.4700	0.5379	0.330	-0.1184	1.1943
95	1.6292	0.5379	0.330	-0.1184	1.1943
96	-1.3863	-2.6057	0.668	-3.9366	1.1943 -1.2749
		2.0057	0.008	-3.9366	-1.2/49
	Lower95%	Upper95%			
0bs	Predict	Predict	Residual		
1	-1.7623	2.0772	-0.1575		
2	-1.7623	2.0772	-0.1575		
3	-1.7623	2.0772	-0.1575		
4	-1.7623	2.0772	-0.1575		
5	-1.7623	2.0772	-0.1575		
6	-3.5983	0.3786	0.6936		
7	0.3410	4.1625	-0.7477		
8	0.3410	4.1625	-0.5201		
9	0.3410	4.1625	-0.5201		
10	0.3410	4.1625	-0.6225		
11	-1.6691	1.9958	-0.3377		
12	-1.6691	1.9958	1.9136		
13	-1.6691	1.9958	1.6082		
14	-1.6691	1.9958	0.0678		

	Lower95%	Upper95%	
0bs	Predict	Predict	Residual
15	1 6601		
15	-1.6691	1.9958	-1.0308
16	-1.1292	2.5944	0.6024
17	-1.1292	2.5944	1.2484
18	-1.1292	2.5944	1.6824
19	-1.1292	2.5944	1.6025
20	-1.1292	2.5944	1.6025
21	-1.1662	2.7013	0.3311
22	-1.1662	2.7013	0.3311
23	-1.1662	2.7013	0.2070
24	•	•	
25			
26	-1.3957	2.3460	-0.3798
27	-1.3957	2.3460	-0.1387
28	-1.3957	2.3460	-0.2128
29	-1.3957	2.3460	0.0555
30	-1.3957	2.3460	-0.00514
31 32	•	•	
32	•	•	
34	•	•	
35	•	•	•
36	-1.3943		:
37	-3.4084	2.9753	0.7875
38	-1.0677	0.6005	1.4432
39	-1.0677	2.8150	1.2342
40	-1.0677	2.8150	1.2342
41	-1.0677	2.8150	-0.3789
42	-3.8396	2.8150	1.0104
43	-3.8396	-0.00107	-0.1199
44	-3.8396	-0.00107	0.1484
45	-3.8396	-0.00107	-0.1199
46	-3.8396	-0.00107 -0.00107	-0.1199
47	-0.8597	2.7866	0.6825
48	-0.8597	2.7866	-0.4328
49	-0.8597	2.7866	-0.9634 -0.4328
50	-0.8597	2.7866	-0.4328
51	-0.8597	2.7866	-1.2511
52	-0.7498	2.7866	-0.0834
	0.7430	4.3032	-0.0834

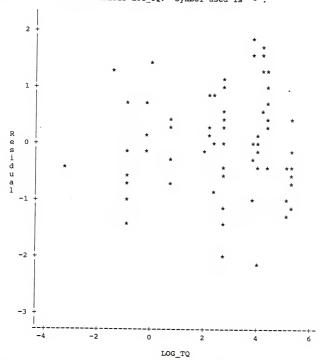
	Lower95%	Upper95%	
0bs	Predict	Predict	Residual
53	-0.7498	2.9032	0.4274
54	-0.7498	2.9032	-1.1821
55	-0.7498	2.9032	-0.4889
56	-0.7498	2.9032	-0.4889
57	-4.3735	-0.6020	-0.7311
58	-4.3735	-0.6020	-1.4242
59	-4.3735	-0.6020	-0.1715
60	-4.3735	-0.6020	-0.5080
61	-4.3735	-0.6020	-1.0188
62	-2.8625	1.0074	-0.7332
63	-2.8625	1.0074	-0.3454
64	-2.8625	1.0074	0.3477
65	-2.8625	1.0074	0.3654
66	-2.8625	1.0074	0.3654
67	-0.7741	3.0125	0.4902
68	-0.7741	3.0125	0.2671
69	-0.7741	3.0125	0.6726
70	-0.7741	3.0125	0.4902
71	-0.7741	3.0125	0.4902
72	-0.4710	3.3552	-0.4713
73	-0.4710	3.3552	-0.4488
74	-0.4710	3.3552	-2.1352
75	-0.4710	3.3552	0.1307
76	-0.4710	3.3552	-0.1751
77	-5.7206	-1.3717	-0.4712
78	-1.8322	1.7898	0.8967
79	-1.8322	1.7898	-0.8951
80	-1.8322	1.7898	0.0212
81	-1.5907	2.0370	0.3974
82	-1.5907	2.0370	0.6214
83	-1.5907	2.0370	0.2286
84	-1.5907	2.0370	-1.9491
85	-1.5907	2.0370	-0.4071
86	-1.5898	2.0380	-1.1404
87	-1.5898	2.0380	-1.1404
88	-1.5898	2.0380	0.0382
89	-1.5898	2.0380	-1.4281
90	-1.5898	2.0380	-0.5808

0bs	Lower95% Predict	Upper95% Predict	Residual
91 92 93 94 95 96	-1.3465 -1.3465 -1.3465 -1.3465 -1.3465 -4.8173	2.4223 2.4223 2.4223 2.4223 2.4223 -0.3941	0.6252 0.9662 -0.0679 -0.0679 1.0913 1.2194

Sum of Residuals -6.28386E-14
Sum of Squared Residuals 59.7784
Predicted Resid SS (Press) 86.9981

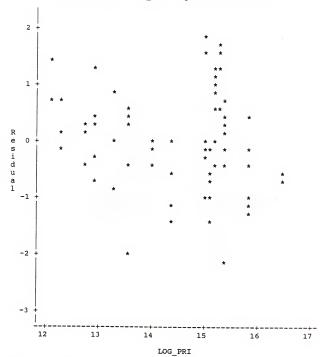


PREDICTION MODEL FOR CLEARING AND GRUBBING Plot of YRESID*LOG_TQ. Symbol used is '*'.



NOTE: 7 obs had missing values. 26 obs hidden.

PREDICTION MODEL FOR CLEARING AND GRUBBING Plot of YRESID*LOG_PRI. Symbol used is '*'.



NOTE: 7 obs had missing values. 24 obs hidden.

PREDICTION MODEL FOR CLEARING AND GRUBBING CONFIDENCE INTERVAL INDIVIDUAL PREDICTION

1 1.000 1.17057 0.17166 7.9824 7.9824 1.000 1.17057 0.17166 7.9824 3 1.000 1.17057 0.17166 7.9824 4 1.000 1.17057 0.17166 7.9824 4 1.000 1.17057 0.17166 7.9824 6 0.400 0.19992 0.02737 1.4602 6 0.400 0.19992 0.02737 1.4602 6 0.400 0.19992 1.00632 64.2344 8 5.650 9.50442 1.40632 64.2344 10 5.100 9.50442 1.40632 64.2344 10 5.100 9.50442 1.40632 64.2344 11 0.840 1.17743 0.18842 7.3579 13 5.880 1.17743 0.18842 7.3579 13 5.880 1.17743 0.18842 7.3579 15 0.420 1.17743 0.18842 7.3579 15 0.420 1.17743 0.18842 7.3579 16 0.300 2.08044 0.32328 13.3886 17 7.250 2.08044 0.32328 13.3886 18 11.190 2.08044 0.32328 13.3886 19 10.330 2.08044 0.32328 13.3886 20 10.330 2.08044 0.32328 13.3886 20 10.330 2.08044 0.32328 13.3886 21 3.000 2.15442 0.31153 14.8990 22 3.000 2.15442 0.31153 14.8990 22 3.000 2.15442 0.31153 14.8990 22 3.000 2.15442 0.31153 14.8990 22 3.000 2.15442 0.31153 14.8990 22 3.000 2.15442 0.31153 14.8990 23 2.650 2.15442 0.31153 14.8990 24 0.100	OBS	DEP VAR VALUE	PREDICT VALUE	LOWER 95%	UPPER 95%
2 1.000 1.17057 0.17166 7.9824 3 1.000 1.17057 0.17166 7.9824 4 1.000 1.17057 0.17166 7.9824 5 1.000 1.17057 0.17166 7.9824 5 1.000 1.17057 0.17166 7.9824 5 1.000 1.17057 0.17166 7.9824 6 0.400 0.19992 0.02737 1.4602 7 4.500 9.50442 1.40632 64.2344 9 5.650 9.50442 1.40632 64.2344 10 5.100 9.50442 1.40632 64.2344 11 0.840 1.17743 0.18842 7.3579 12 7.980 1.17743 0.18842 7.3579 13 5.880 1.17743 0.18842 7.3579 14 1.260 1.17743 0.18842 7.3579 15 0.420 1.17743 0.18842 7.3579 16 3.800 2.08044 0.32328 13.3886 17 7.250 2.08044 0.32328 13.3886 18 11.190 2.08044 0.32328 13.3886 18 11.190 2.08044 0.32328 13.3886 19 10.330 2.08044 0.32328 13.3886 19 10.330 2.08044 0.32328 13.3886 20 10.330 2.08044 0.32328 13.3886 21 3.000 2.15442 0.31153 14.8990 22 3.000 2.15442 0.31153 14.8990 24 0.100 2.5442 0.31153 14.8990 25 0.120 . 26 1.100 1.60824 0.24765 10.4439 27 1.400 1.60824 0.24765 10.4439 30 1.600 1.60824 0.24765 10.4439 31 0.490 33 0.230	000	VALUE	VALUE	PRED	PRED
2 1.000 1.17057 0.17166 7.9824 4 1.000 1.17057 0.17166 7.9824 4 1.000 1.17057 0.17166 7.9824 5 1.000 1.17057 0.17166 7.9824 5 1.000 1.17057 0.17166 7.9824 6 0.400 0.19992 0.02737 1.4602 7 4.500 9.50442 1.40632 64.2344 9 5.650 9.50442 1.40632 64.2344 9 5.650 9.50442 1.40632 64.2344 10 5.100 9.50442 1.40632 64.2344 11 0.840 1.17743 0.18842 7.3579 12 7.980 1.17743 0.18842 7.3579 13 5.880 1.17743 0.18842 7.3579 14 1.260 1.17743 0.18842 7.3579 15 0.420 1.17743 0.18842 7.3579 16 3.800 2.08044 0.32328 13.3886 17 7.250 2.08044 0.32328 13.3886 18 11.190 2.08044 0.32328 13.3886 18 11.190 2.08044 0.32328 13.3886 18 11.190 2.08044 0.32328 13.3886 19 10.330 2.08044 0.32328 13.3886 20 10.330 2.08044 0.32328 13.3886 21 3.000 2.15442 0.31153 14.8990 22 3.000 2.15442 0.31153 14.8990 23 2.650 2.15442 0.31153 14.8990 24 0.100 2.5442 0.31153 14.8990 25 0.120 26 1.100 1.60824 0.24765 10.4439 28 1.300 1.60824 0.24765 10.4439 29 1.700 1.60824 0.24765 10.4439 31 0.490 32 0.130 33 0.230 34 0.270 35 0.650 36 4.845 2.20448 0.24800 19.5957 39 8.230 2.39555 0.34379 16.6925 40 1.640 2.39555 0.34379 16.6925 41 6.580 2.39555 0.34379 16.6925 42 0.100 0.14656 0.02150 0.9989		1.000	1.17057	0.17166	7.9824
3 1.000 1.17057 0.17166 7.9824 4 1.000 1.17057 0.17166 7.9824 5 1.000 1.17057 0.17166 7.9824 6 0.400 0.19992 0.02737 1.4602 7 4.500 9.50442 1.40632 64.2344 8 5.650 9.50442 1.40632 64.2344 10 5.100 9.50442 1.40632 64.2344 11 0.840 1.17743 0.18842 7.3579 12 7.980 1.17743 0.18842 7.3579 13 5.880 1.17743 0.18842 7.3579 14 1.260 1.17743 0.18842 7.3579 15 0.420 1.17743 0.18842 7.3579 16 3.800 2.08044 0.32328 13.3886 17 7.250 2.08044 0.32328 13.3886 18 11.190 2.08044 0.32328 13.3886		1.000	1.17057		
4 1.000 1.17057 0.17166 7.9824 5 1.000 1.17057 0.17166 7.9824 6 0.400 0.19992 0.02737 1.4602 7 4.500 9.50442 1.40632 64.2344 8 5.650 9.50442 1.40632 64.2344 9 5.650 9.50442 1.40632 64.2344 11 0.840 1.17743 0.18842 7.3579 12 7.980 1.17743 0.18842 7.3579 13 5.880 1.17743 0.18842 7.3579 14 1.260 1.17743 0.18842 7.3579 15 0.420 1.17743 0.18842 7.3579 16 3.800 2.08044 0.32328 13.3886 17 7.250 2.08044 0.32328 13.3886 18 11.190 2.08044 0.32328 13.3886 20 10.330 2.08044 0.32328 13.3886		1.000	1.17057	0.17166	
5 1.000 1.17057 0.17166 7.9824 6 0.400 0.19992 0.02737 1.4602 7 4.500 9.50442 1.40632 64.2344 8 5.650 9.50442 1.40632 64.2344 10 5.100 9.50442 1.40632 64.2344 11 0.840 1.17743 0.18842 7.3579 12 7.980 1.17743 0.18842 7.3579 13 5.880 1.17743 0.18842 7.3579 14 1.260 1.17743 0.18842 7.3579 15 0.420 1.17743 0.18842 7.3579 16 3.800 2.08044 0.32328 13.3886 17 7.250 2.08044 0.32328 13.3886 18 11.190 2.08044 0.32328 13.3886 20 10.330 2.08044 0.32328 13.3886 21 3.000 2.15442 0.31153 14.8990 <td></td> <td>1.000</td> <td>1.17057</td> <td>0.17166</td> <td></td>		1.000	1.17057	0.17166	
6 0.400 0.19992 0.02737 1.4602 7 4.500 9.50442 1.40632 64.2344 8 5.650 9.50442 1.40632 64.2344 9 5.650 9.50442 1.40632 64.2344 10 5.100 9.50442 1.40632 64.2344 11 0.840 1.17743 0.18842 7.3579 13 5.880 1.17743 0.18842 7.3579 14 1.260 1.17743 0.18842 7.3579 15 0.420 1.17743 0.18842 7.3579 16 3.800 2.08044 0.32328 13.3886 17 7.250 2.08044 0.32328 13.3886 18 11.190 2.08044 0.32328 13.3886 18 11.190 2.08044 0.32328 13.3886 19 10.330 2.08044 0.32328 13.3886 20 10.330 2.08044 0.32328 13.3886 21 3.000 2.15442 0.31153 14.8990 23 2.650 2.15442 0.31153 14.8990 24 0.100		1.000	1.17057	0.17166	
7 4.500 9.50442 1.40632 64.2344 9 5.650 9.50442 1.40632 64.2344 10 5.100 9.50442 1.40632 64.2344 11 0.840 1.17743 0.18842 7.3579 12 7.980 1.17743 0.18842 7.3579 13 5.880 1.17743 0.18842 7.3579 14 1.260 1.17743 0.18842 7.3579 15 0.420 1.17743 0.18842 7.3579 16 3.800 2.08044 0.32328 13.3886 17 7.250 2.08044 0.32328 13.3886 18 11.190 2.08044 0.32328 13.3886 18 11.190 2.08044 0.32328 13.3886 19 10.330 2.08044 0.32328 13.3886 20 10.330 2.08044 0.32328 13.3886 21 3.000 2.15442 0.31153 14.8990 22 3.000 2.15442 0.31153 14.8990 24 0.100 2.500 2.15442 0.31153 14.8990 25 0.120 0.200 2.5		0.400	0.19992		
8 5.650 9.50442 1.40632 64.2344 9 5.650 9.50442 1.40632 64.2344 10 5.100 9.50442 1.40632 64.2344 11 0.840 1.17743 0.18842 7.3579 12 7.980 1.17743 0.18842 7.3579 13 5.880 1.17743 0.18842 7.3579 15 0.420 1.17743 0.18842 7.3579 16 3.800 2.08044 0.32328 13.3886 17 7.250 2.08044 0.32328 13.3886 18 11.190 2.08044 0.32328 13.3886 19 10.330 2.08044 0.32328 13.3886 21 3.000 2.15442 0.31153 14.8990 22 3.000 2.15442 0.31153 14.8990 23 2.650 2.15442 0.31153 14.8990 24 0.100 . . .	7	4.500	9.50442		
9 5.650 9.50442 1.40632 64.2344 11 0.840 1.17743 0.18842 7.3579 12 7.980 1.17743 0.18842 7.3579 13 5.880 1.17743 0.18842 7.3579 14 1.260 1.17743 0.18842 7.3579 15 0.420 1.17743 0.18842 7.3579 16 3.800 2.08044 0.32328 13.3886 17 7.250 2.08044 0.32328 13.3886 18 11.190 2.08044 0.32328 13.3886 19 10.330 2.08044 0.32328 13.3886 20 10.330 2.08044 0.32328 13.3886 21 3.000 2.15442 0.3123 14.8990 22 3.000 2.15442 0.31153 14.8990 23 2.650 2.15442 0.31153 14.8990 24 0.100 25 0.120 26 1.100 1.60824 0.24765 10.4439 28 1.300 1.60824 0.24765 10.4439 29 1.700 1.60824 0.24765 10.4439 29 1.700 1.60824 0.24765 10.4439 29 1.700 1.60824 0.24765 10.4439 31 0.490 32 0.130 33 0.230 34 0.270 35 0.650 36 4.845 2.20448 0.24800 19.5957 37 1.040 0.24562 0.0309 1.8230 38 8.230 2.39555 0.34379 16.6925 40 1.640 2.39555 0.34379 16.6925 41 6.580 2.39555 0.34379 16.6925 42 0.130 0.14656 0.02150 0.9989		5.650	9.50442		
10 5.100 9.50442 1.40632 64.2344 11 0.840 1.17743 0.18842 7.3579 12 7.980 1.17743 0.18842 7.3579 13 5.880 1.17743 0.18842 7.3579 14 1.260 1.17743 0.18842 7.3579 15 0.420 1.17743 0.18842 7.3579 16 3.800 2.08044 0.32328 13.3886 17 7.250 2.08044 0.32328 13.3886 18 11.190 2.08044 0.32328 13.3886 19 10.330 2.08044 0.32328 13.3886 20 10.330 2.08044 0.32328 13.3886 21 3.000 2.15442 0.31153 14.8990 22 3.000 2.15442 0.31153 14.8990 23 2.650 2.15442 0.31153 14.8990 24 0.100 . 25 0.120 . 26 1.100 1.60824 0.24765 10.4439 27 1.400 1.60824 0.24765 10.4439 28 1.300 1.60824 0.24765 10.4439 29 1.700 1.60824 0.24765 10.4439 30 1.600 1.60824 0.24765 10.4439 31 0.490 . 32 0.130 . 33 0.230 . 34 0.270 . 35 0.650 . 36 4.845 2.20448 0.24800 19.5957 37 1.040 0.24562 0.03309 1.8230 38 8.230 2.39555 0.34379 16.6925 40 1.640 2.39555 0.34379 16.6925 40 1.640 2.39555 0.34379 16.6925 40 1.640 2.39555 0.34379 16.6925 41 6.580 2.39555 0.34379 16.6925 42 0.130 0.14656 0.02150 0.9989	9	5.650	9.50442		
11 0.840 1.17743 0.18842 7.3579 12 7.980 1.17743 0.18842 7.3579 13 5.880 1.17743 0.18842 7.3579 14 1.260 1.17743 0.18842 7.3579 15 0.420 1.17743 0.18842 7.3579 16 3.800 2.08044 0.32328 13.3886 17 7.250 2.08044 0.32328 13.3886 18 11.190 2.08044 0.32328 13.3886 20 10.330 2.08044 0.32328 13.3886 21 3.000 2.15442 0.31153 14.8990 22 3.000 2.15442 0.31153 14.8990 23 2.650 2.15442 0.31153 14.8990 24 0.100 . . . 25 0.120 . . . 26 1.100 1.60824 0.24765 10.4439 28	10	5.100	9.50442		
12 7,980 1.17743 0.18842 7.3579 14 1.260 1.17743 0.18842 7.3579 14 1.260 1.17743 0.18842 7.3579 15 0.420 1.17743 0.18842 7.3579 16 3.800 2.08044 0.32328 13.3886 17 7.250 2.08044 0.32328 13.3886 18 11.190 2.08044 0.32328 13.3886 19 10.330 2.08044 0.32328 13.3886 20 10.330 2.08044 0.32328 13.3886 21 3.000 2.15442 0.31153 14.8990 22 3.000 2.15442 0.31153 14.8990 24 0.100 2.05442 0.31153 14.8990 24 0.100 2.05442 0.31153 14.8990 25 0.120 26 1.100 1.60824 0.24765 10.4439 27 1.400 1.60824 0.24765 10.4439 28 1.300 1.60824 0.24765 10.4439 29 1.700 1.60824 0.24765 10.4439 29 1.700 1.60824 0.24765 10.4439 30 1.600 1.60824 0.24765 10.4439 31 0.490 33 0.230 33 0.230 34 0.270 35 0.650 36 4.845 2.20448 0.24800 19.5957 37 1.040 0.24562 0.03309 1.8230 38 8.230 2.39555 0.34379 16.6925 40 1.640 2.39555 0.34379 16.6925 41 6.580 2.39555 0.34379 16.6925 41 6.580 2.39555 0.34379 16.6925	11	0.840	1.17743		
13 5.880 1.17743 0.18842 7.3579 14 1.260 1.17743 0.18842 7.3579 15 0.420 1.17743 0.18842 7.3579 16 3.800 2.08044 0.32328 13.3886 17 7.250 2.08044 0.32328 13.3886 18 11.190 2.08044 0.32328 13.3886 19 10.330 2.08044 0.32328 13.3886 20 10.330 2.08044 0.32328 13.3886 21 3.000 2.15442 0.31153 14.8990 23 2.650 2.15442 0.31153 14.8990 24 0.100 . . . 25 0.120 . . . 26 1.100 1.60824 0.24765 10.4439 28 1.300 1.60824 0.24765 10.4439 29 1.700 1.60824 0.24765 10.4439 30 </td <td>12</td> <td>7.980</td> <td>1.17743</td> <td></td> <td></td>	12	7.980	1.17743		
14 1.260 1.17743 0.18842 7.3579 15 0.420 1.17743 0.18842 7.3579 16 3.800 2.08044 0.32328 13.3886 17 7.250 2.08044 0.32328 13.3886 18 11.190 2.08044 0.32328 13.3886 19 10.330 2.08044 0.32328 13.3886 20 10.330 2.08044 0.32328 13.3886 21 3.000 2.15442 0.31153 14.8990 22 3.000 2.15442 0.31153 14.8990 23 2.650 2.15442 0.31153 14.8990 24 0.100 . . . 25 0.120 . . . 26 1.100 1.60824 0.24765 10.4439 27 1.400 1.60824 0.24765 10.4439 28 1.300 1.60824 0.24765 10.4439 30<	13	5.880	1.17743		
15 0.420 1.17743 0.18842 7.3579 16 3.800 2.08044 0.32328 13.3886 17 7.250 2.08044 0.32328 13.3886 18 11.190 2.08044 0.32328 13.3886 19 10.330 2.08044 0.32328 13.3886 20 10.330 2.08044 0.32328 13.3886 21 3.000 2.15442 0.31153 14.8990 22 3.000 2.15442 0.31153 14.8990 23 2.650 2.15442 0.31153 14.8990 24 0.100 25 0.120 26 1.100 1.60824 0.24765 10.4439 27 1.400 1.60824 0.24765 10.4439 28 1.300 1.60824 0.24765 10.4439 29 1.700 1.60824 0.24765 10.4439 30 1.600 1.60824 0.24765 10.4439 31 0.490 32 0.130 33 0.230 34 0.270 35 0.650 36 4.845 2.20448 0.24800 19.5957 37 1.040 0.24562 0.03309 1.8230 38 8.230 2.39555 0.34379 16.6925 40 1.640 2.39555 0.34379 16.6925 40 1.640 2.39555 0.34379 16.6925 41 6.580 2.39555 0.34379 16.6925 42 0.130 0.14656 0.02150 0.9989	14	1.260	1.17743		
16 3.800 2.08044 0.32328 13.3886 17 7.250 2.08044 0.32328 13.3886 18 11.190 2.08044 0.32328 13.3886 19 10.330 2.08044 0.32328 13.3886 20 10.330 2.08044 0.32328 13.3886 21 3.000 2.15442 0.31153 14.8990 22 3.000 2.15442 0.31153 14.8990 23 2.650 2.15442 0.31153 14.8990 24 0.100 . . . 25 0.120 . . . 26 1.100 1.60824 0.24765 10.4439 27 1.400 1.60824 0.24765 10.4439 29 1.700 1.60824 0.24765 10.4439 31 0.490 . . . 32 0.130 . . . 33 0.230	15	0.420	1.17743		
17 7.250 2.08044 0.32328 13.3886 18 11.190 2.08044 0.32328 13.3886 19 10.330 2.08044 0.32328 13.3886 20 10.330 2.08044 0.32328 13.3886 21 3.000 2.15442 0.31153 14.8990 22 3.000 2.15442 0.31153 14.8990 23 2.650 2.15442 0.31153 14.8990 24 0.100 . . . 25 0.120 . . . 26 1.100 1.60824 0.24765 10.4439 27 1.400 1.60824 0.24765 10.4439 29 1.700 1.60824 0.24765 10.4439 30 1.600 1.60824 0.24765 10.4439 31 0.490 . . . 32 0.130 . . . 33 0.230	16	3.800	2.08044		
18 11.190 2.08044 0.32328 13.3886 19 10.330 2.08044 0.32328 13.3886 20 10.330 2.08044 0.32328 13.3886 21 3.000 2.15442 0.31153 14.8990 22 3.000 2.15442 0.31153 14.8990 23 2.650 2.15442 0.31153 14.8990 24 0.100 . . . 25 0.120 . . . 26 1.100 1.60824 0.24765 10.4439 28 1.300 1.60824 0.24765 10.4439 29 1.700 1.60824 0.24765 10.4439 30 1.600 1.60824 0.24765 10.4439 31 0.490 . . . 32 0.130 . . . 33 0.230 . . . 34 0.270 .	17	7.250			
19 10.330 2.08044 0.23228 13.3886 20 10.330 2.08044 0.32328 13.3886 21 3.000 2.15442 0.31153 14.8990 22 3.000 2.15442 0.31153 14.8990 23 2.650 2.15442 0.31153 14.8990 24 0.100 2.55 0.120	18	11.190	2.08044		
20 10.330 2.08044 0.32328 13.3886 21 3.000 2.15442 0.31153 14.8990 22 3.000 2.15442 0.31153 14.8990 23 2.650 2.15442 0.31153 14.8990 24 0.100	19	10.330	2.08044		
21 3.000 2.15442 0.31153 14.8990 22 3.000 2.15442 0.31153 14.8990 23 2.650 2.15442 0.31153 14.8990 24 0.100 25 0.120 26 1.100 1.60824 0.24765 10.4439 28 1.300 1.60824 0.24765 10.4439 29 1.700 1.60824 0.24765 10.4439 30 1.600 1.60824 0.24765 10.4439 31 0.490 32 0.130 33 0.230 33 0.230 34 0.270 35 0.650 36 4.845 2.20448 0.24800 19.5957 37 1.040 0.24562 0.03309 1.8230 38 8.230 2.39555 0.34379 16.6925 40 1.640 2.39555 0.34379 16.6925 41 6.580 2.39555 0.34379 16.6925 41 6.580 2.39555 0.34379 16.6925 41 6.580 2.39555 0.34379 16.6925	20	10.330	2.08044		
22 3.000 2.15442 0.31153 14.8990 23 2.650 2.15442 0.31153 14.8990 24 0.100	21	3.000	2.15442		
23	22	3.000	2.15442		
24	23	2.650	2.15442		
26 1.100 1.60824 0.24765 10.4439 27 1.400 1.60824 0.24765 10.4439 28 1.300 1.60824 0.24765 10.4439 29 1.700 1.60824 0.24765 10.4439 30 1.600 1.60824 0.24765 10.4439 31 0.490		0.100			
27	25	0.120			
27	26	1.100	1.60824	0.24765	10.4439
28 1.300 1.60824 0.24765 10.4439 29 1.700 1.60824 0.24765 10.4439 30 1.600 1.60824 0.24765 10.4439 31 0.490	27	1.400	1.60824		
29 1.700 1.60824 0.24765 10.4439 30 1.600 1.60824 0.24765 10.4439 31 0.490	28	1.300	1.60824		
30		1.700	1.60824		
31	30	1.600	1.60824		
33 0.230	31	0.490			
34 0.270	32	0.130			
35 0.650 36 4.845 2.20448 0.24800 19.5957 37 1.040 0.24562 0.03309 1.8230 38 8.230 2.39555 0.34379 16.6925 39 8.230 2.39555 0.34379 16.6925 40 1.640 2.39555 0.34379 16.6925 41 6.580 2.39555 0.34379 16.6925 42 0.130 0.14656 0.02150 0.9989	33	0.230			
36 4.845 2.20448 0.24800 19.5957 37 1.040 0.24562 0.03309 1.8230 38 8.230 2.39555 0.34379 16.6925 39 8.230 2.39555 0.34379 16.6925 40 1.640 2.39555 0.34379 16.6925 41 6.580 2.39555 0.34379 16.6925 42 0.130 0.14656 0.02150 0.9989	34	0.270			
37 1.040 0.24562 0.03309 1.8230 38 8.230 2.39555 0.34379 16.6925 39 8.230 2.39555 0.34379 16.6925 40 1.640 2.39555 0.34379 16.6925 41 6.580 2.39555 0.34379 16.6925 42 0.130 0.14656 0.02150 0.9989		0.650			
37 1.040 0.24562 0.03309 1.8230 38 8.230 2.39555 0.34379 16.6925 39 8.230 2.39555 0.34379 16.6925 40 1.640 2.39555 0.34379 16.6925 41 6.580 2.39555 0.34379 16.6925 42 0.130 0.14656 0.02150 0.9989	36	4.845	2.20448	0.24800	19.5957
38 8.230 2.39555 0.34379 16.6925 39 8.230 2.39555 0.34379 16.6925 40 1.640 2.39555 0.34379 16.6925 41 6.580 2.39555 0.34379 16.6925 42 0.130 0.14656 0.02150 0.9989	37	1.040	0.24562		
39 8.230 2.39555 0.34379 16.6925 40 1.640 2.39555 0.34379 16.6925 41 6.580 2.39555 0.34379 16.6925 42 0.130 0.14656 0.02150 0.9989					
40 1.640 2.39555 0.34379 16.6925 41 6.580 2.39555 0.34379 16.6925 42 0.130 0.14656 0.02150 0.9989		8.230	2.39555		
41 6.580 2.39555 0.34379 16.6925 42 0.130 0.14656 0.02150 0.9989	40		2.39555		
42 0.130 0.14656 0.02150 0.9989	41	6.580			
	42	0.130	0.14656		
	43	0.170	0.14656		

PREDICTION MODEL FOR CLEARING AND GRUBBING CONFIDENCE INTERVAL INDIVIDUAL PREDICTION

OBS	DEP VAR VALUE	PREDICT VALUE	LOWER 95% PRED	UPPER 95% PRED
44	0.130	0.14656	0.02150	0.9989
45	0.130	0.14656	0.02150	0.9989
46	0.290	0.14656	0.02150	0.9989
47	1.700	2.62064	0.42328	16.2250
48	1.000	2.62064	0.42328	16.2250
49	1.700	2.62064	0.42328	16.2250
50	1.000	2.62064	0.42328	16.2250
51	0.750	2.62064	0.42328	16.2250
52	2.700	2.93497	0.47245	18.2326
53	4.500	2.93497	0.47245	18.2326
54	0.900	2.93497	0.47245	18.2326
55	1.800	2.93497	0.47245	18.2326
56	1.800	2.93497	0.47245	18.2326
57	0.040	0.08309	0.01261	0.5477
58	0.020	0.08309	0.01261	0.5477
59	0.070	0.08309	0.01261	0.5477
60	0.050	0.08309	0.01261	0.5477
61	0.030	0.08309	0.01261	0.5477
62	0.190	0.39552	0.05712	2.7385
63	0.280	0.39552	0.05712	2.7385
64	0.560	0.39552	0.05712	2.7385
65	0.570	0.39552	0.05712	2.7385
66	0.570	0.39552	0.05712	2.7385
67	5.000	3.06238	0.46110	20.3389
68	4.000	3.06238	0.46110	20.3389
69	6.000	3.06238	0.46110	20.3389
70 71	5.000	3.06238	0.46110	20.3389
72	5.000	3.06238	0.46110	20.3389
72	2.640	4.22953	0.62435	28.6521
74	2.700	4.22953	0.62435	28.6521
75	0.500	4.22953	0.62435	28.6521
76	4.820	4.22953	0.62435	28.6521
77	3.550	4.22953	0.62435	28.6521
78	0.018	0.02884	0.00328	0.2537
78 79	2.400	0.97902	0.16006	5.9883
80	0.400	0.97902	0.16006	5.9883
81	1.860	0.97902	0.16006	5.9883
82	2.327	1.25002	0.20378	7.6679
83	1.571	1.25002 1.25002	0.20378	7.6679
84	0.178	1.25002	0.20378	7.6679
85	0.832	1.25002	0.20378	7.6679
86	0.400	1.25002	0.20378	7.6679
0.0	0.400	1.25125	0.20397	7.6756

PREDICTION MODEL FOR CLEARING AND GRUBBING CONFIDENCE INTERVAL INDIVIDUAL PREDICTION

OBS	DEP VAR VALUE	PREDICT VALUE	LOWER 95% PRED	UPPER 95% PRED
87 88 89 90 91 92 93 94	0.40 1.30 0.30 0.70 3.20 4.50 1.60 1.60 5.10	1.25125 1.25125 1.25125 1.25125 1.71245 1.71245 1.71245 1.71245	0.20397 0.20397 0.20397 0.20397 0.26016 0.26016 0.26016 0.26016	7.6756 7.6756 7.6756 7.6756 11.2719 11.2719 11.2719 11.2719
96	0.25	0.07385	0.00809	0.6743

PREDICTION MODEL FOR CLEARING AND GRUBBING CONFIDENCE INTERVAL MEAN

	DDD			
OBS	DEP VAR VALUE	PREDICT VALUE	LOWER 95% MEAN	UPPER 95%
ODS	VALUE	VALUE	MEAN	MEAN
1	1.000	1.17057	0.55189	2.4828
2	1.000	1.17057	0.55189	2.4828
3	1.000	1.17057	0.55189	2.4828
4	1.000	1.17057	0.55189	2.4828
5	1.000	1.17057	0.55189	2.4828
6	0.400	0.19992	0.08022	0.4982
7	4.500	9.50442	4.58629	19.6965
8	5.650	9.50442	4.58629	19.6965
9	5.650	9.50442	4.58629	19.6965
10	5.100	9.50442	4.58629	19.6965
11	0.840	1.17743	0.72309	1.9172
12	7.980	1.17743	0.72309	1.9172
13	5.880	1.17743	0.72309	1.9172
14	1.260	1.17743	0.72309	1.9172
15	0.420	1.17743	0.72309	1.9172
16	3.800	2.08044	1.15503	3.7473
17	7.250	2.08044	1.15503	3.7473
18	11.190	2.08044	1.15503	3.7473
19	10.330	2.08044	1.15503	3.7473
20	10.330	2.08044	1.15503	3.7473
21	3.000	2.15442	0.98071	4.7328
22	3.000	2.15442	0.98071	4.7328
23	2.650	2.15442	0.98071	4.7328
24	0.100	•	•	•
25	0.120			•
26 27	1.100	1.60824	0.86816	2.9792
	1.400	1.60824	0.86816	2.9792
28	1.300	1.60824	0.86816	2.9792
29	1.700	1.60824	0.86816	2.9792
30	1.600	1.60824	0.86816	2.9792
31 32	0.490 0.130	•	•	•
33		•	•	•
34	0.230 0.270	•	•	•
35	0.650	•	•	•
36	4.845	2 20440		
37	1.040	2.20448 0.24562	0.60937 0.09523	7.9750
38	8.230	2.39555	1.07056	0.6335
39	8.230	2.39555		5.3604
40	1.640	2.39555	1.07056 1.07056	5.3604 5.3604
41	6.580	2.39555	1.07056	5.3604
42	0.130	0.14656	0.06918	
43	0.170	0.14656	0.06918	0.3105 0.3105
43	0.170	0.14030	0.00318	0.3102

PREDICTION MODEL FOR CLEARING AND GRUBBING CONFIDENCE INTERVAL MEAN

OBS	DEP VAR	PREDICT	LOWER 95%	UPPER 95%
OBS	VALUE	VALUE	MEAN	MEAN
44	0.130	0.14656	0.06918	0.31047
45	0.130	0.14656	0.06918	0.31047
46	0.290	0.14656	0.06918	0.31047
47	1.700	2.62064	1.66872	4.11558
48	1.000	2.62064	1.66872	4.11558
49	1.700	2.62064	1.66872	4.11558
50	1.000	2.62064	1.66872	4.11558
51	0.750	2.62064	1.66872	4.11558
52	2.700	2.93497	1.84392	4.67162
53	4.500	2.93497	1.84392	4.67162
54	0.900	2.93497	1.84392	4.67162
55	1.800	2.93497	1.84392	4.67162
56	1.800	2.93497	1.84392	4.67162
57	0.040	0.08309	0.04294	0.16081
58	0.020	0.08309	0.04294	0.16081
59 60	0.070	0.08309	0.04294	0.16081
61	0.050 0.030	0.08309	0.04294	0.16081
62	0.030	0.08309	0.04294	0.16081
63	0.190	0.39552 0.39552	0.17951	0.87145
64	0.260	0.39552	0.17951 0.17951	0.87145
65	0.570	0.39552	0.17951	0.87145 0.87145
66	0.570	0.39552	0.17951	0.87145
67	5.000	3.06238	1.54891	6.05469
68	4.000	3.06238	1.54891	6.05469
69	6.000	3.06238	1.54891	6.05469
70	5.000	3.06238	1.54891	6.05469
71	5.000	3.06238	1.54891	6.05469
72	2.640	4.22953	2.02842	8.81916
73	2.700	4.22953	2.02842	8.81916
74	0.500	4.22953	2.02842	8.81916
75	4.820	4.22953	2.02842	8.81916
76	3.550	4.22953	2.02842	8.81916
77	0.018	0.02884	0.00811	0.10249
78	2.400	0.97902	0.65657	1.45984
79	0.400	0.97902	0.65657	1.45984
80	1.000	0.97902	0.65657	1.45984
81	1.860	1.25002	0.82759	1.88807
82 83	2.327	1.25002	0.82759	1.88807
84	1.571 0.178	1.25002	0.82759	1.88807
85	0.178	1.25002	0.82759	1.88807
86	0.832	1.25002 1.25125	0.82759	1.88807
- 0	0.400	1.25125	0.82832	1.89011

PREDICTION MODEL FOR CLEARING AND GRUBBING CONFIDENCE INTERVAL

MEAN REDICT LOWER 95% UPPER 95 VALUE MEAN MEAN

	DEP VAR	PREDICT	LOWER 95%	UPPER 95%
OBS	VALUE	VALUE	MEAN	MEAN
87	0.40	1.25125	0.82832	1.89011
88	1.30	1.25125	0.82832	1.89011
89	0.30	1.25125	0.82832	1.89011
90	0.70	1.25125	0.82832	1.89011
91	3.20	1.71245	0.88830	3.30123
92	4.50	1.71245	0.88830	3.30123
93	1.60	1.71245	0.88830	3.30123
94	1.60	1.71245	0.88830	3.30123
95	5.10	1.71245	0.88830	3.30123
96	0.25	0.07385	0.01952	0.27945

PREDICTION MODEL FOR EXCAVATION

Model: MODEL1

Dependent Variable: LOG Q

Analysis of Variance

Source Prob>F	DF	Sum o Square		F Value
Model 0.0001	15	167.9313	39 11.19543	14.300
Error C Total	96 111	75.1594 243.0908		
Root MSE Dep Mean C.V.	6	.88482 .05121 .62223	R-square Adj R-sq	0.6908 0.6425

NOTE: Model is not full rank. Least-squares solutions for the parameters are not unique. Some statistics will be misleading. A reported DF of 0 or B means that the estimate is biased.

The following parameters have been set to 0, since the variables are a linear combination of other variables as shown.

 $\begin{array}{rcl}
NB & = 0 \\
LIMITED & = 0
\end{array}$

TYP_SUB = +1.0000 * INTERCEP -1.0000 * TYP_LAT -1.0000 * TYP REG

PREDICTION MODEL FOR EXCAVATION

Parameter Estimates

Variable	DF	Parameter Estimate	Standard Error	T for H0: Parameter=0
INTERCEP	В	5.755543	1.15383762	4.988
LOG TQ	1	0.437740	0.06741440	6.493
RC _	1	-2.554510	0.97370163	-2.624
NB	0	0	0.00000000	
II	1	-3.820465	1.03950182	-3.675
NC	1	-1.786693	0.99542305	-1.795
SG	1	-2.846023	1.21128889	-2.350
RURAL	1	-0.600389	0.38804644	-1.547
URBAN	1	0.442833	0.39311273	1.126
LIMITED	0	0	0.00000000	
LIGHT	1	1.242225	0.66366146	1.872
HEAVY	1	-0.943232	0.53831398	-1.752
MEDIUM	1	0.209213	0.52829870	0.396
TYP_LAT	В	0.122206	0.80662778	0.152
TYP_REG	В	-0.339945	0.53058174	-0.641
MAT_SAN	1	-0.733178	0.36182121	-2.026
MAT_ROC	1	-0.569347	0.73862584	-0.771
MAT_MUC	1	-0.058412	0.66913117	-0.087
TYP_SUB	0	0	0.00000000	•
Variable	DF	Prob > T		
INTERCEP	В	0.0001		
LOG TQ	1	0.0001		
RC -	1	0.0101		
NB	0			
II	1	0.0004		
NC	1	0.0758		
SG	1	0.0208		
RURAL	1	0.1251		
URBAN	1	0.2628		
LIMITED	0			
LIGHT	1	0.0643		
HEAVY	1	0.0829		
MEDIUM	1	0.6930		
TYP_LAT	В	0.8799		
TYP_REG	В	0.5232		
MAT_SAN	1	0.0455		
MAT_ROC	1	0.4427		
MAT_MUC	1	0.9306		
TYP_SUB	0	•		

PREDICTION MODEL FOR BASE

Model: MODEL1

Dependent Variable: LOG_PR

Analysis of Variance

Source Prob>F	DF	Sum Squar		Mean Square	F Value
Model 0.0001	13	111.705	65	8.59274	6.094
Error C Total	119 132	167.785 279.490		1.40996	
Root MSE Dep Mean C.V.	6	.18742 .68603 .75968		quare R-sq	0.3997 0.3341

NOTE: Model is not full rank. Least-squares solutions for the parameters are not unique. Some statistics will be misleading. A reported DF of 0 or B means that the estimate is biased.

The following parameters have been set to 0 since the

The following parameters have been set to 0, since the variables are a linear combination of other variables as shown.

LIMITED = 0

MEDIUM = +1.0000 * INTERCEP -1.0000 * RC -1.0000

* NB -1.0000 * II -1.0000 * NC -1.0000 * SG
+1.0000 * RURAL +1.0000 * URBAN -1.0000 * LIGHT

PREDICTION MODEL FOR BASE

Parameter Estimates

Variable	DF	Parameter Estimate	Standard Error	T for H0: Parameter=0
INTERCEP	В	3.557789	1.49403559	2,381
LOG_TQ	1	0.333261	0.08751048	3.808
RC _	В	1.592424	1.19927021	1.328
NB	В	2.434882	1.62305736	1.500
II	В	0.394522	1.32232460	0.298
NC	В	1.687546	1.31803515	1.280
SG	В	0.931067	1.22972997	0.757
RURAL	В	-1.062293	0.62745081	-1.693
URBAN	В	-1.356593	0.70336046	-1.929
LIMITED	0	0	0.00000000	
LIGHT	В	0.710581	0.51668602	1.375
HEAVY	В	-0.402573	0.42092363	-0.956
MEDIUM	0	0	0.00000000	
MAT_S	1	0.435642	0.80627156	0.540
MAT_R	1	-0.697203	0.61044422	-1.142
MAT_A	1	0.175503	0.66527526	0.264
Variable	DF	Prob > T		
INTERCEP	В	0.0188		
LOG TQ	1	0.0002		
RC	В	0.1868		
NB	В	0.1362		
II	В	0.7660		
NC	В	0.2029		
SG	В	0.4505		
RURAL	В	0.0931		
URBAN	В	0.0561		
LIMITED	0			
LIGHT	В	0.1716		
HEAVY	В	0.3408		
MEDIUM	0	•		
MAT_S	1	0.5900		
MAT_R	1	0.2557		
MAT_A	1	0.7924		

PREDICTION MODEL FOR ASPHALT

Model: MODEL1

Dependent Variable: LOG PR

Analysis of Variance

Source Prob>F	DF	Sum Squar		F Value
Model 0.0001	12	179.389	68 14.94914	27.549
Error C Total	159 171	86.279 265.668		
Root MSE Dep Mean C.V.	6	.73664 .15602 .96615	R-square Adj R-sq	0.6752 0.6507

NOTE: Model is not full rank. Least-squares solutions for the parameters are not unique. Some statistics will be misleading. A reported DF of 0 or B means that the estimate is biased.

The following parameters have been set to 0, since the variables are a linear combination of other variables as shown.

SG = 0

PREDICTION MODEL FOR ASPHALT

Parameter Estimates

Variable	DF	Parameter Estimate	Standard Error	T for H0: Parameter=0
INTERCEP	1	1.197071	1.01069511	1.184
LOG_TQ	1	0.558623	0.05482873	10.189
RC _	1	0.611475	0.60726660	1.007
NB	1	1.194745	0.65508380	1.824
II	1	0.153371	0.65915601	0.233
NC	1	0.070499	0.68073696	0.104
SG	0	0	0.00000000	
RURAL	1	-0.423256	0.37440741	-1.130
URBAN	1	-0.199363	0.41219455	-0.484
LIGHT	1	0.506167	0.85325634	0.593
HEAVY	1	-0.465685	0.84815043	-0.549
MEDIUM	1	-0.050946	0.82502085	-0.062
LIMITED	1	-0.274218	0.48376369	-0.567
SA	1	-0.221864	0.17256957	-1.286

Variable	DF	Prob > T
INTERCEP	1	0.2380
LOG_TQ	1	0.0001
RC _	1	0.3155
NB	1	0.0701
II	1	0.8163
NC	1	0.9176
SG	0	
RURAL	1	0.2600
URBAN	1	0.6293
LIGHT	1	0.5539
HEAVY	1	0.5837
MEDIUM	1	0.9508
LIMITED	1	0.5716
SA	1	0.2004

PREDICTION MODEL FOR STORM DRAINS

Model: MODEL1

Dependent Variable: LOG_PR

Analysis of Variance

Source Prob>F	DF	Sum Squar		Mean Square	F Value
Model 0.0001	12	53.303	72	4.44198	8.105
Error	69	37.816	23	0.54806	
C Total	81	91.119	95		
Root MSE Dep Mean C.V.	3.	.74031 .68330 .09912	R-sq Adj		0.5850 0.5128

NOTE: Model is not full rank. Least-squares solutions for the parameters are not unique. Some statistics will be misleading. A reported DF of 0 or B means that the estimate is biased.

The following parameters have been set to 0, since the variables are a linear combination of other variables as shown.

NB = 0

PREDICTION MODEL FOR STORM DRAINS

Parameter Estimates

Variable	DF	Parameter Estimate	Standard Error	T for H0: Parameter=0
INTERCEP	1	2.830616	0.94433243	2.997
LOG_TQ	1	0.286849	0.07693538	3.728
RC	1	-0.128761	0.51101104	-0.252
NB	0	0	0.00000000	
II	1	-0.219912	0.75908999	-0.290
NC	1	-0.191264	0.68748899	-0.278
SG	1	-1.298789	0.60321362	-2.153
RURAL	1	-0.146479	0.46762328	-0.313
URBAN	1	-0.115760	0.40123196	· - 0.289
HEAVY	1	-0.002649	0.84882994	-0.003
MEDIUM	1	0.223525	0.81835320	0.273
LIGHT	1	-0.461404	0.97466863	-0.473
DIA	1	-0.029787	0.01083138	-2.750
DEPTH	1	0.026092	0.09334668	0.280

Variable	DF	Prob > T
INTERCEP	1	0.0038
LOG_TQ	1	0.0004
RC	1	0.8018
NB	0	
II	1	0.7729
NC	1	0.7817
SG	1	0.0348
RURAL	1	0.7550
URBAN	1	0.7738
HEAVY	1	0.9975
MEDIUM	1	0.7856
LIGHT	1	0.6374
DIA	1	0.0076
DEPTH	1	0.7807

APPENDIX D COMPUTER SOURCE CODE

```
*TAB1:
PROC PRINT DATA = PHD.CLEAR4 SPLIT = '*';
 TITLE 'DATA SET FOR CLEARING AND GRUBBING':
 LABEL
JOB NO
              'PROJECT*NUMBER'
PROD RT =
              'PRODUCTION RATE*ACRES/DAY'
TOT QTY =
              'F1'
PRICE
              1221
RC
          =
              'F3'
NB
          =
              'FA'
II
          =
              1F51
NC
          =
              'F6'
SG
          =
              'F7'
RURAL
              'F8'
URBAN
        =
              1F91
LIMITED =
              'F10'
LIGHT
              'F11'
MEDIUM
          =
              'F12'
HEAVY
             'F13'
          =
TYP_L
             'C1'
         =
TYP M
             'C2'
         =
TYP_H
         = 'C3'
    VAR
JOB NO
PROD RT
TOT OTY
PRICE
RC
NB
II
NC
SG
RURAL
URBAN
LIMITED
LIGHT
MEDIUM
HEAVY
TYP L
TYP M
TYP_H
:
RUN:
PROC PRINT DATA = PHD.EXCAV4 SPLIT = '*';
 TITLE 'DATA SET FOR EXCAVATION';
 LABEL
```

```
JOB NO
            =
                'PROJECT*NUMBER'
QTY
                'PRODUCTION RATE*CY/DAY'
 TOTOTY
            =
                'F1'
PRICE
            =
                1F21
RC
                1F31
NB
            =
                'F4'
TT
            =
                'F5'
NC
                'F6'
SG
            =
                'F7'
RURAL
            =
                'F8'
URBAN
                'F9'
LIMITED
            =
                'F10'
LIGHT
            =
                'F11'
MEDIUM
            =
                'F12'
HEAVY
           =
                'F13'
TYP REG
           =
                'E1'
TYP LAT
           =
                'E2'
TYP SUB
           =
                'E3'
MAT SAN
           =
                'E4'
MAT ROC
          =
                'E5'
MAT MUC
                'E6'
    VAR
ЈОВ МО
QTY
TOTOTY
PRICE
RC
NB
ΙI
NC
SG
RURAL
URBAN
LIMITED
LIGHT
MEDIUM
HEAVY
TYP REG
TYP LAT
TYP SUB
MAT SAN
MAT ROC
MAT MUC
;
RUN:
PROC PRINT DATA = PHD.BASE4 SPLIT = '*';
*LAB3:
 TITLE 'DATA SET FOR BASE';
 LABEL
```

```
JOB NO = 'PROJECT*NUMBER'
PROD RT = 'PRODUCTION RATE*SY/DAY'
TOT QTY =
             1F1 1
PRICE
        =
             'F2'
RC
         =
             'F3'
NB
             'F4'
II
             'F5'
NC
         =
             'F6'
SG
             'F7'
RURAL
        '=
             'F8'
URBAN
        =
             'F9'
LIMITED =
             'F10'
LIGHT =
             'F11'
MEDIUM
        =
             'F12'
HEAVY
            'F13'
        =
MAT S
        =
             'B1'
MAT_R
        =
            'B2'
        = 'B3'
MAT_A
    VAR
JOB NO
PROD RT
TOT QTY
PRICE
RC
NB
ΙI
NC
SG
RURAL
URBAN
LIMITED
LIGHT
MEDIUM
HEAVY
MAT S
MAT R
MAT A
RUN:
*LAB6:
PROC PRINT DATA = PHD.ASPHALT5 SPLIT = '*';
TITLE 'DATA SET FOR ASPHALT PAVEMENT' ;
LABEL
JOB NO
             'PROJECT*NUMBER'
PROD RT
         =
             'PRODUCTION RATE*TN/DAY'
       =
TOT_QTY
             'F1'
PRICE
        =
             'F2'
RC
        =
             'F3'
NB
        =
             'F4'
II
             'F5'
```

```
NC
                'F6'
           =
SG
                'F7'
RURAL
                'F8'
URBAN
                1 F9 1
LIMITED
           =
                'F10'
LIGHT
                'F11'
MEDIUM
                'F12'
HEAVY
                'F13'
           =
SM AREA
                'A1'
    VAR
JOB NO
PROD RT
TOT OTY
PRICE
RC
NB
TT
NC
SG
RURAL
URBAN
LIMITED
LIGHT
MEDIUM
HEAVY
SM AREA
:
RUN:
*LAB7:
PROC PRINT DATA = PHD.STORM5 SPLIT = '*';
 TITLE 'DATA SET FOR STORM DRAIN' ;
 LABEL
ЈОВ ИО
                'PROJECT*NUMBER'
PROD RT
                'PRODUCTION RATE*LF/DAY'
TOT QTY
                'F1'
PRICE
           =
                'F2'
RC
                'F3'
           =
NB
           =
                1 F4 1
ΙI
           =
                'F5'
NC
           =
                'F6'
SG
           =
                'F7'
RURAL
           =
                'F8'
URBAN
           =
                'F9'
LIMITED
                'F10'
LIGHT
           =
                'F11'
MEDIUM
           =
                'F12'
HEAVY
                'F13'
DEPTH
                'ST1'
DIA
                'ST2'
;
```

```
VAR
JOB NO
PROD RT
TOT OTY
PRICE
RC
NB
TT
NC
SG
RURAL
URBAN
LIMITED
LIGHT
MEDIUM
HEAVY
DEPTH
DIA
RUN;
PROC REG DATA = PHD.CLEAR4;
  MODEL PROD RT =
TOT QTY PRICE RC NB II NC SG RURAL URBAN LIMITED
LIGHT MEDIUM HEAVY TOT_QTY2
TYP L TYP M TYP H
/ SELECTION=MAXR CP
 :
RUN:
PROC REG
          DATA = PHD.CLEAR4;
  MODEL PROD RT =
TOT_QTY PRICE RC NB II NC RURAL URBAN LIMITED
LIGHT MEDIUM
                   TOT QTY2
     TYP_M TYP_H
  CP P
OUTPUT OUT=REG1 OUT
P=YHAT
R=YRESID:
PLOT RESIDUAL. * PREDICTED. = ' * ';
TITLE 'PREDICTION MODEL FOR CLEAR AND GRUBB';
RUN:
PROC PLOT DATA= REG1_OUT;
PLOT YRESID*TOT_QTY="*";
PLOT YRESID*TOT QTY2='*';
PLOT YRESID*PRICE='*':
RUN;
PROC REG DATA = PHD.CLEAR4;
```

```
MODEL LOG PR =
LOG TO LOG PRI RC NB II NC SG RURAL URBAN
LIMITED
LIGHT MEDIUM HEAVY LOG TO2
TYP L TYP M TYP H
INAC LH INAC LM INAC LL
INAC_UH INAC_UM INAC_UL
INAC RH INAC RM INAC RL
/ SELECTION=MAXR CP
  :
RUN:
PROC REG DATA = PHD.CLEAR5;
   MODEL LOG_PR =
LOG TO
              RC NB TT NC SG
LIGHT
            MEDIUM HEAVY
TYP M TYP H
RURAL URBAN LIMITED
/ CP P CLM CLT
OUTPUT OUT=REG2 OUT
P=YHAT
R=YRESID
L95M = L95M
U95M =U95M
L95 =1.95
U95 =U95
:
PLOT RESIDUAL.*PREDICTED.='*';
TITLE 'PREDICTION MODEL FOR CLEARING AND
GRUBBING';
RUN:
PROC PLOT DATA= REG2 OUT;
PLOT YRESID*LOG_TQ='*';
PLOT YRESID*LOG PRI='*':
RUN:
DATA TRANS :
SET REG2 OUT:
YHAT = EXP(YHAT);
L95 = EXP(L95);
L95M = EXP(L95M);
U95M = EXP(U95M);
U95 = EXP(U95)
YRESID= EXP(YRESID);
RUN;
PROC PRINT DATA = TRANS SPLIT='*';
VAR PROD RT YHAT L95 U95
TITLE2 'CONFIDENCE INTERVAL':
TITLE3 'INDIVIDUAL PREDICTION':
```

```
LABEL
PROD RT = 'DEP VAR*VALUE'
       = 'PREDICT*VALUE'
L95
        = LOWER 95% * PRED'
1195
        ='UPPER 95%*PRED':
RIIN:
PROC PRINT DATA = TRANS SPLIT='*';
VAR PROD RT YHAT 1.95M
                       U95M :
TITLE2 'CONFIDENCE INTERVAL';
TITLE3 'MEAN':
LAREL.
PROD RT
            ='DEP VAR*VALUE'
YHAT
        = 'PREDICT*VALUE'
T.95M
        = LOWER 95% * MEAN!
U95M
        ='UPPER 95%*MEAN':
RUN:
DATA PHD. EXCAV5:
SET PHD. EXCAV5 ;
INAC LH = LIMITED *HEAVY;
INAC LM = LIMITED *MEDIUM;
INAC LL = LIMITED *LIGHT:
INAC UH = URBAN *HEAVY:
INAC UM = URBAN *MEDIUM:
INAC UL = URBAN *LIGHT:
INAC RH = RURAL *HEAVY:
INAC RM = RURAL
                 *MEDIUM;
INAC RL = RURAL
                  *LIGHT:
LOG Q = LOG(OTY):
LOG TQ = LOG(TOTOTY);
LOG PRI= LOG(PRICE):
LOG TQ2= LOG(TOTQTY2);
RUN;
PROC REG DATA = PHD.EXCAV5;
   MODEL LOG Q
LOG TO LOG PRI
                RC
                    NB II NC SG RURAL URBAN
LIMITED
LIGHT MEDIUM HEAVY LOG TQ2
TYP_LAT TYP_SUB TYP_REG MAT SAN MAT ROC MAT MUC
INAC LH INAC LM INAC LL
INAC UH INAC UM INAC UL
INAC_RH INAC_RM INAC_RL
/ SELECTION=MAXR CP
TITLE 'MODEL SELECTION EXCAVATION';
 ;
RUN:
PROC REG DATA = PHD. EXCAV5;
   MODEL LOG Q
                =
LOG TO
                   RC NB II NC SG RURAL URBAN
LIMITED
LIGHT HEAVY MEDIUM
TYP_LAT TYP_REG MAT_SAN MAT_ROC MAT_MUC TYP SUB
```

```
/ CP P CLM CLI
OUTPUT OUT=REG2 OUT
P=YHAT
R=YRESID
L95M =L95M
U95M = U95M
L95 =L95
U95 =U95
PLOT RESIDUAL. * PREDICTED. = ' * ' :
TITLE 'PREDICTION MODEL FOR EXCAVATION';
RUN:
PROC PLOT DATA= REG2 OUT:
PLOT YRESID*LOG TQ='*';
RUN:
DATA TRANS :
SET REG2 OUT:
YHAT = EXP(YHAT);
L95 = EXP(L95):
L95M = EXP(L95M);
U95M = EXP(U95M);
U95 = EXP(U95)
YRESID= EXP(YRESID);
RUN:
PROC PRINT DATA = TRANS SPLIT='*';
VAR QTY YHAT L95 U95 :
TITLE2 'CONFIDENCE INTERVAL';
TITLE3 'INDIVIDUAL PREDICTION';
LABEL.
OTY
       ='DEP VAR*VALUE'
TAHY
       = 'PREDICT*VALUE'
L95
       = LOWER 95%*PRED
U95
       ='UPPER 95%*PRED';
RUN:
PROC PRINT DATA = TRANS SPLIT='*';
VAR QTY YHAT L95M U95M :
TITLE2 'CONFIDENCE INTERVAL';
TITLE3 'MEAN';
LABEL
       = DEP VAR*VALUE
YTO
YHAT
      = 'PREDICT*VALUE'
L95M
      ='LOWER 95%*MEAN'
U95M
       ='UPPER 95%*MEAN';
RUN:
DATA PHD.BASE5:
SET PHD. BASE5 :
INAC LH = LIMITED *HEAVY:
INAC LM = LIMITED *MEDIUM;
```

```
INAC LL = LIMITED *LIGHT;
INAC UH = URBAN *HEAVY;
INAC UM = URBAN
                  *MEDIUM;
INAC UL = URBAN
                  *LIGHT:
INAC RH = RURAL
                  *HEAVY:
INAC RM = RURAL
                  *MEDIUM:
INAC RL = RURAL
                 *LIGHT;
TOT QTY2 = TOT QTY * TOT QTY;
LOG PR = LOG (PROD RT);
LOG_TQ = LOG(TOT_QTY);
LOG_PRI= LOG(PRICE);
LOG TQ2= LOG(TOT QTY2);
RUN:
PROC REG
          DATA = PHD.BASE5;
   MODEL LOG PR =
LOG TO LOG PRI RC NB II NC SG RURAL URBAN
LIMITED
LIGHT MEDIUM HEAVY LOG TO2
MAT S MAT R MAT A
INAC LH INAC LM INAC LL
INAC UH INAC UM INAC UL
INAC_RH INAC_RM INAC_RL
/ SELECTION=RMAX CP;
TITLE 'MODEL SELECTION BASE ':
RUN:
PROC REG
          DATA = PHD.BASE5;
   MODEL LOG PR =
LOG TO
                   RC NB II NC SG RURAL URBAN
LIMITED
LIGHT HEAVY MEDIUM
MAT_S MAT_R MAT_A
  CP P CLM CLI
OUTPUT OUT=REG1 OUT
P=YHAT
R=YRESID
L95M =L95M
U95M = U95M
L95 =L95
U95 =U95
PLOT RESIDUAL. *PREDICTED. = ' * ';
TITLE 'PREDICTION MODEL FOR BASE':
RUN;
PROC PLOT DATA= REG1 OUT;
PLOT YRESID*LOG TO='*':
PLOT YRESID*LOG PRI='*';
RUN:
```

```
DATA TRANS :
SET REG1 OUT:
YHAT = EXP(YHAT):
L95 = EXP(L95);
L95M = EXP(L95M);
U95M = EXP(U95M);
U95 = EXP(U95)
YRESID= EXP(YRESID):
RUN:
PROC PRINT DATA = TRANS SPLIT='*';
VAR PROD RT YHAT L95
                        1195
TITLE2 'CONFIDENCE INTERVAL';
TITLE3 'INDIVIDUAL PREDICTION':
LABEL.
PROD RT = DEP VAR*VALUE
TAHY
        = 'PREDICT*VALUE'
T.95
        ='LOWER 95%*PRED'
1195
        ='UPPER 95%*PRED':
RUN:
PROC PRINT DATA = TRANS SPLIT='*';
VAR PROD RT YHAT L95M
                        U95M:
TITLE2 'CONFIDENCE INTERVAL':
TITLE3 'MEAN';
LABEL.
PROD RT = DEP VAR*VALUE
YHAT
        = 'PREDICT*VALUE'
1.95M
        = LOWER 95% *MEAN!
U95M
        ='UPPER 95%*MEAN':
RUN:
DATA PHD. ASPHALT6;
SET PHD. ASPHALT6:
INAC LH = LIMITED *HEAVY;
INAC LM = LIMITED *MEDIUM:
INAC LL = LIMITED *LIGHT:
INAC UH = URBAN
                 *HEAVY:
INAC UM = URBAN
                  *MEDIUM:
INAC UL = URBAN
                  *LIGHT;
INAC RH = RURAL
                  *HEAVY;
INAC RM = RURAL
                  *MEDIUM;
INAC_RL = RURAL
                 *LIGHT;
TOT QTY2 = TOT_QTY * TOT QTY;
LOG PR = LOG(PROD RT);
LOG TQ = LOG(TOT_QTY);
LOG PRI= LOG(PRICE);
LOG TQ2= LOG(TOT QTY2);
RUN:
PROC REG
           DATA = PHD.ASPHALT6:
   MODEL LOG PR
LOG TQ LOG PRI
                RC
                    NB II NC SG RURAL URBAN
LIMITED
LIGHT MEDIUM HEAVY LOG TQ2
```

```
SM AREA
INAC LH INAC LM INAC LL
INAC UH INAC UM INAC UL
INAC RH INAC RM INAC RL
/ SELECTION=MAXR CP;
TITLE 'MODEL SELECTION ASPHALT';
RUN:
PROC REG DATA = PHD.ASPHALT6:
   MODEL LOG PR =
LOG TO
              RC NB II NC SG RURAL URBAN
LIGHT HEAVY MEDIUM LIMITED
SA
   CP P CLM CLI
OUTPUT OUT=REG1 OUT
P=YHAT
R=YRESID
L95M = L95M
U95M = U95M
L95 =L95
U95 =U95
PLOT RESIDUAL. *PREDICTED. = '*':
TITLE 'PREDICTION MODEL FOR ASPHALT':
RIIN:
PROC PLOT DATA= REG1 OUT;
PLOT YRESID*LOG TO='*':
PLOT YRESID*LOG PRI='*';
RUN:
DATA TRANS :
SET REG1 OUT:
YHAT = EXP(YHAT);
L95 = EXP(L95);
L95M = EXP(L95M);
U95M = EXP(U95M);
U95 = EXP(U95)
YRESID= EXP(YRESID);
RUN:
PROC PRINT DATA = TRANS SPLIT='*';
VAR PROD RT YHAT L95
TITLE2 'CONFIDENCE INTERVAL':
TITLE3 'INDIVIDUAL PREDICTION';
LABEL
PROD RT = 'DEP VAR*VALUE'
YHAT
      = 'PREDICT*VALUE'
L95
       ='LOWER 95%*PRED'
U95
      ='UPPER 95%*PRED';
```

```
RUN:
PROC PRINT DATA = TRANS SPLIT='*';
VAR PROD RT YHAT L95M
                       U95M :
TITLE2 'CONFIDENCE INTERVAL':
TITLE3 'MEAN':
LABET.
PROD RT = 'DEP VAR * VALUE '
TAHY
       ='PREDICT*VALUE'
L95M
        = ! LOWER 95% * MEAN!
U95M
        ='UPPER 95%*MEAN';
RUN:
DATA PHD.STORM6:
SET PHD.STORM6 ;
INAC_LH = LIMITED *HEAVY;
INAC LM = LIMITED *MEDIUM;
INAC LL = LIMITED *LIGHT;
INAC UH = URBAN
                 *HEAVY;
INAC UM = URBAN *MEDIUM;
INAC UL = URBAN *LIGHT;
INAC RH = RURAL
                *HEAVY;
INAC RM = RURAL
                *MEDIUM:
INAC RL = RURAL
                 *LIGHT;
TOT_{Q}TY2 = TOT_{Q}TY * TOT_{Q}TY;
LOG PR = LOG(PROD RT);
LOG TQ = LOG (TOT QTY);
LOG PRI= LOG(PRICE);
LOG TQ2= LOG (TOT QTY2);
RUN:
PROC REG
          DATA = PHD.STORM6;
   MODEL LOG PR =
LOG_TQ LOG PRI
                RC
                    NB II NC SG RURAL URBAN
LIMITED
LIGHT MEDIUM HEAVY LOG TQ2
DEPTH DIA
INAC_LH INAC_LM INAC LL
INAC UH INAC UM INAC UL
INAC RH INAC RM INAC RL
/ SELECTION=MAXR CP:
TITLE 'MODEL SELECTION STORM DRAINS ';
RUN;
PROC REG
           DATA = PHD.STORM6:
  MODEL LOG_PR =
LOG_TQ LOG PRI RC
                     II NC SG RURAL URBAN
      HEAVY MEDIUM
    INAC_UH INAC_RH INAC RL
DIA
   CP P CLM CLI
OUTPUT OUT=REG1 OUT
P=YHAT
R=YRESID
```

```
L95M = L95M
U95M = U95M
L95 =L95
U95 =U95
PLOT RESIDUAL. *PREDICTED. = ' * ';
TITLE 'PREDICTION MODEL FOR STORM DRAINS';
RUN:
PROC PLOT DATA= REG1 OUT;
PLOT YRESID*LOG TQ='*';
PLOT YRESID*LOG PRI='*';
PLOT YRESID*DIA='*':
RUN:
DATA TRANS ;
SET REG1 OUT;
YHAT = EXP(YHAT);
L95 = EXP(L95);
L95M = EXP(L95M);
U95M = EXP(U95M);
U95 = EXP(U95)
YRESID= EXP(YRESID);
RUN;
PROC PRINT DATA = TRANS SPLIT='*':
VAR PROD RT YHAT L95 U95 ;
TITLE2 'CONFIDENCE INTERVAL';
TITLE3 'INDIVIDUAL PREDICTION';
LABEL
PROD RT = 'DEP VAR*VALUE'
YHAT
      = 'PREDICT*VALUE'
L95
       ='LOWER 95%*PRED'
U95
       ='UPPER 95%*PRED';
RUN:
PROC PRINT DATA = TRANS SPLIT='*':
VAR PROD RT YHAT L95M U95M :
TITLE2 'CONFIDENCE INTERVAL':
TITLE3 'MEAN':
LABEL
PROD RT = 'DEP VAR*VALUE'
       = 'PREDICT*VALUE'
YHAT
L95M
       ='LOWER 95%*MEAN'
U95M
       ='UPPER 95%*MEAN';
RUN:
```

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I certify that I have read this study and that in my opinion it conforms to acceptable standards of scholarly presentation and is fully adequate, in scope and quality, as a dissertation for the degree of Doctor of Philosophy.

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